



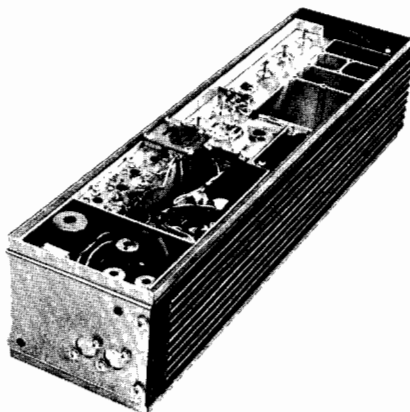
communications

MASTR

Progress Line

132-174 MC RECEIVER MODELS 4ER41A22-27

(WITH NOISE BLANKERS)



SPECIFICATIONS *

FCC Filing Designation

ER-41-A

Frequency Range

132-174 MC

Audio Output

2 watts at less than 10% distortion
(using Speaker Model 4EZ16A10)

Sensitivity

12-db SINAD (EIA Method) 0.35 μ v
20-db Quieting Method 0.5 μ v

Selectivity

EIA Two-Signal Method -85 db (adjacent channel, 30 KC channels)
20-db Quieting Method -100 db at ± 15 KC

Spurious Response

-100 db

Frequency Stability

$\pm 0.0005\%$ (-30°C to $+60^{\circ}\text{C}$)

Modulation Acceptance

± 6 KC (narrow-band)

Squelch Sensitivity

Critical Squelch 0.15 μ v
Maximum Squelch Greater than 20 db quieting (less than 2 μ v)

Intermodulation (EIA)

-60 db

Maximum Frequency Separation

0.4%

Frequency Response

+1 and -8 db of a standard 6-db per octave
de-emphasis curve from 300 to 3000 cps
(1000-cps reference)

*These specifications are intended primarily for the use of the serviceman. Refer to the appropriate Certified and Guaranteed Specification Sheet for the complete specifications.

Maintenance Manual LBI-3595

ER-41-A

GENERAL  ELECTRIC

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WARNING

No one should be permitted to handle any portion of the equipment that is supplied with high voltage; or to connect any external apparatus to the units while the units are supplied with power.

DESCRIPTION

General Electric MASTR Progress Line Receiver Type ER-41-A is a double conversion, superheterodyne FM receiver designed for operation on the 132-174 megacycle band.

The receiver is of single-unit construction and is completely housed in an aluminum casting for maximum shielding and rigidity. The top part of the casting contains the front end through the 1st Low IF Amplifier stages and the Noise Blanker Board. The bottom portion of the casting contains the Audio Squelch Board and the optional Channel Guard Board.

CIRCUIT ANALYSIS

The MASTR Progress Line Receiver is completely transistorized, using a total of 26 silicon transistors. Input leads to the receiver are individually filtered by the 20-pin feed-through by-pass connector J443.

A regulated +10 volts is used for all receiver stages except the audio PA stage which operates from the 12-volt system supply.

Centralized metering jack J442 is provided for use with General Electric Test Set, Model 4EX3A10, for ease of alignment and servicing. The Test Set meters the oscillator, multiplier, and limiter stages as well as the discriminator, audio PA, voice coil and regulated 10 volts.

RF AMPLIFIERS (A301/A302 and A303/A304)

The 1st RF Amplifier A301 (132-150.8 MC) or A302 (150.8-174 MC) consists of three tuned helical resonators and an RF amplifier stage (Q1). The RF signal from the antenna is coupled by RF cable W441 to a tap on L301/L304. The tap is positioned to insure the proper impedance match to the antenna. RF energy is coupled through the three coils by openings in the shield walls, to the base of RF amplifier Q1. The output of Q1 is LC coupled through transformer T1/T2 to helical resonators L307/L309 and L308/L310, and then to a second RF amplifier stage A303 (132-150.8 MC) or A304 (150.8-174 MC).

The output of the A303/A304-Q1 is coupled through transformer T1/T2 to helical resonator L112/L113, and then to the base of the 1st mixer (A305-Q1). Neutralizing for the 2nd RF amplifier stage is provided by A303/A304-C7.

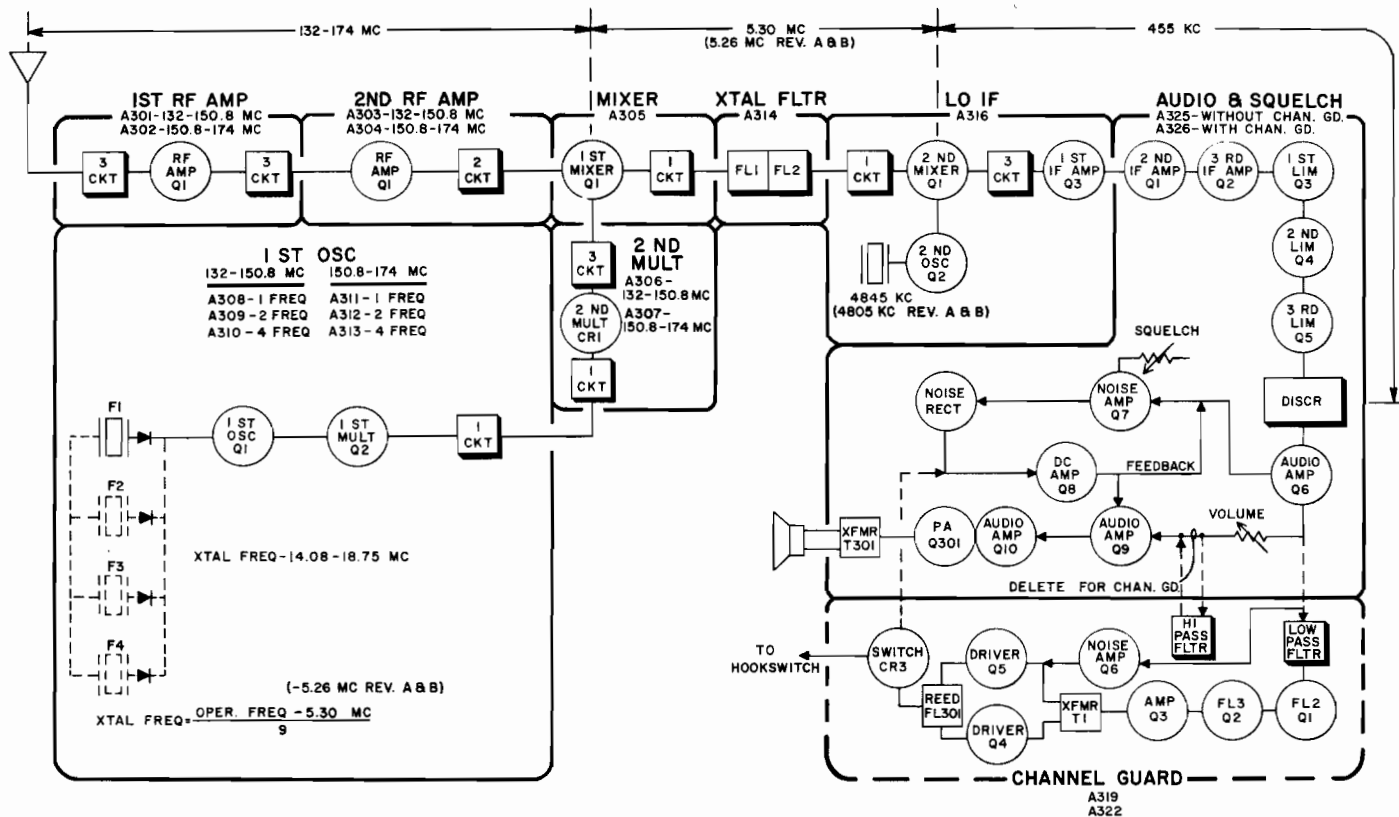


Figure 1 - Receiver Block Diagram

1ST OSCILLATOR AND MULT-1 (A308-A313)

The receiver 1st oscillator operates in a transistorized Colpitts oscillator circuit. The oscillator crystal operates in a fundamental mode at a frequency of approximately 14 to 18 megacycles. The crystal is cut to provide temperature compensation at the high end of the temperature range and is thermistor compensated at low temperatures. This provides $\pm .0005\%$ frequency stability as soon as the receiver is energized--without the warm-up time required by crystal ovens or warmers.

In single-frequency receivers, a jumper from P6 to C311 connects the regulated 10 volts to the crystal circuit, which forward biases diode CRL1. Forward biasing the diode reduces its impedance, so that the crystal frequency is applied to the base of oscillator transistor Q1. Feedback for the oscillator is developed across C21/C22. The oscillator output is fed through C24 to the base of the 1st multiplier Q2.

Multi-frequency receivers use only one oscillator transistor, and up to three additional crystal circuits, identical to the F1 crystal circuit, can be added. The 10-volt jumper is removed, and the proper frequency is selected by switching the desired crystal circuit to +10 volts by means of a frequency selector switch on the Control Unit.

The output of the 1st multiplier (tripler Q2) is transformer-coupled (T1/T2) to the 2nd multiplier assembly. The 1st multiplier tank is tuned to three times the crystal frequency. This stage is metered at centralized metering jack J442-4 through metering network CR5, R16, R303 and C32.

2ND MULTIPLIER (A306/A307)

Coupling from the 1st multiplier tank is through A306-T1/T2 to the anode of multiplier diode A306-CR1. Three resonant LC circuits (T3/T4, T5/T6 and T7/T8) follow CR1 and are tuned to nine times the crystal frequency. The 2nd multiplier output is fed through C13 to the base of the first mixer.

1ST MIXER (A305) AND CRYSTAL FILTER (A314)

The RF signal from the RF amplifiers and the low-side injection voltage from the 2nd multiplier are applied to the base of 1st mixer A305-Q1. The mixer collector tank (L1 and C3) is tuned to 5.30 megacycles (5.26 MC in Revision A and B receivers), and provides impedance matching to the high IF filter.

The highly selective, two-stage crystal filter (A314) following the 1st mixer provides the major selectivity for the receiver. The output of the filter is fed through impedance matching transformer A316-T1 to the base of the 2nd mixer.

2ND OSCILLATOR, 2ND MIXER AND 1ST IF AMPLIFIER (A316)

The 2nd oscillator A316-Q2 operates in a Colpitts oscillator circuit, with feedback supplied through C2. The oscillator frequency is 4845 KC (4805 KC in Revision A and B receivers) with the low-side injection voltage fed to the base of the 2nd mixer.

The Hi IF signal from the filter is fed to the base of 2nd mixer A316 (Q1) with the 2nd oscillator output. The 455 KC 2nd mixer output is fed to three tuned low IF circuits (L1, L2, L3). L1, L2 and L3 are required for shaping the nose of the IF waveform, and also reject the undesired output frequencies from the mixer.

The low IF signal is coupled through C14 to the base of the 1st low IF amplifier A316-Q3. The output of A316-Q3 is RC coupled to the base of the 2nd IF amplifier.

2ND IF AMPLIFIERS AND LIMITERS (A325)

Following A316-Q3 are two additional RC coupled low IF amplifiers (A325-Q1 and -Q2). The 2nd IF amplifier stage is metered at J442-2 through metering network C8, CR1 and R12.

After the IF amplifiers are three RC coupled limiter stages (A325-Q3, -Q4 and -Q5). First limiter metering is provided at J442-3 through metering network C13, CR2, R18 and C15.

DISCRIMINATOR (A325)

The receiver utilizes a Foster-Seely type discriminator. The output of the 3rd limiter is connected to a tap on the primary tuned circuit of discriminator T1. This allows the discriminator to operate at a higher level. Diodes CR5 and CR6 rectify the 455 KC IF signals to recover the audio. The stage is metered at J442-10 through metering network R27 and C22.

1ST AUDIO AMPLIFIER (A325)

The output of the discriminator is fed to the 1st audio amplifier (Q6). This stage operates as an emitter-follower to match the impedance of the discriminator to the noise amplifier stage and VOLUME control. Q6 also provides some power gain.

AUDIO AMPLIFIERS

When audio is present in the incoming signal, it is taken off the emitter of Q6 and connected to the VOLUME control through A325-J9. The VOLUME control arm connects to A325-J8 which feeds the audio signal to the base of the 2nd audio amplifier, Q9. C34, C36, C37 and L4 make up the de-emphasis network. The collector current of Q9 should be adjusted to 650 milliamps by potentiometer R47 as indicated by a reading of 0.65 volts at metering jack J442-1. This adjustment should be made with the VOLUME control fully counterclockwise. Thermistor RT1 keeps the output current constant over wide variations in temperature after R47 has been set.

Following Q9 is a Darlington circuit, which consists of compound-connected transistors Q10 and Q310. The Darlington circuit provides a higher input impedance than is normally encountered in transistor amplifiers. Also, this circuit has a more linear operation, with less distortion at maximum power output.

The output of the amplifier stage is coupled by audio transformer T301 to the loudspeaker. Audio high and low are present at the centralized metering jack (J442). When the General Electric Test Set is connected to J442, these leads are connected to the black and green jacks for sensitivity, frequency response, distortion, power output and other measurements.

SQUELCH

Noise from audio amplifier Q6 is used to operate the squelch circuit. When no carrier is present in the receiver, noise is coupled to the base of noise amplifier Q7. The gain of the noise amplifier is determined by the SQUELCH control, which varies the bias on the base of Q7.

The noise amplifier output is fed through a high-pass filter (C30 and L1) which attenuates frequencies below 3 KC. Thermistor RT2 keeps the critical squelch constant over wide variations in temperature.

Noise from the high-pass filter is rectified by CR3 and CR4, and the negative DC output of the noise rectifiers is fed to the base of DC amplifier Q8.

DC amplifier Q8 acts as a squelch switch. A negative output from the noise rectifiers cuts off the DC amplifier. When cut off, the collector is at the +10 volt supply potential. This positive voltage is fed to the base of Q9, a PNP transistor, cutting it off. Since audio stages Q9, Q10 and Q301 are DC coupled, Q10 and Q301 are cut off also. The positive voltage from the collector circuit of the DC amplifier is used as feedback through R33 to the base of noise amplifier Q7, causing it to conduct more heavily. This feedback helps to sharply cut off Q8, providing sharp, rapid switching action.

When the receiver is quieted by a signal, noise voltage from the noise rectifiers is reduced; and the DC amplifier conducts. While conducting, the collector potential of Q8 is negative; and negative feedback to the base of noise amplifier Q7 causes it to conduct less.

This negative voltage is applied to the base of PNP transistor Q9, causing it to conduct. Now, all the audio stages are turned on and sound is heard at the loudspeaker.

With the receiver squelched, the final audio amplifiers are cut off; and the receiver drain is less than 50 milliamps in 12-volt systems.

It should be noted that a hysteresis effect was designed into the squelch circuit and, as a result, the squelch does not operate in the same manner as other conventional squelch circuits. The circuit is designed so that a weak signal will open the squelch. The signal may be reduced by 3 to 5 db without the squelch closing. This limits squelch "flutter" or "picket-fence" operation.

NOISE BLANKER (A320/A321 - FIGURE 2)

An RF signal and noise pulse from the antenna is fed simultaneously to the Noise Blanker and receiver RF amplifier section. The signal and noise is transformer coupled through T1/T2 to the base of the first of three RF amplifier stages. The three amplifier stages (Q1, Q2 and Q3) raise the level of the noise pulse which is coupled through T9/T10 and L13 to the base of pulse detector Q4. A metering network consisting of R13, C21, C22 and CR2 permits the blanker to be metered at centralized metering jack J442-11.

Base bias for the pulse detector is established by R12 and CR1. CR1 is normally conducting, which keeps Q4 in a barely conducting state. A noise pulse applied to the base of Q4 causes it to conduct heavily. This results in a negative pulse at the output (collector) of Q4. Following Q4 is a low-pass RF filter (C23 and L14).

The output of the filter is fed to the base of pulse amplifier, Q5. This stage is biased by CR3, R16 and R18 so that it is just conducting. The negative-going pulse from the pulse detector cuts CR3

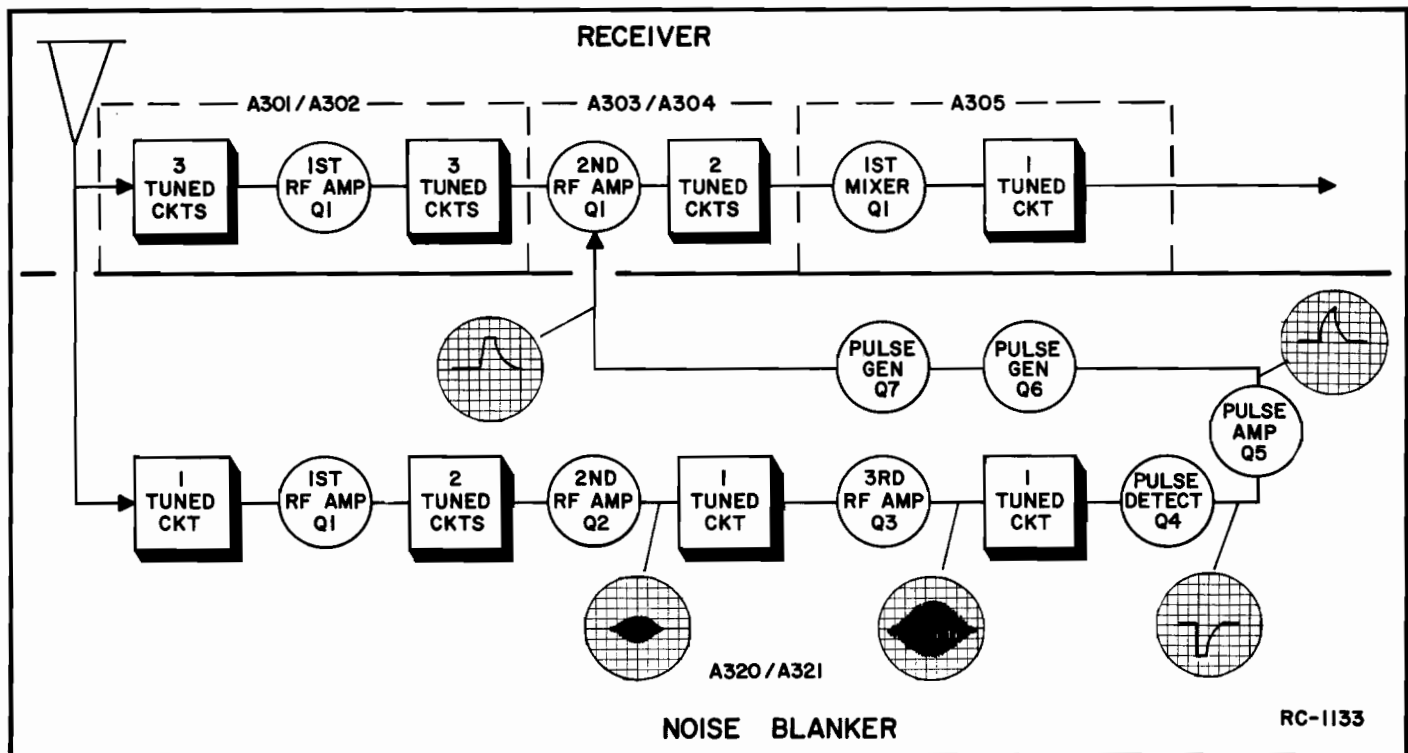


Figure 2 - Noise Blanker Block Diagram

off, which biases Q5 on, and a positive pulse appears at the output of Q5.

Q6 and Q7 form part of the one-shot multivibrator circuit. Bias voltage through R24 keeps Q6 normally turned on. The positive voltage at the collector of Q6 keeps Q7 turned off. The amplified positive-going pulse from the pulse amplifier (Q5) is fed to the base of Q6, cutting the stage off. As Q6 cuts off, Q7 is turned on; and the output is a positive-going blanking pulse. The positive blanking pulse is fed to the emitter of A303/A304-Q1, which cuts off that stage for the duration of the noise pulse.

The blanking pulse width is determined by R24 and C34. Diode CR6 keeps the output pulse a square wave. CR5 prevents oscillation at temperature extremes.

At the same time the blanking pulse is fed to the receiver, samples of the pulse are fed to the automatic repetition rate switch consisting of C29, C33, CR4, R17, R18 and R21. The pulse sample is coupled through C33 and rectified by CR4. This voltage charges C29 and then discharges through R17 and R18, turning off pulse amplifier Q5. The time constant of C29, R17 and R18 are selected so that output pulses from Q7 will never exceed two kilocycles. This prevents blanking the receiver for a long enough time to keep the desired signal from being heard.

As the noise signal from the antenna is applied to the Noise Blanker, the RF signal is applied to the receiver RF amplifier (A301/A302). The six tuned circuits in the receiver provide a time delay for the RF signal, which enables the blanking pulse from the Noise Blanker to cut off the RF amplifier in the receiver before the noise pulse can get there.

MAINTENANCE

MOBILE DISASSEMBLY

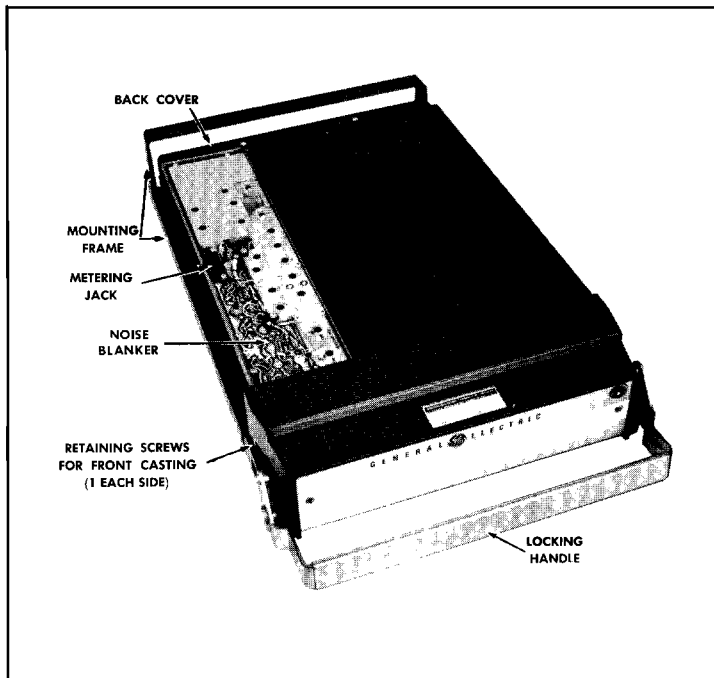


Figure 3 - Removing Top Cover

To service the receiver from the top--

1. Pull locking handle down and pull radio about one inch out of mounting frame.
2. Pry up cover at rear of receiver.
3. Slide cover back and lift off.

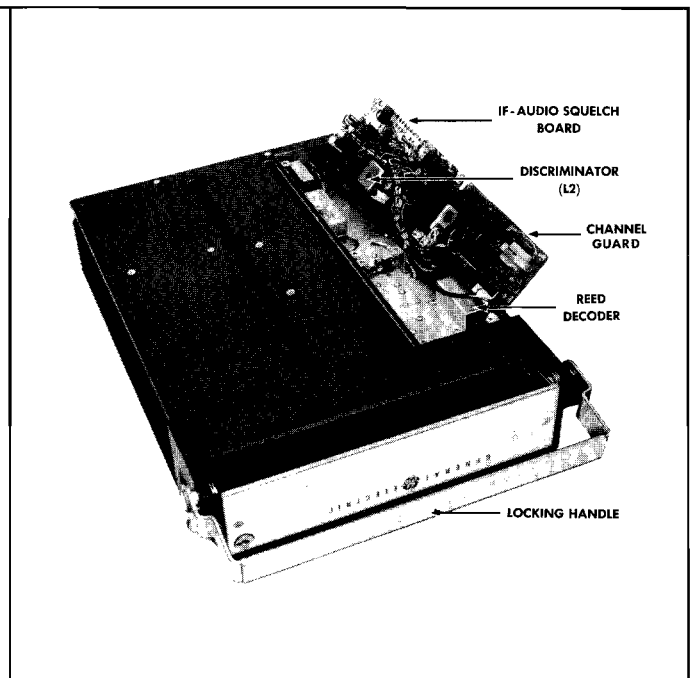


Figure 4 - Removing Bottom Cover

To service the receiver from the bottom--

1. Pull locking handle down. Pull radio out of mounting frame.
2. Remove screws in bottom cover. Pry up cover at back of receiver.
3. Slide cover back and lift off.

To remove the receiver from the system frame--

1. Loosen the two Phillips-head retaining screws in front casting (see Figure 3), and pull casting away from system frame.
2. Remove the four screws in the back cover.
3. Remove the two screws holding the receiver at each end of the system frame.
4. Disconnect the antenna jack and the 20-pin connector from the front of the receiver, and slide the unit out of the system frame.

FRONT END ALIGNMENT

EQUIPMENT REQUIRED

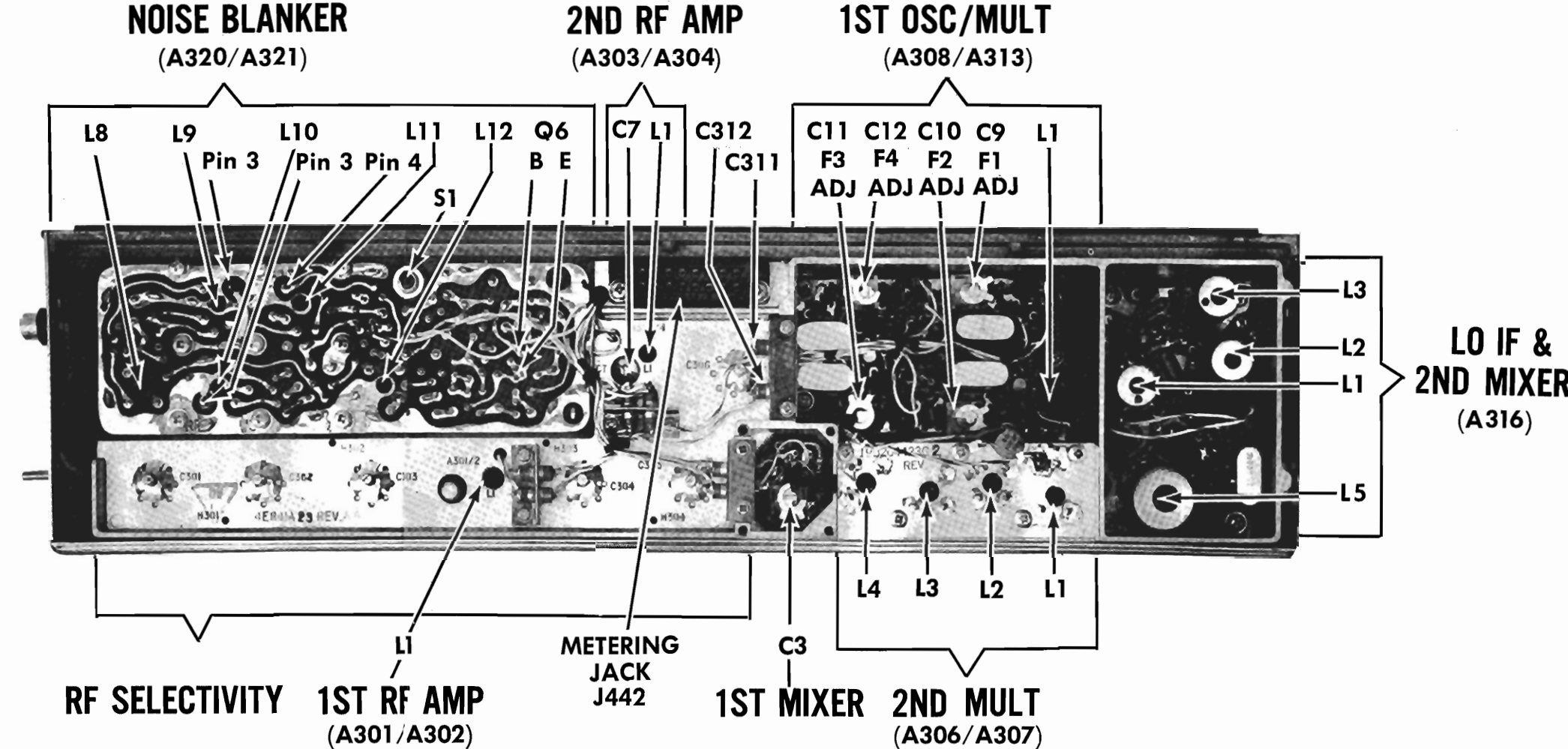
1. G-E Test Set Model 4EX3A10 (or 20,000 ohms-per-volt multimeter).
2. A 132-174 MC signal source. Connect a one-inch piece of insulated wire no larger than .065 inch to generator output probe.

PRELIMINARY CHECKS AND ADJUSTMENTS

1. Connect Test Set Model 4EX3A10 to receiver centralized metering jack J442 and set meter sensitivity switch to the TEST 1 position.
2. With VOLUME control full counterclockwise and Test Set in position G, adjust R47 on IF-AUDIO & SQUELCH BOARD for reading of 0.65 volts. If using Multimeter, connect leads to J442-1 (AUDIO-PA) and J442-8 (System Negative).
3. With Test Set in position J, check for regulated +10 volts. If using Multimeter, measure from C311 to C312.
4. If using Multimeter, connect the positive lead to J442-16 (ground).
5. Disable the Channel Guard.

ALIGNMENT PROCEDURE

STEP	METERING POSITION		TUNING CONTROL	METER READING	PROCEDURE
	4EX3A10	Multimeter - at J442			
OSCILLATOR AND MULTIPLIERS					
1.	D (MULT-1)	Pin 4	L1 (on 1st OSC/MULT) and L1 (on 2nd MULT)	See Procedure	Tune L1 (1st OSC/MULT) for maximum meter reading. Then tune L1 (2nd MULT) for minimum meter reading.
2.	E (MULT-2)	Pin 5	L1 (on 1st OSC/MULT) and L1 (on 2nd MULT)	Maximum	Tune L1 (1st OSC/MULT) and L1 (2nd MULT) for maximum meter reading.
3.	A (DISC)	Pin 10		Zero	Apply an on-frequency signal into Hole 304. Adjust the signal generator for discriminator zero.
4.	B (2nd IF AMP)	Pin 2	L2, L3 and L4 (on 2nd MULT)	Maximum	Apply an on-frequency signal as above. Tune L2, L3 and L4 for maximum meter reading, keeping signal below saturation.
RF AMPLIFIER					
5.	B (2nd IF AMP)	Pin 2	L1 (on 1st RF AMP) C301, C302, C303, C304 and C305	Maximum	Apply an on-frequency signal to the antenna jack. Tune C301 through C305 and L1 for maximum meter reading, keeping signal below saturation.
FREQUENCY ADJUSTMENT					
6.	A (DISC)	Pin 10	C9 on 1st OSC/MULT (C10, C11 and C12 for multi-frequency	Zero	Apply an on-frequency signal to the antenna jack. Tune C9 for zero discriminator reading. In multi-frequency units, tune C10, C11 and C12 as required.



TEST PROCEDURES

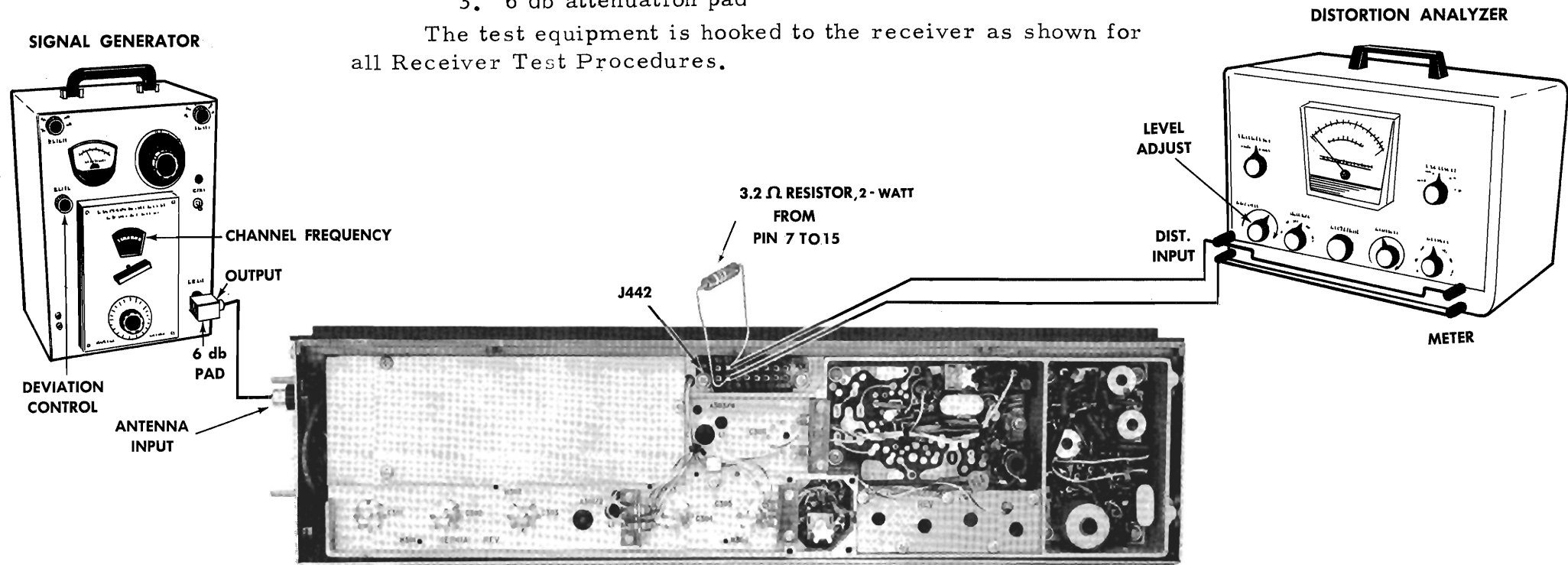
These Test Procedures are designed to help you to service a receiver that is operating---but not properly. The problems encountered could be low power, poor sensitivity, distortion, limiter not operating properly, and low gain. By following the sequence of test steps starting with Step 1, the defect can be quickly localized. Once the defective stage is pin-pointed, refer to the "Service Check" listed to correct the problem. Additional corrective measures are included in the Troubleshooting Procedure. Before starting with the Receiver Test Procedures, be sure the receiver is tuned and aligned to the proper operating frequency.

TEST EQUIPMENT REQUIRED

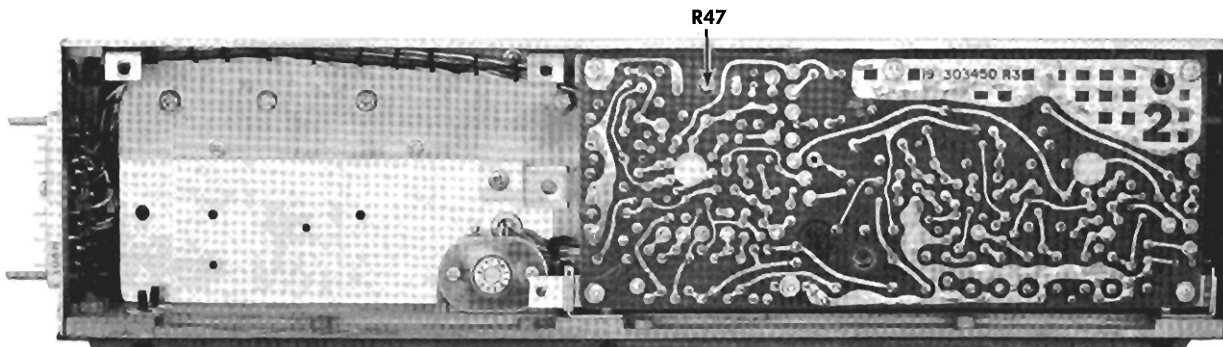
for test hookup shown:

- 1. Distortion Analyzer similar to: Heath # 1M-12
- 2. Signal Generator similar to: Measurements # M-560
- 3. 6 db attenuation pad

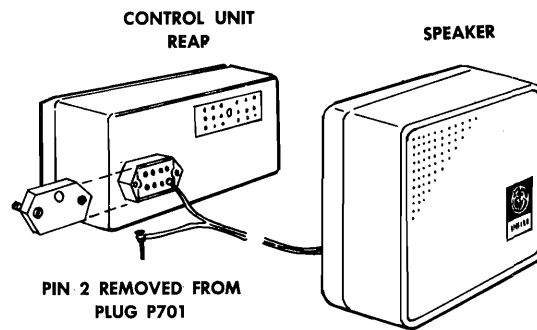
The test equipment is hooked to the receiver as shown for all Receiver Test Procedures.



COMPONENT TOP VIEW



COMPONENT BOARD WIRING VIEW



STEP 1

AUDIO POWER OUTPUT AND DISTORTION

TEST PROCEDURE

Measure Audio Power Output as follows:

- 1. Connect a 1,000-microvolt test signal modulated by 1,000 cycles ± 3.3 KC deviation to the antenna jack J441.
- 2. Two-Watt Speaker: When speaker is used, disconnect speaker lead pin from J701-2 (on rear of Control Unit). Hook up a 3.2-ohm load resistor from J442-15 to J442-7

OR

Handset:

When handset is used, lift handset off of hookswitch.

- 3. Two-Watt Speaker: Connect Distortion Analyzer input across the 3.2-ohm resistor as shown

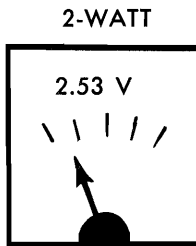
OR

Handset:

Connect Distortion Analyzer input from J442-15 to J442-7.

- 4. Two-watt speaker--set volume control for two-watt output (2.53 VRMS):

VOLTMETER SCALE ON DISTORTION ANALYZER



- 5. Make distortion measurements according to manufacturer's instructions. Reading should be less than 10% (5% is typical).

SERVICE CHECK

If the distortion is more than 10%, or maximum audio output is less than two watts (for two-watt speaker) make the following checks:

- 1. Battery and regulator voltage---low voltage will cause distortion. (Refer to Receiver Schematic Diagram for voltages.)
- 2. Audio Bias Adjust (R47)---should be adjusted for 0.65 volts. (Refer to Receiver Alignment on reverse side of page).
- 3. Audio Gain (Refer to Receiver Troubleshooting Procedure).
- 4. Discriminator Alignment (Refer to Receiver Alignment on reverse side of page).

STEP 2

USABLE SENSITIVITY (12 db SINAD)

TEST PROCEDURE

Measure sensitivity of the receiver modulated at the standard test modulation as follows:

- 1. Be sure Test Step 1 checks out properly.

- 2. Reduce the Signal Generator output from setting in Test Step 1.
- 3. Adjust Distortion Analyzer LEVEL control for a +2 db reading.
- 4. Set CONTROL from LEVEL to DISTORTION reading. Repeat Steps 1, 2 and 3 until difference in reading is 12 db (+2 db to -10 db).
- 5. The 12-db difference (Signal plus Noise and Distortion to noise plus distortion ratio) is the "usable" sensitivity level. Reading should be less than 0.35 microvolts with audio output at least one watt (1.83 volts RMS across the 3.2-ohm receiver load).

SERVICE CHECK

If the sensitivity level is more than 0.35 microvolts, make the following checks:

- 1. Alignment of RF stages (Refer to RF Alignment in Receiver Alignment on reverse side of page.)
- 2. Gain measurements as shown on the Receiver Troubleshooting Procedure.

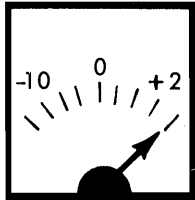
STEP 3

MODULATION ACCEPTANCE BANDWIDTH (IF BANDWIDTH)

TEST PROCEDURE

- 1. Be sure Test Steps 1 and 2 check out properly.
- 2. Set Signal Generator output for twice the microvolt reading obtained in Test Step 2 - 4.
- 3. Increase Signal Generator frequency deviation.
- 4. Adjust LEVEL Control for +2 db.

DB SCALE ON DISTORTION ANALYZER



- 5. Set CONTROL from LEVEL to DISTORTION reading. Repeat Steps 3, 4 and 5 until difference between readings becomes 12 db (from +2 db to -10 db).

LEVEL DISTORTION ON DISTORTION ANALYZER



- 6. Deviation control reading for the 12-db difference is the Modulation Acceptance Bandwidth of the receiver. It should be more than ± 6 KC (but less than ± 9 KC).

SERVICE CHECK

If the Modulation Acceptance Bandwidth test does not indicate the proper width, check the following:

- 1. Make gain measurements as shown on the Receiver Troubleshooting Procedure.
- 2. Voltage reading of Limiter (Q4) should read 0.4 volts RMS with a one-microvolt input signal on Test Set Meter or 0.9 volts with voltmeter. (Measure at J442-2).

STEP 1 - QUICK CHECKS

SYMPTOM	PROCEDURE
NO SUPPLY VOLTAGE	Check power connections and continuity of supply leads, and check fuse in power supply. If fuse is blown, check receiver for short circuits.
NO REGULATED 10 VOLTS	Check the 12-volt supply. Then check regulator circuit (See Troubleshooting Procedure for Power Supply).
LOW 2ND LIM READING	Check supply voltages and then check oscillator reading at J442-4 as shown in STEP 2. Make SIMPLIFIED VTVM GAIN CHECKS from 2nd Mixer through 2nd Limiter stages as shown in STEP 2.
LOW OSCILLATOR READING	Check alignment of Oscillator (Refer to Front End Alignment Procedure). Check voltage and resistance reading of 1st Oscillator/Multiplier Q1/Q2. Check crystal Y1.
LOW RECEIVER SENSITIVITY	Check Front End Alignment (Refer to Receiver Alignment Procedure). Check antenna connections, cable and relay. Check voltage and resistance readings of RF Amp and 1st and 2nd Mixers. Make SIMPLIFIED GAIN CHECKS (STEP 2).
LOW AUDIO	Check Audio PA (Q341) output current at J442-1. If reading is low-- a. Check BIAS ADJ for 0.65 VDC at J442-1 and -8 (STEP 2). b. Check Q341. Check unsquelched voltage readings in Audio section (Refer to Receiver Schematic Diagram). Check voltage and resistance readings on Channel Guard receiver.
IMPROPER SQUELCH OPERATION	Check voltage and resistance readings of Squelch circuit (Refer to Receiver Schematic Diagram).
DISCRIMINATOR IDLING TOO FAR OFF ZERO	See if discriminator zero is on 455 KC.

STEP 3- VOLTAGE RATIO READINGS

EQUIPMENT REQUIRED:

- RF VOLTMETER (SIMILIAR TO BOONTON MODEL 91-CA OR MILLIVAC TYPE MV-18 C.
- SIGNAL ON RECEIREE FREQUENCY (BELOW SATURATION). CORRECT FREQUENCY CAN BE DETERMINED BY ZEROING THE DISCRIMINATOR. USE 1,000 CYCLE SIGNAL WITH 2.3 KC DEVIATION FOR AUDIO STAGE.

PROCEDURE:

- APPLY PROBE TO INPUT OF STAGE (FOR EXAMPLE, BASE OF RF AMP). PEAK RESONANT CIRCUIT OF STAGE BEING MEASURED AND TAKE VOLTAGE READING (E₁).
- MOVE PROBE TO INPUT OF FOLLOWING STAGE (1ST MIXER*). REPEAK FIRST RESONANT CIRCUIT THEN PEAK CIRCUIT BEING MEASURED AND TAKE READING (E₂).
- CONVERT READINGS BY MEANS OF THE FOLLOWING FORMULA.

VOLTAGE RATIO = $\frac{E_2}{E_1}$

- CHECK RESULTS WITH TYPICAL VOLTAGE RATIOS SHOWN ON DIAGRAM.
- * NOTE: ON 1ST MIXER, REMOVE CRYSTAL BEFORE MEASURING BASE VOLTAGE. REPLACE CRYSTAL TO MEASURE COLLECTOR VOLTAGE.
ON 2ND MIXER, INCREASE SIGNAL INPUT TO APPROX. 0.3 V TO OVERRIDE INJECTION VOLTAGE.

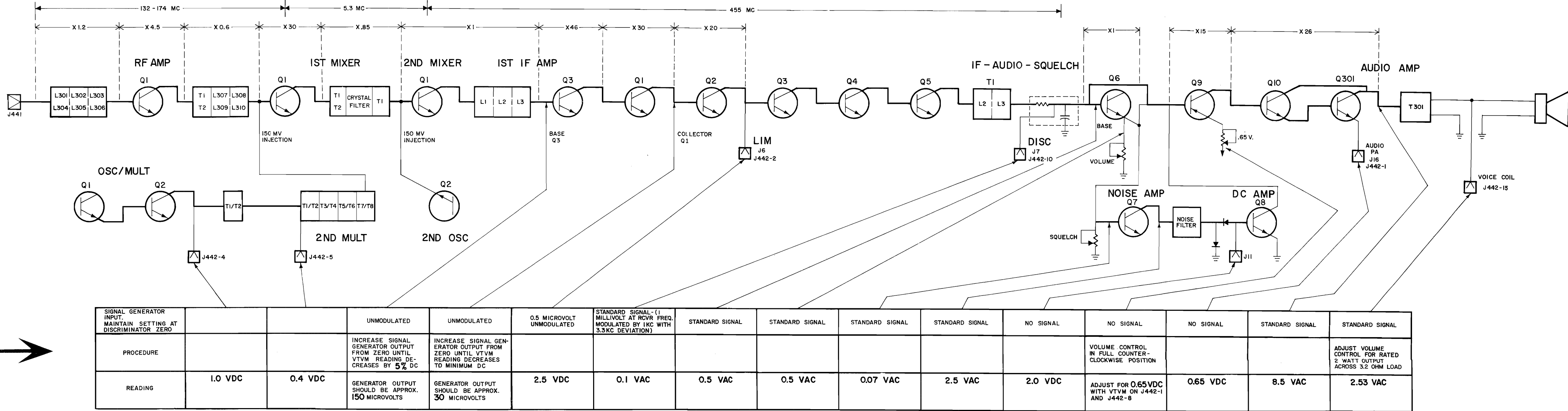
STEP 2- SIMPLIFIED VTVM GAIN CHECKS

EQUIPMENT REQUIRED:

- VTVM-AC & DC
- SIGNAL GENERATOR (MEASUREMENTS M560 EQUIV.)

PRELIMINARY STEPS:

- SET VOLUME CONTROL FULLY CLOCKWISE.
- SET SQUELCH CONTROL FULLY COUNTERCLOCKWISE.
- RECEIVER SHOULD BE PROPERLY ALIGNED.
- CONNECT SIGNAL GENERATOR TO ANTENNA JACK.
- VTVM CONNECTS BETWEEN GROUND AND POINTS INDICATED BY ARROWS.

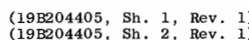


RC-1218

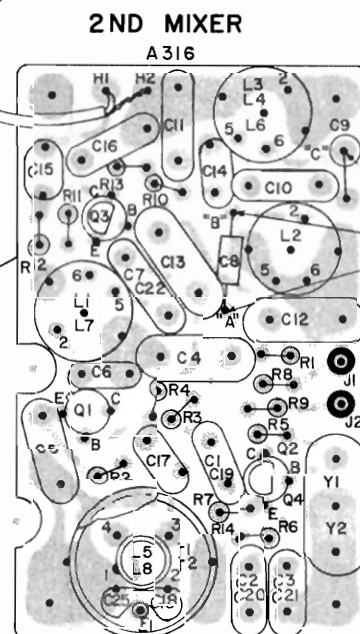
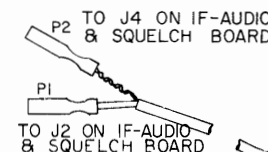
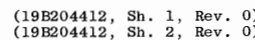
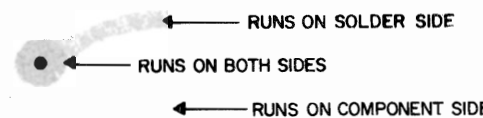
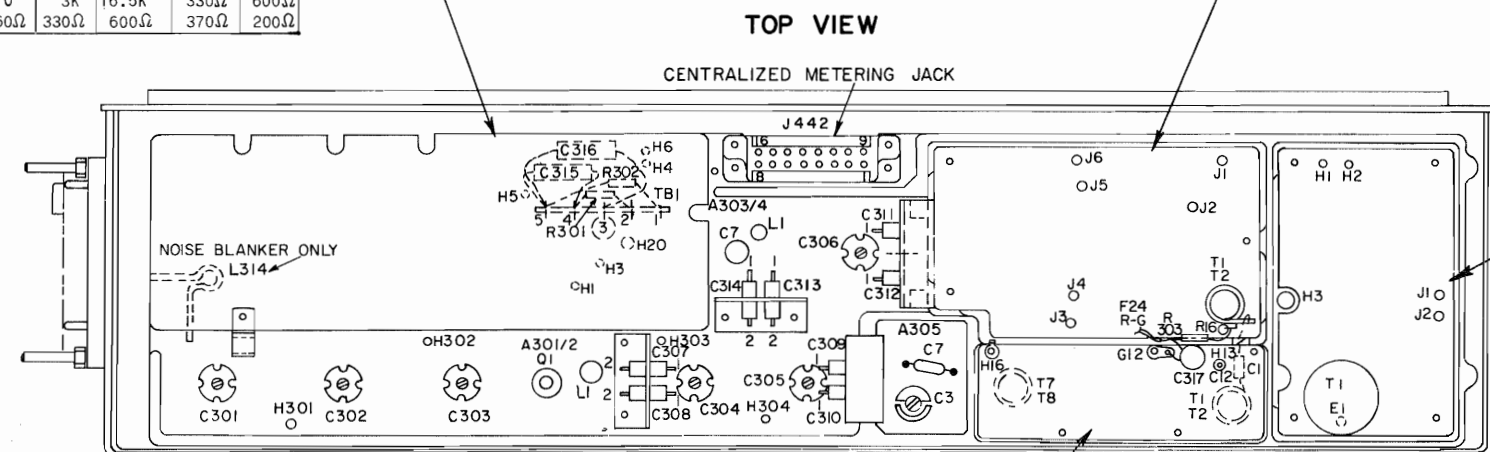
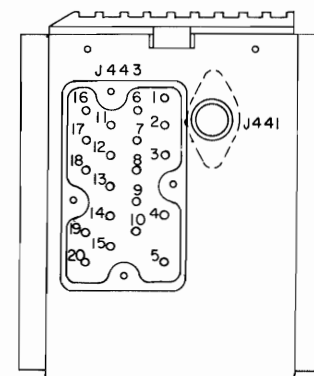
TROUBLESHOOTING PROCEDURE

132 — 174 MC, MASTR RECEIVER
MODELS 4ER41A10-45

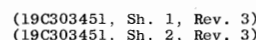
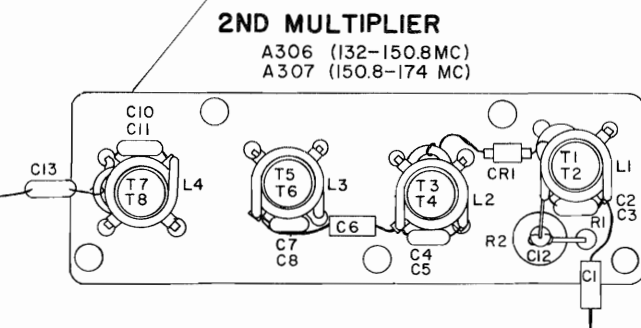
13 — 174 MC, MASTR RECEIVER
MODELS 4ER41A10-45



TRANSISTOR	EMITTER		BASE		COLLECTOR	
	—	+	—	+	—	+
A320/321						
Q1	200Ω	360Ω	1.6K	360Ω	360Ω	500Ω
Q2	100Ω	360Ω	1.5K	65Ω	30Ω	30Ω
Q3	200Ω	360Ω	1.6K	360Ω	360Ω	500Ω
Q4	100Ω	100Ω	11K	2.6K	5K	6K
Q5	1K	1K	3.3K	75K	3.3K	3.3K
Q6	0	0	3K	16.5K	330Ω	600Ω
Q7	41Ω	260Ω	30Ω	600Ω	370Ω	200Ω

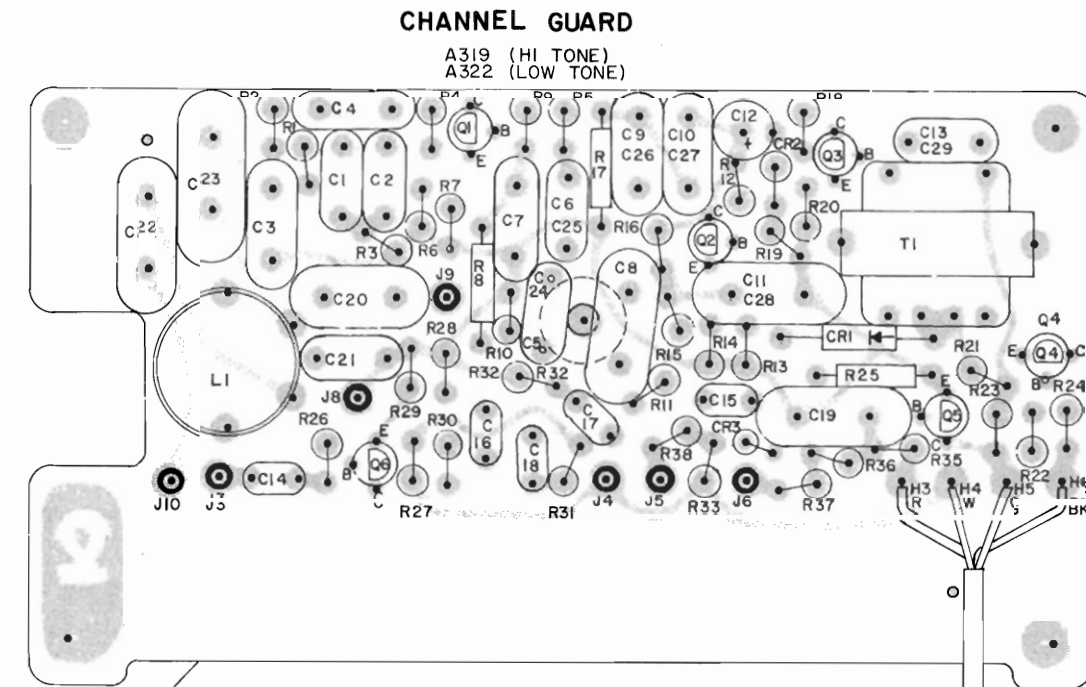
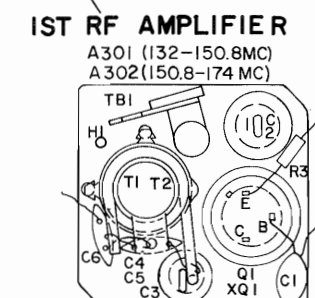
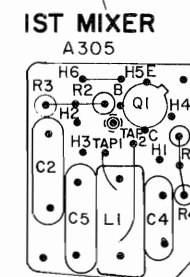
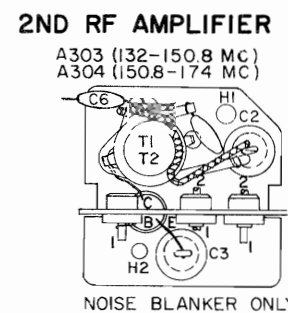
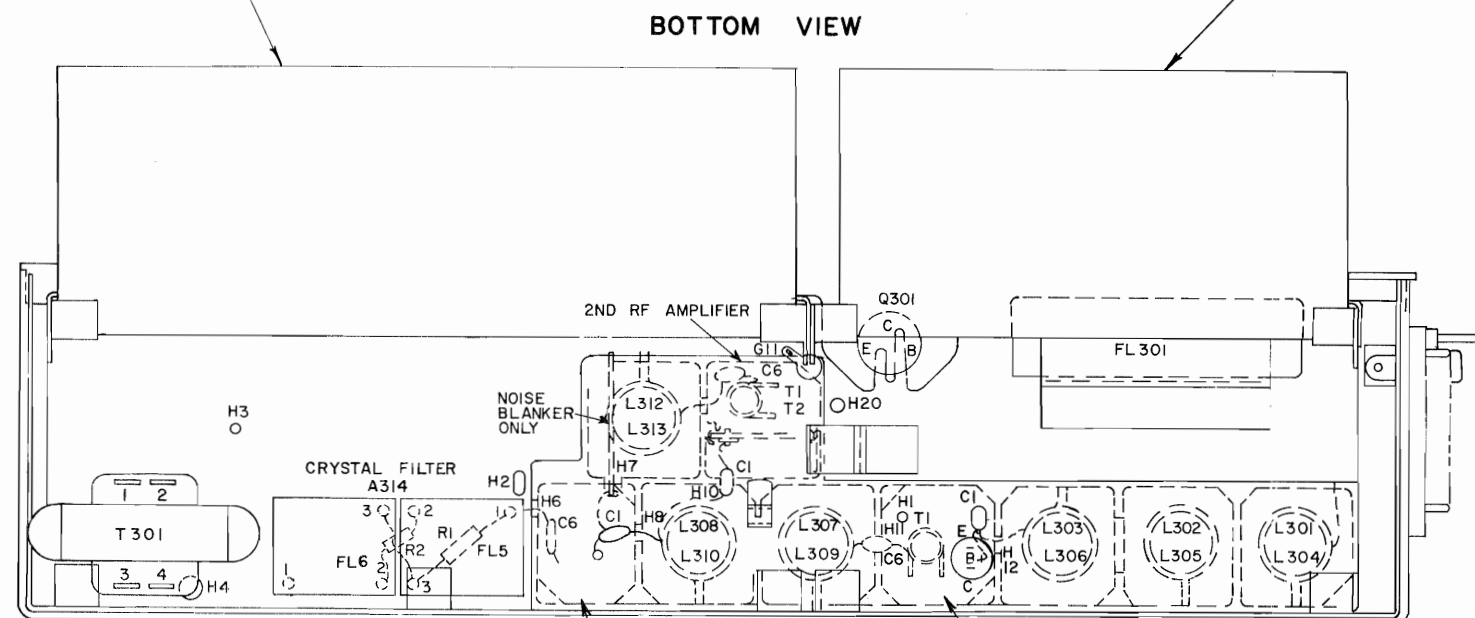


(19B204436, Sh. 1, Rev. 1)
(19B204436, Sh. 2, Rev. 1)



TRANS/STOR	EMITTER		BASE		COLLECTOR	
	\rightarrow	\leftarrow	\rightarrow	\leftarrow	\rightarrow	\leftarrow
A308/313-Q1	1K	1K	6.5K	2.8K	100 Ω	100 Ω
A308/313-Q2	70 Ω	15K	1K	160 Ω		
A305-Q1	2.7K	2.7K	7.5K	3.8K	1.6K	1.6K
A301/302-Q1	290 Ω	270 Ω	240 Ω	240 Ω	100 Ω	100 Ω
A316-Q1	3.8K	5.3K	2.5K	2.9K	200 Ω	200 Ω
A316-Q2	2.7K	6.8K	5.5K	2.7K	200 Ω	200 Ω
A316-Q3	2.2K	2.3K	2.3K	2.2K	2.7K	3.2K
A317-Q1	1K	2K	13.5K	4.1K	4.1K	5.2K
A317-Q2	2.1K	2K	13.5K	4.1K	4.1K	5.2K
A317-Q3	2.1K	2K	13.5K	4.1K	4.1K	5.2K
A317-Q4	1K	1K	13.5K	4.1K	4.1K	5.2K
A317-Q5	1.0K	10K	13.5K	2.8K	350 Ω	
A317-Q6	3.2K \times 2	MEG	36.0K	2.5K	0	0
A317-Q7	1.7K	1.7K	11.0K	4.0K	7.0K	16K
A317-Q8	180 Ω	180 Ω	100K	2.8K	11.0K	14K
A317-Q9	2.2K	2.2K	4.1K	45K	2.3K	2.3K
A317-Q10	40 Ω	35 Ω	2.3K	2.3K	40 Ω	36 Ω
A301-Q301	1 Ω	1 Ω	40 Ω	35 Ω	40 Ω	36 Ω

* READINGS MAY VARY DUE TO DIFFERENCES
IN TRANSISTORS.



(19B204553, Sh. 1, Rev. 2)
(19B204553, Sh. 2, Rev. 2)

TRANSISTOR	EMITTER		BASE		COLLECTOR	
	—	+	—	+	—	+
A319/322						
Q1	56Ω	56Ω	8.3K	145Ω	6.5K	8.3K
Q2	270Ω	270Ω	8K	500Ω	5K	5.5K
Q3	1K	1K	75K	3K	1K	1K
Q4	0	0	14K	45Ω	1K	1K
Q5	0	0	14K	45Ω	1K	1K
Q6	20Ω	20Ω	4.5K	85Ω	2K	2K

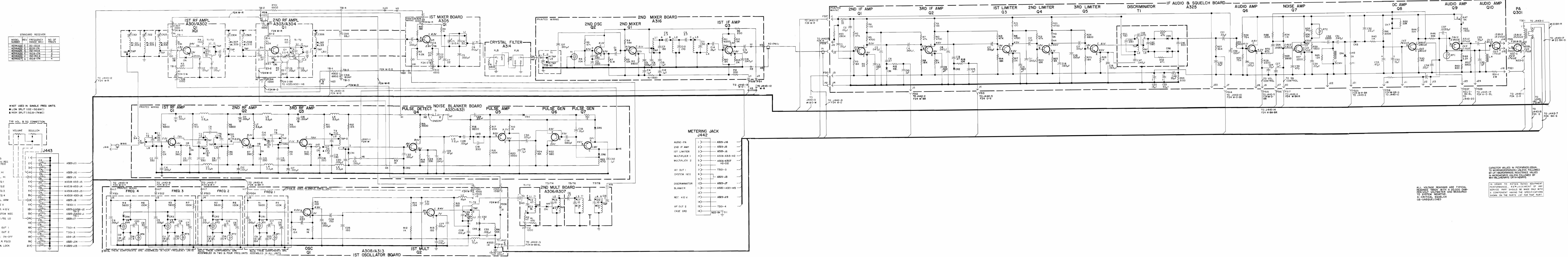
RESISTANCE READINGS

ALL READINGS ARE TYPICAL READINGS MEASURED WITH A 20,000 OHM-PER-VOLT METER, AND WITH CONTROL CABLE DISCONNECTED (OR IN STATIONS, PLUG TO J443 DISCONNECTED). READINGS ARE MADE WITH A SHORTING JUMPER CONNECTED FROM C311-1 (+12V) TO C112-1 (-12), AND ARE MEASURED FROM TRANSISTOR PINS TO C311-1, +OR - SIGNS SHOW METER LEAD TO C311-1.

- CAUTION -

ALWAYS REMOVE THE SHORTING JUMPER AFTER MAKING RESISTANCE READINGS. APPLYING POWER WITH THE SHORTING JUMPER CONNECTED MAY DAMAGE THE UNIT

FOR READINGS OF:	USE SCALE:
1-100 Ω	X 1
100-1K Ω	X 10
1K-50K Ω	X 1,000
50K Ω	X 100,000



SCHEMATIC DIAGRAM

132 — 174 MC RECEIVER
 MODELS 4ER41A22-27
 (WITH NOISE BLANKER)

[illegible]

(CONT'D FROM PAGE 14) (LBI-3584)

SYMBOL	G-E PART NO	DESCRIPTION
T3 and T4		----- SUBASSEMBLIES(Cont'd) -----
		----- TRANSFORMERS(Cont'd) -----
		COIL ASSEMBLY
	T3 PL-19B204425-G1 (4ER41A22, 24, 26) T4 PL-19B204425-G2 (4ER41A23, 25, 27)	
C6	5496218-P48	----- CAPACITORS -----
		Ceramic disc: temp-comp, radial leads, 24 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A22, 24 and 26).
	C7 7489162-P39	Silver mica, dipped phen: radial leads, 330 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
	C37 5496218-P44	Ceramic disc: temp-comp, radial leads, 15 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A23, 25 and 27).
L9	PL-19A121755-G1	----- INDUCTORS -----
		Coil.
		----- MISCELLANEOUS -----
	5491798-P5	Tuning slug.
T5 and T6		COIL ASSEMBLY
	T5 PL-19B204426-G1 (4ER41A22, 24, 26) T6 PL-19B204426-G2 (4ER41A23, 25, 27)	
		----- CAPACITORS -----
	C9 7489162-P39	Silver mica, dipped phen: radial leads, 330 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C10	5496218-P48	Ceramic disc: temp-comp, radial leads, 24 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A22, 24 and 26).
	C38 5496218-P45	Ceramic disc: temp-comp, radial leads, 18 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A23, 25 and 27).
		----- INDUCTORS -----
	L10 PL-19A121750-G1	Coil.
L10		----- MISCELLANEOUS -----
	5491798-P5	Tuning slug.
T7 and T8		COIL ASSEMBLY
	T7 PL-19B204427-G1 (4ER41A22, 24, 26) T8 PL-19B204427-G2 (4ER41A23, 25, 27)	
		----- CAPACITORS -----
	C15 7489162-P39	Silver mica, dipped phen: radial leads, 330 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C26	5496218-P46	Ceramic disc: temp-comp, radial leads, 20 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A22, 24 and 26).
		Mylar® dielectric, dipped phen: radial leads, .022 µf ±20%, 200 VDCW.
	C39 5496218-P44	Ceramic disc: temp-comp, radial leads, 15 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A23, 25 and 27).
		----- INDUCTORS -----
L11	PL-19A121752-G1	Coil.
		----- MISCELLANEOUS -----
	5491798-P5	Tuning slug.

SYMBOL	G-E PART NO	DESCRIPTION
T9 and T10		----- SUBASSEMBLIES(Cont'd) -----
		----- TRANSFORMERS(Cont'd) -----
		COIL ASSEMBLY
	T9 PL-19B204428-G1 (4ER41A22, 24, 26) T10 PL-19B204428-G2 (4ER41A23, 25, 27)	
C19	7489162-P39	----- CAPACITORS -----
		Silver mica, dipped phen: radial leads, 330 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
	C27 5496218-P47	Ceramic disc: temp-comp, radial leads, 22 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A22, 24 and 26).
	C40 5496218-P44	Ceramic disc: temp-comp, radial leads, 15 pf ±5%, 500 VDCW, temp coef 0 PPM. (Used in Models 4ER41A23, 25 and 27).
L12	PL-19A121751-G1	----- INDUCTORS -----
		Coil.
	L13 19A121104-P1	Coil.
	5491798-P5	----- MISCELLANEOUS -----
A325		Tuning slug.
		IF/AUDIO ASSEMBLY
		PL-19D402327-G7
		----- CAPACITORS -----
C1	19A115028-P116	Mylar® dielectric, dipped phen: radial leads, 0.22 µf ±20%, 200 VDCW.
	C2	
	C3 19A115028-P111	Mylar® dielectric, dipped phen: radial leads, .047 µf ±20%, 200 VDCW.
	C4 5494481-P112	Ceramic disc: radial leads, .001 µf ±10%, 500 VDCW; sim to RMC Type JF Discap.
C5	19A115028-P109	Mylar® dielectric, dipped phen: radial leads, .022 µf ±20%, 200 VDCW.
	C6 19A115028-P111	Mylar® dielectric, dipped phen: radial leads, .047 µf ±20%, 200 VDCW.
	C7 5494481-P112	Ceramic disc: radial leads, .001 µf ±10%, 500 VDCW; sim to RMC Type JF Discap.
	C8 5496218-P717	Ceramic disc: temp-comp, radial leads, 47 pf ±10%, 500 VDCW, temp coef -750 PPM.
C9	19A115028-P109	Mylar® dielectric, dipped phen: radial leads, .022 µf ±20%, 200 VDCW.
	C10 19A115028-P114	Mylar® dielectric, dipped phen: radial leads, 0.1 µf ±20%, 100 VDCW.
	C11 19A115028-P111	Mylar® dielectric, dipped phen: radial leads, .047 µf ±20%, 200 VDCW.
	C12 5494481-P112	Ceramic disc: radial leads, .001 µf ±10%, 500 VDCW; sim to RMC Type JF Discap.
C13	5496218-P717	Ceramic disc: temp-comp, radial leads, 47 pf ±10%, 500 VDCW, temp coef -750 PPM.
	C14 19A115028-P109	Mylar® dielectric, dipped phen: radial leads, .022 µf ±20%, 200 VDCW.
	C15 19A115028-P114	Mylar® dielectric, dipped phen: radial leads, 0.1 µf ±20%, 200 VDCW.
	C16 5496219-P421	Ceramic disc: temp-comp, radial leads, 100 pf ±10%, 500 VDCW, temp coef -220 PPM.
C17	5494481-P112	Ceramic disc: radial leads, .001 µf ±10%, 500 VDCW; sim to RMC Type JF Discap.
	C18 and C19 19A115028-P109	Mylar® dielectric, dipped phen: radial leads, .022 µf ±20%, 200 VDCW.
	C20 5496267-P14	Tubular, hermetically sealed, tantalum, dry solid: axial leads, 15 µf ±20%, 20 VDCW; sim to Sprague 150D156X0020B2.

SYMBOL	G-E PART NO	DESCRIPTION
C21	19B209243-P9	----- SUBASSEMBLIES(Cont'd) -----
		----- CAPACITORS(Cont'd) -----
	C22 19A115028-P107	Polyester dielectric: radial leads, 0.22 µf ±20%, 40 VDCW; sim to AmpereX C280AA/P220K.
	C23 5491000-P1	Mylar® dielectric, dipped phen: radial leads, .01 µf ±20%, 200 VDCW.
C24	19A115028-P107	Tubular, hermetically sealed, electrolytic: axial leads, 30 µf +75% -10%, 25 VDCW; sim to Sprague S45553.
		Mylar® dielectric, dipped phen: radial leads, .01 µf ±20%, 200 VDCW.
	C25 5494481-P112	Ceramic disc: radial leads, .001 µf ±10%, 500 VDCW; sim to RMC Type JF Discap.
	C27 19B209243-P7	Polyester dielectric: radial leads, 0.1 µf ±20%, 40 VDCW; sim to AmpereX C280AA/P100K.
C28	5496267-P17	Tubular, hermetically sealed, tantalum, dry solid: axial leads, 1 µf ±20%, 35 VDCW; sim to Sprague 150D105X0035A2.
	C29 19B209243-P9	Polyester dielectric: radial leads, 0.22 µf ±20%, 40 VDCW; sim to AmpereX C280AA/P220K.
	C31 19B209243-P5	Polyester dielectric: radial leads, .047 µf ±20%, 40 VDCW; sim to AmpereX C280AA/P47K.
	C32 19B209243-P9	Polyester dielectric: radial leads, 0.22 µf ±20%, 40 VDCW; sim to AmpereX C280AA/P220K.
C33	5496267-P28	Tubular, hermetically sealed, tantalum, dry solid: axial leads, 0.47 µf ±20%, 35 VDCW; sim to Sprague 150D474X0035A2.
	C34 19B209243-P9	Polyester dielectric: radial leads, 0.22 µf ±20%, 40 VDCW; sim to AmpereX C280AA/P220K.
	C35 5496267-P6	Tubular, hermetically sealed, tantalum, dry solid: axial leads, 33 µf ±20%, 10 VDCW; sim to Sprague 150D336X0010B2.
	C37 19A115028-P303	Mylar® dielectric, dipped phen: radial leads, .0033 µf ±10%, 200 VDCW.
C38	5495670-P10	Tubular, hermetically sealed, electrolytic: axial leads, 100 µf +75% -10%, 15 VDCW; sim to Sprague 30D172A1.
	C39 5490008-P143	Silver mica, dipped phen: radial leads, 470 pf ±10%, 300 VDCW; sim to Electro Motive Type DM-15.
	C48 5495670-P9	Tubular, hermetically sealed, electrolytic: axial leads, 35 µf +75% -10%, 15 VDCW; sim to Sprague 30D169A1.
	C50 5496267-P14	Tubular, hermetically sealed, tantalum, dry solid: axial leads, 15 µf ±20%, 20 VDCW; sim to Sprague 150D156X0020B2.
C52	4029003-P16	Silver mica, dipped phen: radial leads, .0022 µf ±5%, 500 VDCW; sim to Electro Motive Type DM-20.
	C53 5491189-P106	Mylar® dielectric, dipped epoxy: radial leads, 0.1 µf ±20%, 50 VDCW; sim to Good-All Type 601PE.
	C54 7491930-P3	Tubular, Mylar® dielectric: axial leads, .0047 µf ±20%, 100 VDCW; sim to G-E Type 61F.
		----- DIODES AND RECTIFIERS -----
C61 and C62	7777146-P3	Germanium; sim to Type 1N90.
	C63 and C64 19A11250-P1	Silicon.
	CR7 19A11250-P1	Silicon.
		----- JACKS AND RECEPTACLES -----
J1 thru J24	4033513-P4	Contact, electrical: sim to Bead Chain L93-3.
		----- INDUCTORS -----
	L1 PL-4031476-G1	Choke. Includes:
	7773023-P25	Tuning slug.

SYMBOL	G-E PART NO	DESCRIPTION
L4	5491736-P6	----- SUBASSEMBLIES(Cont'd) -----
		----- INDUCTORS(Cont'd) -----
		Choke: 3.5 mh ±10% ind at 1 KC, 2.5 ohms DC res max; sim to Aladdin 33-494.
		----- TRANSISTORS -----
Q1 thru Q8	19A115123-P1	Silicon, NPN; sim to Type 2N2712.
	Q9 19A115247-P1	Silicon, PNP; sim to Type 2N1024.
	Q10 19A115300-P1	Silicon, NPN; sim to Type 2N3053.
		----- RESISTORS -----
R1	3R77-P330K	Fixed composition: 33 ohms ±10%, 1/2 w.
	R2 3R77-P473K	Fixed composition: 47,000 ohms ±10%, 1/2 w.
	R3 3R77-P183J	Fixed composition: 18,000 ohms ±5%, 1/2 w.
	R4 3R77-P101K	Fixed composition: 100 ohms ±10%, 1/2 w.
R5	3R77-P472K	Fixed composition: 4700 ohms ±10%, 1/2 w.
	R6 3R77-P202J	Fixed composition: 2000 ohms ±5%, 1/2 w.
	R7 3R77-P473K	Fixed composition: 47,000 ohms ±10%, 1/2 w.
	R8 3R77-P183J	Fixed composition: 18,000 ohms ±5%, 1/2 w.
R9	3R77-P101K	Fixed composition: 100 ohms ±10%, 1/2 w.
	R10 3R77-P472K	Fixed composition: 4700 ohms ±10%, 1/2 w.
	R11 3R77-P202J	Fixed composition: 2000 ohms ±5%, 1/2 w.
	R12 3R77-P103K	Fixed composition: 10,000 ohms ±10%, 1/2 w.
R13	3R77-P473K	Fixed composition: 47,000 ohms ±10%, 1/2 w.
	R14 3R77-P183J	Fixed composition: 18,000 ohms ±5%, 1/2 w.
	R15 3R77-P101K	Fixed composition: 100 ohms ±10%, 1/2 w.
	R16 3R77-P472K	Fixed composition: 4700 ohms ±10%, 1/2 w.
R17	3R77-P202J	Fixed composition: 2000 ohms ±5%, 1/2 w.
	R18 3R77-P103K	Fixed composition: 10,000 ohms ±10%, 1/2 w.
	R19 3R77-P473K	Fixed composition: 47,000 ohms ±10%, 1/2 w.
	R20 3R77-P183J	Fixed composition: 18,000 ohms ±5%, 1/2 w.
R21	3R77-P472K	Fixed composition: 4700 ohms ±10%, 1/2 w.
	R23 3R77-P202J	Fixed composition: 2000 ohms ±5%, 1/2 w.
	R24 3R77-P682K	Fixed composition: 6800 ohms ±10%, 1/2 w.
	R25 3R77-P183J	Fixed composition: 18,000 ohms ±5%, 1/2 w.
R26	3R77-P102J	Fixed composition: 1000 ohms ±5%, 1/2 w.
	R27 3R77-P683K	Fixed composition: 68,000 ohms ±10%, 1/2 w.
	R28 3R77-P222J	Fixed composition: 2200 ohms ±5%, 1/2 w.
	R29 and R30 3R77-P753J	Fixed composition: 75,000 ohms ±5%, 1/2 w.
R31	3R77-P512J	Fixed composition: 5100 ohms ±5%, 1/2 w.
	R32 3R77-P102J	Fixed composition: 1000 ohms ±5%, 1/2 w.
	R34 3R77-P113K	Fixed composition: 11,000 ohms ±10%, 1/2 w.
	R36 3R77-P153K	Fixed composition: 15,000 ohms ±10%, 1/2 w.
R37	3R77-P222J	Fixed composition: 2200 ohms ±5%, 1/2 w.
	R38 3R77-P751J	Fixed composition: 750 ohms ±5%, 1/2 w.
	R39 3R77-P562J	Fixed composition: 5600 ohms ±5%, 1/2 w.
	R40 3R77-P113K	Fixed composition: 11,000 ohms ±10%, 1/2 w.
R41	3R77-P204K	Fixed composition: 0.2 megohm ±10%, 1/2 w.
	R44 3R77-P153K	Fixed composition: 15,000 ohms ±10%, 1/2 w.
	R45 3R77-P181K	Fixed composition: 180 ohms ±10%, 1/2 w.
	R46 3R77-P333K	Fixed composition: 33,000 ohms ±10%, 1/2 w.
R47	19B209115-P1	Variable, carbon film: 5000 ohms ±20%, 0.15 w, linear taper; sim to CTS Type UPE-70.

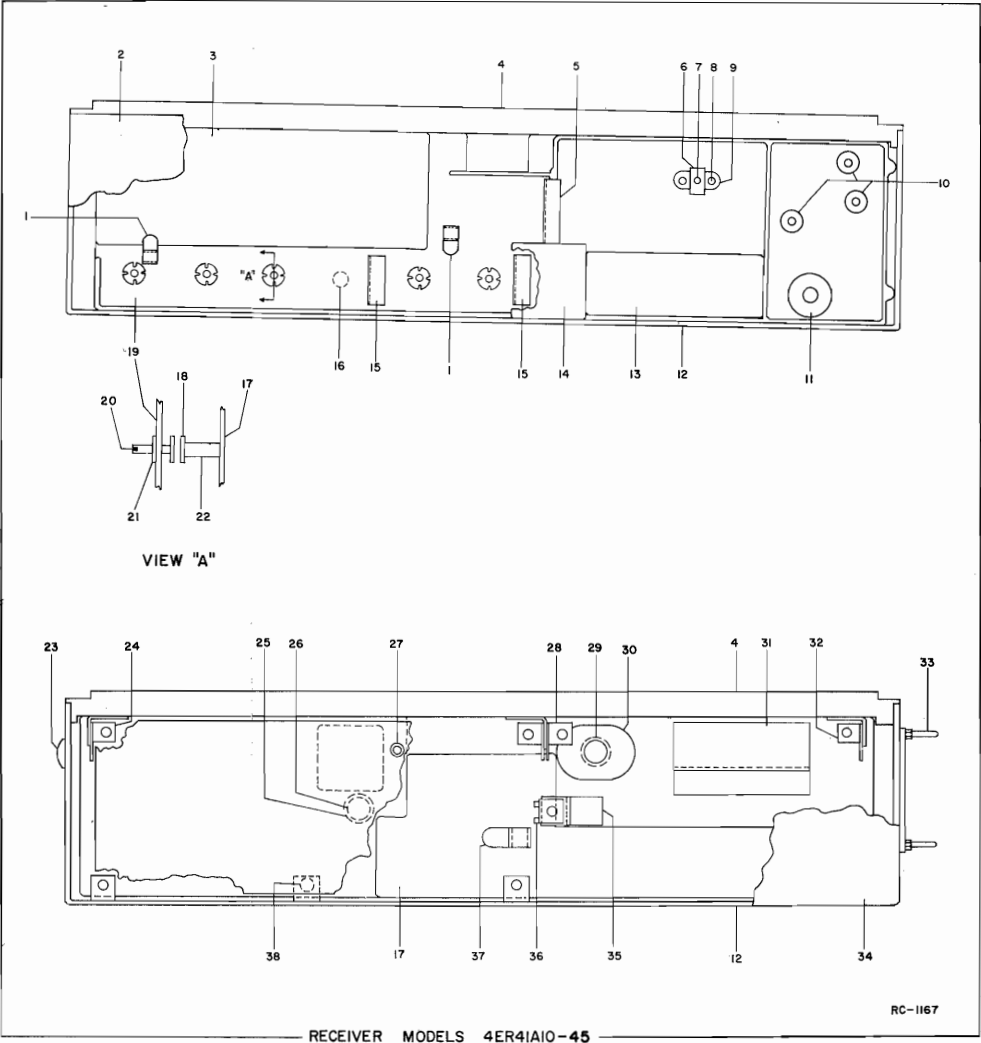
SYMBOL	G-E PART NO	DESCRIPTION
R48	3R77-P222J	----- SUBASSEMBLIES(Cont'd) -----
		----- RESISTORS(Cont'd) -----
		Fixed composition: 2200 ohms ±5%, 1/2 w.
	R49 3R77-P821K	Fixed composition: 820 ohms ±10%, 1/2 w.
R50	3R77-P392K	Fixed composition: 3900 ohms ±10%, 1/2 w.
	R51 19B209022-P15	Wirewound, phen: 1 ohm ±5%, 2 w; sim to IRC Type BWH.
	R52 3R77-P152K	Fixed composition: 1500 ohms ±10%, 1/2 w.
	R53 5495948-P444	Deposited carbon, epoxy coated: 0.28 megohm ±1%, 1/2 w; sim to Texas Instruments Type CDI/2MR.
R59	3R77-P512K	Fixed composition: 5100 ohms ±10%, 1/2 w.
	R65 3R77-P123K	Fixed composition: 12,000 ohms ±10%, 1/2 w.
	R66 3R77-P223K	Fixed composition: 22,000 ohms ±10%, 1/2 w.
	R68 3R77-P134J	Fixed composition: 0.13 megohm ±5%, 1/2 w.
R69	3R77-P392J	Fixed composition: 3900 ohms ±5%, 1/2 w.
	R70 3R77-P471J	Fixed composition: 470 ohms ±5%, 1/2 w.
		----- THERMISTORS -----
	RT1 19B209143-P2	Rod: axial leads, 4000 ohms ±10% res, 1 w max; sim to Globar Type 789F-12.
RT2	19B209143-P3	Rod: axial leads, 850 ohms ±10% res, 1 w max; sim to Globar Type 789F.
		----- TRANSFORMERS -----
		DISCRIMINATOR ASSEMBLY
		PL-19C303612-G1
C41 and C42	19B209196-P1	----- CAPACITORS -----
		Ceramic disc: temp-comp, radial leads, 280 pf ±5%, 500 VDCW, temp coef -115 ±30 PPM.
	C45 7489162-P43	Silver mica, dipped phen: radial leads, 470 pf ±5%, 300 VDCW; sim to Electro Motive Type DM-15.
	C46 7489162-P35	Silver mica, dipped phen: radial leads, 220 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C47	5491189-P4	Mylar® dielectric, dipped epoxy: radial leads, .047 µf ±20%, 50 VDCW; sim to Good-All Type 601PE.
		----- DIODES AND RECTIFIERS -----
	CR5 and CR6 19A11250-P1	Silicon.
		----- INDUCTORS -----
L2 and L3	PL-19A121532-G1	Coil.
		----- RESISTORS -----
	R56 3R152-P331J	Fixed composition: 330 ohms ±5%, 1/4 w.
	R57 and R58 3R152-P473J	Fixed composition: 47,000 ohms ±5%, 1/4 w.
		----- CAPACITORS -----
C315 and C316	5496267-P11	Tubular, hermetically sealed, tantalum, dry solid: axial leads, 68 µf ±20%, 15 VDCW; sim to Sprague 150D686X0015H2.
	C317 5494481-P12	Ceramic disc: radial leads, .001 µf ±10%, 500 VDCW; sim to RMC Type JF Discap.

(CONT'D ON PAGE 16)

SYMBOL	G-E PART NO	DESCRIPTION
J442	19B209125-P2	----- JACKS AND RECEPTACLES ----- Connector: 18 contacts rated at 5 amps min at 1000 VDC max.
J443	PL-19C303426-G1	Connector: 20 pin contacts.
P301 thru P303	4029840-P2	----- PLUGS ----- Contact, electrical: solder coated brass; sim to Amp 42827-2. (Used in Models 4ER41A24-27).
P304 thru P309	4029840-P2	Contact, electrical: solder coated brass; sim to Amp 42827-2.
P310	4029840-P1	Contact, electrical: solder coated brass; sim to Amp 41854.
P311 thru P320	4029840-P2	Contact, electrical: solder coated brass; sim to Amp 42827-2.
P321	4029840-P1	Contact, electrical: solder coated brass; sim to Amp 41854.
P325	4029840-P2	Contact, electrical: solder coated brass; sim to Amp 42827-2.
P329	4029840-P2	Contact, electrical: solder coated brass; sim to Amp 42827-2.
P337	4029840-P2	Contact, electrical: solder coated brass; sim to Amp 42827-2. (Used in Models 4ER41A24-27).
Q301	19A115527-P1	----- TRANSISTORS ----- Silicon, PNP.
R301 and R302	3R152-P681K	----- RESISTORS ----- Fixed composition: 680 ohms $\pm 10\%$, 1/4 w.
R303	3R152-P102K	Fixed composition: 1000 ohms $\pm 10\%$, 1/4 w.
T301	19B209083-P1	----- TRANSFORMERS ----- Audio freq: Pri 1: 19 ohms $\pm 10\%$ imp at 3 w, 0.866 ohm DC res max, Sec 1: 3.5 ohms $\pm 10\%$ imp at 3 w, 0.222 ohm DC res max.
TB1	7487424-P7	----- TERMINAL BOARDS ----- Miniature, phen: 4 terminals.
C301 thru C305	19B209135-P1	RF CIRCUIT ASSEMBLY PL-19C303472-G3 (4ER41A22, 24, 26) PL-19C303472-G4 (4ER41A23, 25, 27)
C307 thru C314		----- CAPACITORS ----- Refer to Mechanical Parts (RC-1167).
J441		----- JACKS AND RECEPTACLES ----- (Part of W441).
L301	PL-19B204461-G4	----- INDUCTORS ----- Coil. (Used in Models 4ER41A22, 24 and 26).
L302	19B200616-P2	Coil. (Used in Models 4ER41A22, 24 and 26).
L303	PL-19B204461-G4	Coil. (Used in Models 4ER41A22, 24 and 26).
L304	PL-19B204461-G1	Coil. (Used in Models 4ER41A23, 25 and 27).
L305	19B200616-P1	Coil. (Used in Models 4ER41A23, 25 and 27).
L306	PL-19B204461-G1	Coil. (Used in Models 4ER41A23, 25 and 27).
L307	PL-19B204461-G4	Coil. (Used in Models 4ER41A22, 24 and 26).

SYMBOL	G-E PART NO	DESCRIPTION
L308	PL-19B204461-G6	----- INDUCTORS(Cont'd) ----- Coil. (Used in Models 4ER41A22, 24 and 26).
L309	PL-19B204461-G3	Coil. (Used in Models 4ER41A23, 25 and 27).
L310	PL-19B204461-G6	Coil. (Used in Models 4ER41A23, 25 and 27).
L311	19A121385-P1	Coil.
L312	PL-19B204461-G6	Coil. (Used in Models 4ER41A22, 24 and 26).
L313	PL-19B204461-G3	Coil. (Used in Models 4ER41A23, 25 and 27).
L314	19A121289-P1	Coil.
W441	19B209122-P1	----- CABLES ----- Connector, coaxial: includes cable jack (J441), approx 5 inches long.
1	7145451-P1	MECHANICAL PARTS (SEE RC-1167) Cable clamp. (Used in Models 4ER41A24-27).
2	PL-19C303396-G4	Cover: approx 14-13/32 x 3-9/16 x 9/32 inches.
3	19B204890-P1	(Not used).
4	PL-19C303394-G2	Heat sink: approx 14-9/16 x 3-7/32 x 13/32 inches thick.
5	19A121222-P1	Angle support: approx 1-5/32 x 11/32 x 9/32 inches. (Used with C311 and C312 in PL-19C303472-G3 and 4).
6	4033089-P1	Clip. (Part of XY1-4 in A308-313).
7	19B200525-P8	Rivet. (Part of XY1-4 in A308-313).
8	4033751-P1	Electrical contact: sim to Methode 752 V (PB). (Part of XY1-4 in A308-313).
9	4039307-P1	Crystal socket. (Part of XY1-4 in A308-313).
10	4029739-P2	Can: approx 7/8 x 1/2 x 1/2 inches thick. (Part of L1-3 in A316).
11	4034252-P5	Can: approx 1-3/16 x 3/4 x 1/32 inches thick. (Part of T1 in A316).
12	PL-19C303389-G1	Chassis: approx 14-1/2 x 3-1/2 x 3-7/32 inches.
13	19B204396-P1	Support: approx 3 x 1 x 1/32 inches thick. (Used in A306 and 307).
14	19A121071-P1	Plate: approx 1-11/32 x 1-5/16 x 1/32 inches thick.
15	19A121221-P1	Angle support: approx 15/16 x 5/16 x 1/32 inches. (Used with C307-310 in PL-19C303472-G3 and 4).
16	7162414-P1	Mounting ring, transistor socket: approx 7/16 inch dia; sim to Elco 757. (Used with Q1 in A301 and 302).
17	19B204397-P1	RF plate: approx 8-5/8 x 2-5/8 x 1/32 inches thick.
18	PL-4036765-G2	Screw: approx 1/4 x 1/16 inches dia, with 6/32 threads. (Part of C301-305 in PL-19C303472-G3 and 4).
19	19C303562-P1	RF chassis: approx 13-3/4 x 3-1/4 x 1-13/16 inches. (Used in PL-19C303472-G3 and 4).
20	PL-4036765-G4	Screw: approx 9/16 x 1/16 inches dia, with 6-32 threads. (Part of C301-305 in PL-19C303472-G3 and 4).
21	7117825-P1	Spring, washer: approx 15/32 inch dia, with 6-32 threads; sim to Tinnerman C4578B-632-24. (Part of C301-305 in PL-19C303472-G3 and 4).
22	4036899-P4	Ceramic insulator: approx 1 x 3/8 inches dia; sim to Centralab 3BX845C. (Part of C301-305 in PL-19C303472-G3 and 4).
23	4033986-P6	Plug button: approx 7/16 inch dia; sim to United Car Fastener BS-48199.

SYMBOL	G-E PART NO	DESCRIPTION
24	PL-19B204583-G3	MECHANICAL PARTS(Cont'd) Hinge.
25	4035439-P1	Transistor heat sink: approx 1/4 x 1/2 inches dia; sim to Birtcher 3AL-635-2R. (Used with Q10 in A325).
26	4036555-P1	Washer insulator: nylon. (Used with Q9 and 10 in A325).
27	4035306-P11	Fiber washer: approx 1/8 x 3/16 x 1/32 inches thick. (Used with L1 in A325).
28	PL-19B204583-G1	Hinge.
29	19A121284-P1	Mica insulator: approx 11/16 inch dia. (Used with Q301).
30	19A121283-P1	Support. (Used with Q301).
31	PL-19A121229-G1	(Not used).
32	PL-19B204583-G2	(Not used).
33	19A121676-P1	Guide pin: approx 1 x 1/8 inches dia with 4-40 mounting thread.
34	PL-19C303396-G2	Cover: approx 14-9/16 x 3-7/32 x 13/32 inches.
35	19A121297-P1	Angle: approx 1-5/16 x 1 x 1/2 inches.
36	7160861-P4	Spring clip nut: sim to Tinnerman C6452-82-157.
37	4029851-P6	Cable clamp: nylon; sim to Weckesser 5/16-4.
38	19A115461-P2	Spring washer: approx 1/4 inch dia; sim to Shakeproof 3597-04-00.



PRODUCTION CHANGES

Changes in the equipment to improve performance or to simplify circuits are identified by a "Revision Letter", which is stamped after the model number of the unit. The revision stamped on the unit includes all previous revisions. Refer to the Parts List for descriptions of parts affected by these revisions.

REV. A & B - These revisions were incorporated into initial shipments.

REV. C - To minimize chance of interference, IF frequency changed from 5.26 MC to 5.30 MC Changed crystal filter A314 and A316-Y1.