# WAG-AERO FLY-BY-NIGHT RECEIVER: IN STALLATION, OPERATION, AND MAINTENANCE 



## GENERAL INFORMATION.

## Functional Description.

The Wag-Aero FBN (Fly-By-Night) Aviation Receiver was designed for operation at small airports to monitor conversations or to provide pilot control of lighting. It is tunable over a range of $118-137 \mathrm{MHz}$ in 25 kHz increments.

## Modes of Operation Available:

The FBN Receiver has a microcontroller responsible for watching what is happening on the air. It can be programmed to perform several different tasks in response. In this configuration, it is normally used for control of airport landing lights.

- Runway lights may be controlled in varying intensities by keying the microphone 3,5 , or


## Table 1. Quick Reference

Frequency range: 118-137 MHz
Channel Spacing: 25 kHz . Frequency set with dip switch; (repeaking coils required for freq change more than 2 MHz - use A28 tool)
Sensitivity ( $10 \mathrm{~dB} \mathrm{~S} / \mathrm{N}$ ): $0.2 \mu \mathrm{~V}$
Squelch Sensitivity: adjustable $0.2 \mu \mathrm{~V}$ to $5.0 \mu \mathrm{~V}$
Adjacent Channel Selectivity: 80 dB
Temp stability: $\pm 10 \mathrm{ppm}+20$ to $+30^{\circ} \mathrm{C}$; $\pm 20 \mathrm{ppm}-30$ to +50 deg C .
Audio Output: 2 Watts (8 ohms)
S-meter output: will drive external 1 mA meter
Front panel controls: volume, squelch, LED.
Control outputs: three separately controlled open-collector switching transistors able to sink up to 50 mA to ground on circuits up to 15 Vdc . External relays can be controlled for high current loads.
Antenna connector: RCA jack ( 50 ohms). Can be extended to a uhf jack on cabinet.
Power, audio, s-meter, control connections: solder terminals on pc board Operating Power: $+13.6 \mathrm{Vdc}+-10 \%$ at $75-$ 200 mA , depending on audio level. 115 Vac adapter supplied.

7 times in a 5 -second period.

- Lights remain on for a programmable period of time, usually 15 minutes.
- Various programming options allow for change in intensity after initial turn-on and flashing lights to warn of turnoff.
- Front panel LED indicates when lights have been activated at any intensity.

Other settings allow the receiver to be used simply to monitor or to watch for downed aircraft, but this manual concentrates on using it to control landing lights.

## INSTALLATION.

Following are general instructions for installation of the receiver. For proper operation and to prevent damage to the unit, it is recommended that a qualified two-way radio technician do the installation.

## Mounting.

The receiver enclosure can be mounted against any vertical surface with screws through the mounting flanges. If you want to use a simple whip antenna for localized operation, mounting the unit with the connectors up will allow you to simply attach a whip antenna to the connector.

Selecting a location for the receiver depends on several factors. It should be near the electrical circuit for the runway lights so the relay to switch the lights is close to the receiver. It should also be near an ac outlet to provide power for the receiver.

If you want to use the whip antenna, you want to select a location which allows the antenna to pick up transmissions well and not be near sources of interference such as motors or fluorescent lights. Normally, the higher the antenna, the better, and it should not be in an area enclosed by metal siding, which could restrict the range. If you cannot find a location which provides interference free rece ption with an indoor antenna, you may want to use a roof mounted antenna of some sort. A simple scanner radio antenna from Radio Shack should do the job nicely.

The speaker can be mounted wherever convenient within the distance allowed by the cable.

## Cover Removal.

If you need to remove the cover for
any reason, remove the four screws on the side of the cover, and slide it off. Do not remove screws from bottom.

## Relay Mounting.

The relay should be mounted in an electrical cabinet for safety, and it should be mounted on a metal surface for proper heatsinking. As shown in the derating curve in figure 3C, the relay may be operated with a load up to 4 Amp at room temperature with no heatsink. For operation at elevated temperatures or for load currents over 4 Amp , the relay needs to be heat sunk to a large metal surface, and a good size metal electrical cabinet should provide ample surface for that.

To provide heatsinking for the relay, it must be mounted on a bare metal surface. If necessary, an aluminum plate can be installed in the cabinet to provide bare metal for heatsinking. Before screwing the $1 \mathrm{e}-$ lay to the heatsink surface, spread a very thin layer of heatsink compound on the metal relay base to transfer the heat to the heatsink. The heatsink compound and a toothpick for applying it are provided in a small plastic bag taped to the relay for shipping.

- CAUTION: Installer is responsible to ensure that proper heatsinking is provided. Warranty does not cover damage to relay which might result from improper installation.


## Electrical Connections.

The antenna connection is made with a coaxial connector. The power, speaker, and relay connections are made with a DB9 connector. Table 2 identifies the terminals used for these connections. Figure 2 shows the terminals on the DB9 connector.

## Antenna Connections.

For normal operation, the whip antenna supplied with the unit should be sufficient to provide useful range.

## Table 2. Power, Audio, and

 Control Connections| Function | Wire | Pin |
| :--- | :---: | :---: |
| Power Ground | blk | 6 |
| Power +12Vdc | blk/wht | 1 |
| Speaker audio | spkr | 8 |
| Speaker ground | spkr | 7 |
| + Relay Input | red | 2 |
| - Relay Input (3 clicks) | orn | $3^{*}$ |
| - Relay Input (5 clicks) | - | $4^{*}$ |
| - Relay Input (7 clicks) | - | $5^{*}$ |
| Note: The orange wire is tied to pins 3, 4, |  |  |
| and 5 in the plug. See Operation. |  |  |



It should be plugged into the coaxial connector and extended to full length.

In the unlikely event that you need to use an outside antenna, it should be connected with good, low-loss 50 ohm coaxial cable plugged into the antenna connector with a suitable BNC plug.

## Power Connections.

The receiver operates on +13.6 Vdc at about 200 mA peak with full audio. An ac power adapter is provided; so all you need to do is plug it into a source of 115 Vac once the installation is completed.

If you want to operate the receiver on some other source of power, be sure to use a regulated and filtered 12 Vdc power supply and observe m larity when connecting the power supply in place of the ac adapter supplied with the unit. Operating with reverse polarity will damage the unit.

## Control Outputs.

The FBN Receiver has three output transistors used to control relays for operating the runway lights with three, five, or seven clicks of the microphone push-to-talk button. Each transistor can sink as much as 50 mA at voltages up to +15 Vdc . In other words, the transistors switch ground on and off and can be used to ground one end of a circuit. The common use is to ground one side of a relay input to energize a relay.


For this application, one relay is provided to simply turn runway lights on with three microphone clicks. The input side of the relay should be connected as shown in figure 3A, with the red wire connected to the positive input, terminal 3 , and the orange wire connected to the negative input, terminal 4. Be careful not to reverse polarity.

## Runway Light Connections.

The solid state relay provided will control runway lights of either 115 Vac or 230 Vac with a load current up to 10 Amp if proper heatsinking is provided. Connect the output or load side of the relay in series with the hot ac line to the runway lights as shown in figure 3A. The load terminals of the relay are not polarity sensitive; so terminals 1 and 2 are interchangeable.

## OPTIONAL APPLICATIONS.

The FBN Receiver has many options which allow for use in other applications. You can probably skip this section, but very detailed information is provided for those who may be interested. Here are some other ways the receiver can be used.

- CAUTION: Be careful not to exceed the voltage or current capabilities of the transistors. Also, be very careful about transients generated by inductive loads, such as relays. The relay supplied is a solid-state relay, and it does not present a problem. However, conventional relay coils must have a diode connected across the coil to absorb transients from inductive kickback, which can reach several hundred volts when the coil is switched off. See application diagrams, which follow, for examples of how to connect the diode, which basically must conduct any energy of reverse polarity; so the diode is connected backwards from regular polarity of the power source. Therefore, the diode does not conduct unless


Wiring side of DB-9 female jack used on chassis


Figure 2. Connector Pinout.
there is a reverse voltage.
Application \#1: Runway Light Operation. To allow pilot control of runway lights (PCL), the three output transistors are turned on by clicking the microphone button in the aircraft, as explained later under Operation. Three clicks in five seconds turns on Output A, five clicks turns on Output B, and seven clicks turns on Output C. Only one can be on at one time. The outputs can be used to control relays to turn on the ac power for the lights. Think about how you want the lights to operate before wiring the outputs. There are ways to provide different options, depending on the wiring. The three outputs can be used to control relays for three levels of lighting. If you use fewer levels of lighting, any relays not wired will allow someone to turn off the lights. Therefore, you may want to parallel unused outputs with others to limit the options the pilot has and perhaps prevent undesired consequences, such as locking the lights off for 15 minutes or turning off the lights accidentally. See more information in Operation section.

Figure 3 shows two ways to turn on large ac loads with the receiver.


Figure 3A. Solid State Relay Wiring.


Figure 3B. Small Relay Switching Power Contactor.

The preferred method is to use a modern solid state relay which can be controlled with a small dc current and switch large ac loads. Solid state relays can be obtained from electrical supply houses and industrial suppliers, such as Grainger. You can buy extra relays from Grainger $\mathrm{p} / \mathrm{n} 6 \mathrm{C} 900$ relay (Omron p/n G3NA-210B-DC524). You may need another model, depending on the load current and other factors.

Figure 3A shows how to wire a solid state relay, with the negative side of the control input switched by the output of the receiver.

The older method of switching large loads is to use a small dc relay to turn on a large ac power contactor. This method is shown in figure 3B. Make sure that the smaller relay can be operated with less than 50 mA of current, and be sure to place a reverse polarity diode across the coil to prevent inductive kickback from damaging the receiver. This diode can be almost any type, including 1N4148, 1N914, 1N4001.

Variable runway light intensities can be controlled with 3,5 , and 7 mic clicks if the proper relays are connected for the lighting system in use. Actual connections depend on the particular lighting system, and it is impossible to make general recommendations here on how to do it.

Application \#2: ELT Detection. In the ELT mode which may be used to watch for downed aircraft, Output A and Output B are normally off, and Output C is normally on. This gives you two outputs to use to turn on something if a downed aircraft is detected. Output C turns off upon detection of an ELT signal, allowing it to be used for muting the audio until detection occurs. There may also be other applications. Here are several ideas for how to use these outputs.

Output A or B can be used to trip some sort of alarm when a downed aircraft is detected. An alarm circuit can be tripped by sinking current to ground within the limits outlined earlier.

The FBN Receiver normally is muted when no signal is present and unsquelched when a signal is on the air. However, you may have an application where you don't want to listen to any signal until an ELT has been on the air long enough to signify an alert. In such a case, you can wire Output C to the input of the Volume control (right hand lug) with a short hookup wire to mute the audio until the alarm is tripped. If you want to monitor sometimes and not wait for
an alert, you can install a switch inline with this wire to the Volume control so it only grounds the Volume control when you want that feature in effect.

## Reset Provisions.

In some installations, it may be desirable to reset the microcontroller used for PCL and ELT operation. For instance, you might want to have a switch on the unit to turn off runway lights manually or you might want to reset the ELT alarm manually. In such a case, simply wire a pushbutton switch from ground to External Reset terminal E7 on the pc board. When you press the button, it will cause the microcontroller to reboot from scratch and reset everything to the starting condition.

Any device which can generate a momentary ground (connected to ground plane on pc board) can be used to do the reset. For instance, a touch tone controller can be used to momentarily ground E7 to reset the micro. Such a setup would be handy if the FBN Receiver is connected to a repeater, and there probably are other cases where this feature would be useful.

## OPERATION.

## General.

The FBN Receiver has one microcontroller which is responsible for watching the squelch to determine what is happening on the air. It can be programmed to perform several different tasks in response. It can also be programmed for no special features so the receiver can be used just to monitor a channel, for example, at a small airport or at a pilot's home.

Basic operation is rather obvious. The Volume control, on the right side of the unit, sets the listening level. The Squelch control, on the left, sets the threshold at which signals will be heard and quiets background noise in between transmissions. Set it just clockwise far enough to quiet the speaker when no transmission is in progress. The LED is used to indicate various conditions as explained for each mode below.

## Default Mode.

The FBN Receiver normally is shipped set up to provide the following operation for the control of runway lights. You need not read any of the following sections unless you want to do other things.

The Receiver default setup allows it to turn runway lights on if the pilot clicks his/her microphone button
three, five, or seven times within five seconds. If the mic is clicked any other number of times, the lights will not turn on. The lights will stay on for 15 minutes, flash during the final minute as a warning, and then turn off. Changes are not allowed after the lights are turned on.

Note that pilots should be told to use three clicks to turn on the lights. Assuming that your lighting system does not allow for varying intensities, the unit has been wired to allow 5 or 7 clicks to also turn on the lights just as a safety measure; othe rwise, sending 5 or 7 clicks would lock off the lights for 15 minutes.

Mode switch $\mathbf{S 2}$ is set as follows for the default condition: 1101011.

## Mode Switch.

(You only need to read the following sections if you want to do something other than the default mode of operation.)

Seven position dip switch S 2 is used to program the microcontroller which provides special features. In the discussion below, "1" indicates that a particular switch is ON or closed and " 0 " indicates that a switch is OFF or open.

Positions 1 and 2 set the mode of operation. The four possible modes are as follows:

$$
\begin{aligned}
& 00=\text { monitor mode } \\
& 01=\text { test mode } \\
& 10=\text { ELT mode } \\
& 111=\text { PCL mode }
\end{aligned}
$$

Position 3 is set to allow an option in the basic operation as follows:

In ELT mode, turning on this switch allows the ELT alarm to automatically reset.

In PCL mode, turning on this switch allows changes to be made by the pilot after initially turning on lights.

Position 4 is an optional setting for the PCL mode. It controls how the output responds during the last minute runway lights are on. (It has no function for other modes, such as ELT mode.) If switch position 4 is turned on, the runway lights will flash during the last minute they are on to warn pilots that the lights are about to go out. If the switch is off, no flashing will occur; lights will simply turn off at the end of the timer period.

Positions 5 through 7 set the time delay for ELT and PCL modes in $5 \mathrm{mi}-$ nute increments. The switches set a four digit binary number which, multiplied by 5 , is the time delay in minutes. Following are example settings:

$$
\begin{array}{ll}
000=1 \mathrm{~min} & 100=20 \mathrm{~min} \\
001=5 \mathrm{~min} & 101=25 \mathrm{~min} \\
010=10 \mathrm{~min} & 110=30 \mathrm{~min} \\
011=15 \mathrm{~min} & 111=35 \mathrm{~min}
\end{array}
$$

Note that 000 sets it for one minute, an exception, handy for testing.

## Monitor Mode.

To use the receiver as a basic monitor receiver without the ELT or PCL modes, turn off switch sections 1 and 2. This tells the microcontroller to turn off, thus saving power.

## Test Mode.

Turning on switch section 2 with section 1 turned off sets the microcontroller for a special test mode in which the LED blinks on and off one cycle every two seconds. This allows a technician to check the controller clock accuracy, as there should be about 30 flashes per minute. Note that the controller clock is not as precise as a regular clock; so there may be a small variation in timing. This is normal. The purpose of the test is simply to see if the controller is running properly and that the clock is roughly accurate. The blinking will stop if the squelch is opened.

## Pilot Control of Lighting.

In the PCL mode, if a pilot clicks his push-to-talk button three, five, or seven times within five seconds, runway lights can be activated with Outputs A, B, and C, respectively. Depending on wiring, this can turn on runway lights at up to 3 intensity levels.

As explained earlier, programming the dip switch for PCL mode requires that switch sections 1 and 2 both be turned on. Switch position 3 allows for the option of letting the pilot make a change in settings once the lights are initially activated. Once the lights are activated, they will stay on for the length of time programmed with switch sections 5 through 7. Note that the timing system isn't precise; so if the time is too short, simply increase the setting until you get the about the length of time you want. Position 4 controls whether or not the lights flash during the final minute as a warning that they are about to go out.

When you install the system, carefully plan how you want the lights to respond to any possible condition. With the proper combination of programming and wiring the outputs to relays, you can make the lighting system operate smoothly and safely. Following are factors to be considered.

Your system may have only one or two intensities. Any outputs which
are not wired to one of the relays controlling the lights allows the pilot to turn off the lights. This may be undesirable from a safety standpoint, especially considering that someone may send the required command unintentionally, perhaps even someone trying to access lights at another nearby airport. For this reason, FAA guidelines recommend you not provide any means of turning off the lights remotely. Sending one of the three commands overrides the other two commands. You can prevent turnoff simply by wiring any unused outputs in parallel with another output so that accidental commands will turn on the lights.

The receiver has the option of allowing changes to the command after an initial command is executed. If the switch is on, subsequent commands will be carried out, otherwise, they will be ignored until the time delay is completed for turning off the lights. Allowing changes may be good, depending on the way the relays are wired. If you are sure there is no way to turn the lights off altogether, it allows a pilot to correct an erroneous command or to increase or decrease the intensity. If you do not allow changes and someone, even unintentionally, sends a command, they cannot carry out another command for 15 minutes or whatever the time delay is set for.

The red LED on the front of the receiver will illuminate anytime a command is in effect, that is, whenever one of the outputs is activated.

If you wish to have a way to turn off the lights manually, you can use a reset switch, as explained in the In stallation section. Resetting the controller effectively starts everything from scratch with the lights off.

Turning the power to the receiver off momentarily will also reset the controller. Therefore, consider the safety aspect of providing backup power for your runway lighting system to prevent lights from being turned off by a momentary power outage. A simple way to prevent the receiver from losing power is to operate it from a battery with a trickle charger.

## ELT Detection.

In ELT mode, if a signal is received and keeps the squelch open for a continuous period of time longer than the programmed delay, the ELT alarm will be tripped. The alarm causes Outputs A and B to be turned on and Output C to be turned off. There are many ways to use these output transistors to trigger an external alarm, activate a re-
peater, unmute the audio, etc., as discussed in the Installation section.

As explained earlier, programming the dip switch for ELT mode requires that switch section 1 be turned on and section 2 be turned off.

Switch sections 5 through 7 set the time delay required for triggering the alarm. In order for the alarm to be tripped, the squelch must remain open during the entire time delay you set. Since ELT testing is allowed by the FAA for periods not to exceed 5 minutes, the minimum practical setting for the delay time is 10 minutes.

If the signal disappears or gets weak enough for the squelch to close, the detector will be reset with the timer starting over. Therefore, setting the squelch threshold with the Squelch control determines how weak a signal you want to be able to trip the alarm.

Turning on switch section 3 provides the option of automatically resetting the ELT alarm if the carrier later goes off the air. If section 3 is turned off, the alarm condition remains in effect until the manual reset switch is operated or power to the receiver is turned off and on again. It is considered desirable to have a manual reset switch even if you allow automatic reset. The reset can even be done remotely by touch tone command, as explained in the Installation section.

The red LED on the front of the receiver will illuminate anytime an ELT alarm has occurred, and it remains on until the alarm circuit is reset.

Note: Units supplied in a cabinet have the three outputs wired in parallel at the mating plug, assuming the receiver will be used for pilot controlled lighting. The connection between the three pins must be removed from the plug to use the ELT Detection mode.

## Signal Strength Indicator.

The FBN Receiver has the capability of driving an external signal strength meter. By using the receiver in a portable setup with an S-meter, the FBN Receiver can be used to help find downed aircraft. Therefore, it may be desirable to have more than one receiver, including one set up as a permanent alarm monitor and others used to hunt. Note that the FBN Receiver does not have the S-meter function wired at the 9-pin connector, but you can add a wire from the board to the connector if this feature is of use.

FREQUENCY ADJ USTMENTS.

## Opening Case.

If your receiver was supplied factory installed in a cabinet, remove the four screws on the side of the cabinet, and lift off the cover.

## General Procedure.

The channel frequency is determined by frequency synthesizer circuits, which use dip switch S1 in conjunction with programming in microcontroller U1 to set the channel. The microcontroller reads the dip switch information and does mathematics, applying serial data to the synthesizer ic whenever power is applied. Following is a discussion of how to set the dip switch to the desired channel frequency.

NOTE: If the frequency is changed more than about 1 MHz , a complete alignment of the receiver should be performed, as described in later text. Optimum operation only occurs if the synthesizer is adjusted to match the frequency switch setting and all the tuned amplifier circuits are peaked for the desired frequency.

To determine what channel frequency to use, the microcontroller adds the frequency information from the dip switch to the 118 MHz "base" frequency.

Dip switch settings are binary; each switch section has a different weighting, twice as great as the next lower section. Sections have weights such as $25 \mathrm{kHz}, 50 \mathrm{kHz}$, etc., all the way up to 12.800 MHz . (See Table 3 or the schematic diagram for switch values. Also see the shortcuts and tricks which follow this discussion.)

The system sounds cumbersome, but it really is fairly simple, and you don't need to do this frequently. A piece of paper or a small calculator is handy to aid in determining which sections of the switch to turn on. When done, you might want to record the switch settings in table 4 for future reference.

Begin by subtracting the base frequency, 118.000, from the desired frequency to determine the total value of all the switch sections required to

| Table 3. |  |
| :--- | :--- | Frequency Settings

be turned on.
If the difference is greater than 12.800 MHz , turn on switch \#1, and subtract 12.800 from the difference frequency to determine the remainder. Otherwise, turn off switch \#1.

Do the same for each of the other sections, from highest to lowest weighting, in sequence. Each time you consider the remainder, turn on the switch section with the highest weighting which will fit within the remainder without exceeding it. Each time it is found necessary to turn on a switch section, subtract the value of that section from the remainder to get the new remainder.

As an example, let us consider how to set the receiver for 127.325 MHz . The following discussion is broken down into steps so you can visualize the process easier.
a. $127.325-118.000$ base freq. $=$ 9.325 MHz remainder. Turn on switch \#2, which represents the largest increment to fit remainder. Turn off switch \#1 because its value is larger than 9.325.
b. 9.325-6.400 value of switch $\# 2=2.925 \mathrm{MHz}$. Turn off switch \#3, which is too large a value. Turn on \#4, which is 1.600 MHz , the largest increment to fit the remainder.
c. $2.925-1.600=1.325 \mathrm{MHz}$ remainder. Turn on switch \#5, which has a value of $0.800 \mathrm{MHz}(800 \mathrm{kHz})$.
d. $1.325-0.800=0.525 \mathrm{MHz}$ ( 525 kHz ) remainder. Turn on switch \#6, which has a value of 400 kHz .
e. $525-400=125 \mathrm{kHz}$ remainder. Now it is easy. Looking at the weightings of the switches, you can see that turning on switches 8 and 10 gives 125 kHz . Turn off switches 7 and 9 , which are not needed.
f. When we finished, we had turned on switch sections $2,4,5,6,8$, and 10 . We turned off all the others. This can also be expressed as the binary number 0101110101.

Note: Dip switch information is read by the synthesizer only when power is first applied. If switch settings are changed, turn the power off and on again.

## Shortcut.

If you have access to the internet, our website has a long table of numbers which gives the equivalent binary number settings for every possible frequency. We couldn't print it here because it takes many printed pages of space. Surf to our website at www.hamtronics.com and look for Dip Switch Freq Programming for FBN Receiver near the bottom of the Table of Contents.

Look up the frequency, and it will give you all the binary switch settings. The address is case sensitive, and you must enter the address carefully, exactly as shown.

## Another Trick.

If you have a computer, but no internet access, you can use the calculator program to quickly determine the binary settings for the dip switch. Use this procedure.
a. Start the calculator program, by going to Run under the Start menu, and type CALC.EXE.
b. In the calculator menu, select View - Scientific.
c. Enter the frequency you want to operate on, example 127.325.
d. Subtract the base frequency of 118.000, which gives a remainder of 9.325 MHz in our example.
e. Divide by 25 because the receiver tunes in 25 kHz increments. This gives the answer 0.373 MHz .
f. Multiply by 1000 to convert to kHz . This gives you 373 in our example.
g. Convert this decimal number to binary by clicking on BIN on the toolbar. This reads out as "101110101".
h. The calculator drops any leading zeros. However, we need a ten digit binary number; so add leading zeros (left side of number) to make a total of ten digits. In this case, add one zero to make it "O101110101". This is the binary number to set in the switches. One $=$ ON and zero $=$ OFF.

## ALIGNMENT.

## General Information.

Following are three alignment procedures. The first is alignment of the frequency synthesizer and receiver front end (rf amplifier and mixer). This must be done whenever the channel frequency is changed by more than 1 MHz . The FBN Receiver is a high performance receiver and is designed to be very selective. Therefore, retuning is necessary for optimum performance. The second procedure is alignment of the if stages, which normally is only necessary if some parts are replaced. The third procedure is trimming the crystal oscillator to exact frequency, which should be

done once each year or two to compensate for crystal aging.

## Equipment Needed.

Equipment needed for alignment is a sensitive dc voltmeter and a stable and accurate signal generator for the channel frequency. To adjust the crystal oscillator, a frequency counter is required.

The slug tuned coils in the receiver should be adjusted with the proper .062" square tuning tool to avoid cracking the powdered iron slugs. Variable capacitors and i-f transformers should be adjusted with a plastic tool having a small metal bit. (See A28 and A2 tools in catalog.)

## Opening Case.

If your receiver was supplied factory installed in a cabinet, remove the four screws on the side of the cabinet, and lift off the cover.

## Channel Frequency Alignment.

Alignment is needed whenever the frequency is changed by more than about 1 MHz . Alignment ensures that the frequency synthesizer is optimized at the center of the vco range and that all stages are tuned to resonance.
a. Set dip switches for desired frequency.
b. Set the SQUELCH control fully counterclockwise and the VOLUME control just a little clockwise.
c. Connect power. You should hear white noise.
d. Connect voltmeter to V-tune test point TP1 (top lead of R6). Adjust vco coil L1 for +4 Vdc . (Although the vco will operate over a wide range of tuning voltages from about 1 V to 7 V , operation is optimum if the vco is adjusted to 4 V .)
e. Connect voltmeter to buffer TP2 (top lead of R16). Adjust buffer coil L3 for a peak, typically about +0.5 V to +0.9 V .
f. Connect an accurate signal generator to Jl using a coax cable with RCA plug. Adjust signal generator to exact channel frequency, and turn output level up fairly high (about $1000 \mu \mathrm{~V}$ ).
g. Connect voltmeter to AGC TP4 (top lead of R30).
h. Adjust L4, L5, L6, L7, and L8 for minimum voltage. (Voltage goes down, not up, with increased signal level.)

## Alignment of I-F Stages.

a. Connect an accurate signal generator to test point TP3 (top lead of R19), using coax cable with clip leads.
b. Connect voltmeter to AGC TP4 (top lead of R30).
c. Set generator to exactly 10.695 MHz . Use a frequency counter or a synthesized signal generator. Set level just high enough to reduce the meter reading to about 3 Vdc (about $200 \mu \mathrm{~V}$ ).
d. Adjust T1, T2, and T3 for minimum de voltage. Note that the transformers are fairly close from the factory and usually only require less than 1 turn in either direction.

- Be careful not to turn the slug tight against either the top or bottom because the winding of the transformer can be broken.


## Oscillator Trimming.

Once each year, the crystal oscillator should be checked and adjusted back on frequency. Crystals normally age a little every year, with most of the aging change occurring in the first year.

To make this adjustment, connect an accurate frequency counter to TP3 with a coax cable clip lead, and adjust C6 with an insulated tool (like our model A2 tool). The frequency should be 10.695 MHz above the channel frequency.

The adjustment can theoretically also be done by monitoring the 10.240 oscillator frequency, but it is difficult to pick up the signal from the oscillator without loading the oscillator down. Monitoring at TP3 provides buffering and allows finer resolution because it is at the higher frequency.

## THEORY OF OPERATION.

The FBN Receiver is a frequency synthesized vhf am receiver. Refer to the schematic diagram for the following discussion.

Low noise dual-gate mos fet's are used for the RF amplifier and mixer stages. The output of first mixer Q 5 Is coupled through 10.695 MHz transformer T1 to the second mixer.

U4 provides IF amplification, a $2^{\text {nd }}$ mixer to convert to 455 kHz , a detector, if age, rf age and squelch. ©ramic filters FL1 and FL2 provides adjacent channel selectivity at 455 kHz . T2 and T3 provide impedance matching for the filters. U4c is an envelope detector. It also provides agc for the if stages within U4 and delayed rf age for gate2 of Q 4 . TP4 allows monitoring of the agc voltage as an indication of signal strength to use for alignment. U4c pin 12 provides a current source to drive an external Smeter based on the agc signal level.

Detected audio is applied through volume control R31 to audio amplifier U6. Squelch transistor 88 mutes this audio when no signal is present. 88 is driven through squelch amplifiers

U4d and B7. Squelch control R34 sets the threshold at which the squelch opens. C57 provides a slight delay to eliminate switching clicks when the audio is turned on and off.

The injection frequency for the first mixer is generated by vco (voltage controlled oscillator) 61. The injection frequency is 10.695 MHz above the receive channel frequency. The output of the vco is buffered by Q2 to minimize effects of loading and voltage variations of following stages from modulating the carrier frequency. The buffer output is applied through a double tuned circuit to gate 2 of mixer Q5.

The frequency of the vco stage is controlled by phase locked loop synthesizer U2. A sample of the vco output is applied through the buffer stage and R1 to a prescaler in U2. The prescaler and other dividers in the synthesizer divide the sample down to 5 kHz .

A reference frequency of 10.240 MHz is generated by a crystal oscillator. The reference is divided down to 5 kHz .

The two 5 kHz signals are compared to determine what error exists between them. The result is a slowly varying dc tuning voltage used to phase lock the vco precisely onto the desired channel frequency.

The tuning voltage is applied to carrier tune varactor diode D1, which varies its capacitance to tune the tank circuit formed by L1/C20/C21. C16 limits the tuning range of D 1 . The tuning voltage is applied to D1 through a third order low pass loop filter, which removes the 5 kHz reference frequency from the tuning voltage to avoid whine.

Serial data to indicate the desired channel frequency and other operational characteristics of the synthesizer are applied to synthesizer U2 by microcontroller U1. Everything the synthesizer ic needs to know about the band, division schemes, reference frequency, and oscillator options is generated by the controller. Information about the base frequency of the band the receiver is to operate on and the channel within that band is calculated in the controller based on information programmed in the eprom on the controller and on channel settings done on dip switch S1. Whenever the microcontroller boots at power up, the microcontroller sends several bytes of serial data to the synthesizer, using the data, clock, and /enable lines running between the two ic's.

Some of the 10.240 MHz signal generated in U2 is used for the injec-
tion to second mixer U4a. 89 provides buffering for this injection signal.

Microcontroller U5 provides the intelligence to control runway lights and detect downed aircraft ELT signals. It senses squelch openings at interrupt pin 19, and its three outputs drive switching transistors Q10, Q11, and Q12. These transistors are capable of driving external relays and may be used in other ways as described in the Installation section. Care must be used to avoid reverse polarity, overvoltage, and transients, all which can damage the transistors.
+13.6 Vdc power for the receiver is applied at E3. Audio output amplifier U6 is powered directly by the +13.6 Vdc . All the other stages are powered through voltage regulators for stability and to eliminate noise. U 3 is an 8 Vdc regulator to power if amplifier U4, RF amplifier Q4, mixer Q5, and the vco, buffer, and phase detector in the synthesizer. Additional filtering for the vco and buffer stages is provided by capacitance amplifier Q3, which uses the characteristics of an emitter follower to provide a very stiff supply, eliminating any possible noise on the power supply line. Q6 provides a stiff +5 Vdc supply for the frequency synthesizer and microcontrollers, which are low current CMOS devices.

## TROUBLESHOOTING.

## General.

The usual troubleshooting techniques of checking dc voltages and signal tracing with an RF voltmeter probe and oscilloscope will work well in troubleshooting the FBN Receiver. DC voltage charts and a list of typical audio levels are given to act as a guide to troubleshooting. Although voltages may vary widely from set to set and under various operating and measurement conditions, the indications may be helpful when used in a logical troubleshooting procedure.

## Current Drain.

Power line current drain normally is about 75 mA with volume turned down or squelched and up to 200 mA with full audio output.

If the current drain is approximately 100 mA with no audio output, check to see if voltage regulator U3 is hot. If so, and the voltage on the 8 V line is low, there is a short circuit on the +8 Vdc line somewhere. U3 limits the short circuit current to 100 mA to protect the receiver from damage. If you clear the short circuit, the voltage
should rise again. U3 should not be damaged by short circuits on its output line; however, it may be damaged by reverse voltage or high transient voltages.

A good way to isolate short circuits and other overloads on the 8 V or 5 V lines is to disconnect components in series with the path, for instance, ferrite beads or Q6. With so many things connected to the $\mathrm{B}+$ lines, it is difficult to find the problem without eliminating large portions of the load that way.

## Audio Output Stage.

Note that audio output ic U6 is designed to be heatsunk to the pc board through the many ground pins on the ic. When running moderately low audio levels as most applications require, it is no problem to use an ic socket; so we have provided one for your convenience. If you will be running high audio levels, check to see if the ic is getting hot. If so, you should remove the ic socket, and solder the LM-380N-8 ic directly to the board for better heatsinking.

If audio is present at the volume control but not at the speaker, the audio ic may have been damaged by reverse polarity or a transient on the B+ line. This is fairly common with lightning damage.

If no audio is present on the volume control, the squelch circuit may not be operating properly. Check the dc voltages on U4d, Q7, and Q8.

## RF Signal Tracing.

If the receiver is completely dead, try a 10.695 MHz signal applied to TP-3 (the top lead of R19), using coax clip lead. Connect coax shield to pcb ground. Set level just high enough to get a change of age voltage at TP4. At $10 \mu \mathrm{~V}$, you should notice some degree of change in agc voltage.

Also, check the 10.240 MHz oscillator with a scope or by listening with an hf receiver or service monitor.

A signal generator on the channel frequency can be injected at various points in the front end. If the mixer is more sensitive than the RF amplifier, the RF stage is suspect. Check the dc voltages looking for a damaged fet, which can occur due to transients or reverse polarity on the dc power line. Also, it is possible to have the input gate (gate 1) of the RF amplifier fet damaged by high static charges or high levels of RF on the antenna line, with no apparent change in dc voltages, since the input gate is normally at de ground.

## Synthesizer Circuits.

Following is a checklist of things to look for if the synthesizer is suspected of not performing properly.
a. Check the output frequency of the vco buffer with a frequency counter. It should be 10.695 MHz above the channel frequency.
b. Check tuning voltage at TP1. It should be about +4 Vdc . Actual range over which the unit will operate is about +1 Vdc to just under +8 Vdc . However, for optimum results, the vco should be tuned to allow operation at about +4 Vdc center voltage.
c. Check the operating voltage and bias on the vco and buffer.
d. Check the 10.240 MHz oscillator at pin 1 of the synthesizer ic (actually best to check at lead of R3; avoid trying to probe surface mount ic leads which are close together). A scope should show strong signal (several volts $\mathrm{p}-\mathrm{p}$ ) at 10.240 MHz .
e. Check the oscillator at pin 1 of microcontroller ic U1 with a scope. There should be a strong ac signal (several volts p-p) at the oscillator frequency.
f. The data, clock, and /enable lines between the microcontroller and synthesizer ic's should show very brief and very fast activity, sending data to the synthesizer ic shortly after the power is first applied or a dip switch setting is changed. Because this happens very fast, it can be difficult to see on a scope. Use $100 \mu \mathrm{Sec} / \mathrm{div}$, $5 \mathrm{Vdc} /$ div, and NORMAL trigger.
g. Check the microcontroller to see that its /reset line is held low momentarily when the power is first applied. Cl works in conjunction with an internal resistor and diode in the ic to make C1 charge relatively slowly when the power is applied. It should take about a second to charge up.
h. Check the switch settings to be sure you have the correct frequency information going to the microcontroller. Check each of the output lines of the switch to verify that the voltage actually is present.
i. If you have a scope or spectrum analyzer, you can check the output pin of the divide by 64 prescaler at pin 13 of U2. There should be a strong signal (several volts $p-p$ ) at about 2 MHz . If this signal is absent, there may not be sufficient level of sample signal from the buffer at U2 pin 11. Be careful not to short adjacent pins of the ic.

## Microphonics, Hum, and Noise.

The vco and loop filter are very sensitive to hum and noise pickup
from magnetic and electrical sources. Some designs use a shielded compartment for vco's. We assume the whole board will be installed in a shielded enclosure; so we elected to keep the size small by not using a separate shield on the vco. However, this means that you must use care to keep wiring away from the vco circuit at the right side of the board. Having the board in a metal enclosure will shield these sensitive circuits from florescent lights and other strong sources of noise.

Because the frequency of a synthesizer basically results from a free running $\mathrm{L}-\mathrm{C}$ oscillator, the tank circuit, especially L1, is very sensitive to microphonics from mechanical noise coupled to the coil. You should minimize any sources of vibration which might be coupled to the receiver, such as motors. In addition, it helps greatly to prevent the molded coil from vibrating with respect to the shield can. Both the coil and can are soldered to the board at the bottom, but the top of the coil can move relative to the can and therefore cause slight changes in inductance which show up as frequency modulation. Securing the top of the plastic coil form to the shield can with some type of cement or nail polish greatly reduces the microphonic effects. This practice is recommended in any installation where vibration is a problem, and the factory normally cements this coil for that reason.

Excessive noise on the dc power supply which operates the receiver can cause noise to modulate the synthesizer output. Various regulators and filters in the receiver are designed to minimize sensitivity to wiring noise. However, in extreme cases, such as in mobile installations with alternator whine, you may need to add extra filtering in the power line to prevent the noise from reaching the receiver.

Other usual practices for mobile installations are recommended, such as connecting the + power and ground return lines directly to the battery instead of using cigarette lighter sockets or dash board wiring.

To varying degrees, whine from the 5 kHz reference frequency may be heard on the signal under various circumstances. If the tuning voltage required to tune the vco on frequency is $\checkmark$ very high or low, near one ex-
treme, the whine may be heard. $\Omega$ This can also happen even when the tuning voltage is properly near the 4 Vdc center if there is dc loading on the loop filter. Any current loading, no matter how small, on the loop filter
causes the charge pump in the phase detector to pump harder to maintain the tuning voltage. The result is whine on the signal. Such loading can be caused by connecting a voltmeter to TP1 for testing, and it can also be caused by moisture on the loop filter components.

Phase noise is a type of white noise which phase locked loop synthesizers produce. Many efforts are made during the design of the equipment to reduce it as much as possible. The phase noise in this unit should be almost as good as a crystal oscillator radio. If you notice excessive white noise even though the signal is strong, it may be caused by a noisy vco transistor, Q1. Try swapping with the buffer transistor, Q2, which is the same type and see if that helps. When using a replacement transistor for repairs, be sure to use one of good quality.

If you suspect noise is being introduced in the synthesizer, as opposed to the signal path from the antenna to the detector, you can listen to the injection signal at 10.695 MHz above the channel frequency on a receiver or service monitor and hear what just the injection signal sounds like. Put a pickup lead on top of the receiver board so you have a strong sample to hear so you are sure the noise is not due to weak signal pickup at the test receiver.

## Typical Dc Voltages.

Tables 4-6 give dc levels measured with a sensitive dc voltmeter on a sample unit with 13.6 Vdc B+ applied. All voltages may vary considerably without necessarily indicating trouble. The charts should be used with a logical troubleshooting plan. All voltages are positive with respect to ground except as indicated.

Use caution when measuring voltages on the surface mount ic. The pins are close together, and it is easy to short pins together and damage the ic. We recommend trying to connect meter to a nearby component connected to the pin under question. Also, some pins are not used in this design, and you can generally not be concerned with making measurements on them.

Note: On the schematic diagram, these symbols indicate logic le vels:
indicates active lo ( 0 V in stated condition)
indicates active hi ( 5 V in stated condition)

## Typical Audio Levels.

Table 7 gives rough measurements
of audio levels. Measurements were taken using an oscilloscope, with no input signal, just white noise (squelch open) so conditions can be reproduced easily.

## REPAIRS.

If you need to unsolder and replace any components, be careful not to damage the plated through holes on the pc board. Do not drill out any holes. If you need to remove solder, use a solder sucker or solder wick. A toothpick or dental probe can be used with care to open up a hole.

If you need to replace surface mount ic U2, first be very sure it is damaged. Then, carefully cut each lead off the case with fine nose cutters. Once the case is removed, individual leads can be unsoldered and the board can be cleaned up. Carefully position the new ic, and tack solder the two opposite corner leads before any other leads are soldered. This allows you to melt the solder and reposition the ic if necessary. Once you are sure, the remaining leads can be soldered. If you get a solder short between leads, use a solder sucker or solder wick to remove the excess solder.

| Table 4. Typical Test Point Voltages |  |  |  |
| :--- | :--- | :--- | :---: |
| TP1 |  | Tuning V. Normally set at <br> 4 V |  |
| TP2 | Buffer | approx. 0.8 V |  |
| TP3 | Test Input | (No reading) |  |
| TP4 | AGC | Varies from about 4.5 V <br> with no signal to 0.2 V with <br> strong signal $(\sim 3000 \mu \mathrm{~V})$ |  |


| Xstr | Stage | E(S) | B(G1) | C(D) | G2 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q1 | vco | 1.5 | 2.0 | 7.0 | - |
| Q2 | buffer | 0 | 0.75 | 4.5 | - |
| Q3 | dc filter | 6.8 | 7.4 | 7.6 | - |
| Q4 | RF ampl | 0 | 0 | 8 | 3.5 |
| Q5 | Mixer | 0 | 0 | 8 | 0 |
| Q6 | 5 V regul. | 5 | 5.6 | 8 | - |
| Q7 | sq open | 0 | 0.67 | 0.15 | - |
|  | sq closed | 0 | 0.03 | 5 | - |
| Q8 | sq open | 0 | 0.14 | 0 | - |
|  | sq closed | 0 | 0.66 | 0.01 | - |
| Q9 | Buffer | 0 | 0.7 | 3.3 | - |
| Q10-Q12 on |  | 0 | 0.7 | * | - |
| Q10-Q12 |  | 0 | 0 | * | - |


| Table 6. Typical IC DC Voltages |  |  |  |
| :--- | :--- | :--- | :--- |
| U1-1 | 2.3 | U1-20 | 5 |
| U1-2 | 2.3 |  |  |
| U2-1 | 2.2 | U2-10 | 2.6 |
| U2-2 | 5V locked, | U2-11 | 2.6 |
|  | 2.5 V unlocked | U2-12 | 5 |
| U2-3 | $8^{*}$ | U2-13 | $3.2^{*}$ |
| U2-4 | $8^{*}$ | U2-14 | 5 |
| U2-5 | 8 | U2-15 | $*$ |
| U2-6 | $0-8$ (4V tuned) | U2-16 | $*$ |
| U2-7 | 0 | U2-17 | 5 |
| U2-8 | 4.5 | U2-18 | 0 |
| U2-9 | 5 | U2-19 | 5 |
| * pin | not used | U2-20 | 2 |
| U4-1: | 0.86 | U4-11: | 0.64 |
| U4-2: | 1.4 | U4-12: | 0.2 (no |
| U4-3: | 5.4 | meter connected) |  |
| U4-4: | 0.68 | U4-13: | 4.5 |
| U4-5: | 0 | U4-14: |  |
| U4-6: | 5.5 | sq open | 0.72 |
| U4-7: | 1.4 | sq closed | 0.85 |
| U4-8: | 1.4 | U4-15: |  |
| U4-9: | 0.77 | fully open 3.2 |  |
| U4-10: | 5.6 | fully closed 0 |  |
| U5-1 | 2.3 | U5-20 | 5 |
| U5-2 | 2.3 |  |  |
| U6-1: | 0 | U6-5: | 0 |
| U6-2: | 0 | U6-6: | 6 |
| U6-3: | 0 | U6-7: | 13.6 |
| U6-4: | 0 | U6-8: | 6.8 |


| Table 7. Typical Audio Voltages |  |
| :--- | :--- |
| Audio Test Point | Normal Level |
| U4-9 Detector | 100 mV p-p |
| Top of Volume Con- <br> trol R31 | $75 \mathrm{mV} \mathrm{p-p}$ |
| Speaker Out E2 <br> with volume up full | up to 4V p-p |

## LIMITED WARRANTY.

Hamtronics, Inc. warrants all products manufactured by it to be free from defective material or workmanship for 1 year under normal use and service. Our obligation is limited to repairing or replacing such product which proves to be defective by our examination. Warranty does not apply to parts damaged in use, nor does it cover transportation costs. Semiconductors specifically are excluded because they are easily damaged in use. Hamtronics, Inc. assumes no liability for consequential damages.

If you need service on your unit, please call us at 585-392-9430 and we can advise you.

## PARTS LIST.

Following are notes specific to certain parts.
(1) Microcontrollers must be factory programmed for each application, and they are not interchang eable.
(2 Resistors used as test point or external connection point. These must be installed on the board oriented properly and with the top loop an extra $1 / 6$ " high to allow for connections to the loop later. (See detail in component location diagram.)

- Caution: Ic's and fet's are static sensitive. Use appropriate handling precautions to avoid damage.

| Ref Desig | Description (marking) |
| :---: | :---: |
| C1-C2 | $0.1 \mu \mathrm{f}$ monolithic (104) |
| C3 | n/a |
| C4 | 1 pf |
| C5 | 27pf |
| C6 | 10pf var cap (white) |
| C7 | 27pf |
| C8 | . $001 \mu \mathrm{f}(102,1 \mathrm{nM}$, or 1nK) |
| C9 | $0.1 \mu \mathrm{f}$ monolithic |
| C10 | $0.15 \mu \mathrm{fmylar}$ (red) |
| C11 | . $022 \mu \mathrm{f}$ mylar (223) |
| C12 | . $0022 \mu \mathrm{fer}$ ( 2.2 nK or 222) |
| C13 | $0.1 \mu \mathrm{f}$ monolithic (104) |
| C14 | 100 $\mathrm{\mu f}$ electrolytic |
| C15 | $0.1 \mu \mathrm{f}$ monolithic (104) |
| C16 | 10pf |
| C17-C18 | . $001 \mu \mathrm{f}$ ( $102,1 \mathrm{nM}$, or 1nK) |
| C19 | 100 $\mathrm{\mu f}$ electrolytic |
| C20 | 15pf |
| C21 | 68pf |
| C22 | 4pf |
| C23 | . $001 \mu \mathrm{f}$ ( $102,1 \mathrm{nM}$, or 1nK) |
| C24 | 30pf |
| C25 | 82pf |
| C26 | 2pf |
| C27 | . $001 \mu \mathrm{f}$ ( $102,1 \mathrm{nM}$, or 1 nK ) |
| C28 | 33pf |
| C29 | 82pf |
| C30 | 220pf (221) |
| C31 | 27pf |
| C32 | 0.5 pf (1/2pf) |
| C33 | 27 pf |
| C34 | 0.5 pf (1/2pf) |
| C35 | 22pf |
| C36 | 4pf |
| C37 | 27pf |
| C38 | 82pf |
| C39 | 4pf |
| C40 | . $01 \mu \mathrm{f}$ (103) |
| C41 | . $001 \mu \mathrm{f}$ ( $102,1 \mathrm{nM}$, or 1nK) |
| C42 | . $01 \mu \mathrm{f}$ (103) |
| C43-C45 | 100 ff electrolytic |
| C46 | 470رf electrolytic |
| C47-C49 | $0.1 \mu \mathrm{f}$ monolithic (104) |
| C50-C51 | 100 ff electrolytic |
| C52 | 10hf electrolytic |
| C53 | 100 ff electrolytic |
| C54 | 10hf electrolytic |
| C55 | . $01 \mu \mathrm{f}$ (103) |
| C56 | $0.15 \mu \mathrm{fmylar}$ (red) |
| C57 | $1 \mu \mathrm{felectrolytic}$ |
| C58 | 47pf |
| C59 | . 01 ¢ ( 103 ) |
| C60-C61 | 4.7 ${ }^{\text {f }}$ electrolytic |
| D1 | BB809 varactor diode |
| Note: Factory-built units may use smt part BB132 on rear of board instead. |  |
| D2 | 1N4148 switching diode |
| D3 | mini red LED |
| FL1-FL2 | 455 kHz ceramic filter, type "E" |
| J1 | RCA jack |
| L1 | $21 / 2$ turn slug-tuned coil (red) |
| L2 | $0.33 \mu \mathrm{H}$ RF choke (red-sil-orn-orn) |
| L3-L8 | $21 / 2$ turn slug-tuned coil (red) |
| L9 | $0.33 \mu \mathrm{H}$ RF choke (red-sil-orn-orn) |
| Q1-Q2 | 2N5770 |
| Q3 | 2N3904 |
| Q4-Q5 * | 3SK122 MOS FET |
| Q6-Q12 | 2N3904 |
| R1 | $180 \Omega$ |
| R2 | 2.2 K |
| R3 | 10 meg |
| R4 | 47K |
| R5 | 15K |


| R6 2 | 47K |
| :---: | :---: |
| R7 | 510K |
| R8 | 2.2K |
| R9 | 10K |
| R10 | 6.8K |
| R11 | 3.9K |
| R12 | $180 \Omega$ |
| R13 | $47 \Omega$ |
| R14 | 47K |
| R15 | $470 \Omega$ |
| R16 2 | 3.9 meg |
| R17 | 100K |
| R18 | 27K |
| R19 2 | 47K |
| R20 | 2.2K |
| R21 | $270 \Omega$ |
| R22 | 2.2K |
| R23 | 4.7K |
| R24 | 330K |
| R25 | $180 \Omega$ |
| R26 | $27 \Omega$ |
| R27 | $100 \Omega$ |
| R28 | n/a |
| R29 | $270 \Omega$ |
| R30 2 | 15K |
| R31 | 100K VOLUME |
| R32-R33 | 47K |
| R34 | 100K SQUELCH |
| R35 | 27K |
| R36 | 15K |
| R37 | 6.8K |
| R38 | 8.2K |
| R39 | 100K |
| R40 | $100 \Omega$ |
| R41 | $470 \Omega$ |
| R42-R44 | 4.7 K |
| R45 | $470 \Omega$ |
| S1 | 10 pos. dip switch |
| S2 | 7 pos. dip switch |
| T1 | 10.7 MHz IF xfmr (7A-691F) |
| T2-T3 | 455kHz IF xfmr <br> (RLC-352 or YMC-15002) |
| U1 - 0 | MC68HC705J1A $\mu \mathrm{P}$ |
| U2 * | MC145190F synthesizer |
| U3 | 78L08 regulator |
| U4 | CA3088 i-f ampl detector |
| U5 - | MC68HC705J1A $\mu \mathrm{P}$ |
| U6 | LM380N-8 af output |
| Y1 | 10.240 MHz crystal |
| Z1-Z3 | Ferrite bead, prestrung |



Figure 4. Placement of U2 Under PC Board.
Note that dot on ic goes toward rear of the board.


Figure 5. R121 VHF Aircraft Receiver, Component Locations


