HAMTRONICS[®] R317 UHF RUNWAY LIGHT CONTROLLER: INSTALLATION, OPERATION, & MAINTENANCE



GENERAL INFORMATION.

Functional Description.

The R317 Receiver is designed for small airports to facilitate pilot control of lighting with a uhf comm radio. It builds on proven frequency synthesized receiver technology Hamtronics[®] vhf and uhf fm receivers have been noted for. It is tunable over a range of bands in 25kHz increments. It uses tripletuned circuits in the front end and crystal and ceramic filters in the i-f with steep skirts for excellent adjacent channel and out-of-band selectivity.

The R317 has a microcontroller which is responsible for watching the squelch to determine what is happening on the air. It responds to mic clicks as follows.

Runway lights may be activated by keying the aircraft comm. radio microphone several times, typically three times in five seconds.

If the airport is equipped with variable intensity lighting, the pilot can select intensities by keying the microphone 3, 5, or 7 times in a 5-second period.

Lights remain on for a specific period of time, usually 15 minutes.

A dip switch option permits change in intensity after initial turn-on. Front panel LED

Table 1. Quick Reference

Frequency range: Customized to order Channel spacing: 25 kHz. Frequency set with dip switch; (repeaking coils required for freq change more than 2 MHz - use A1 tool)

Squelch sensitivity: adjustable 0.3 - 2 μ V 12dB sinad sensitivity: 0.3 μ V Adjacent channel selectivity: 100 dB

Image rejection: 60-70dB Temp stability: ±2ppm -30°C to +60°C Control outputs: three separately controlled open-collector switching transis-

tors able to sink up to 50 mA to ground on circuits up to 15Vdc. External solid state relays can be controlled for high current loads.

Antenna connector: RCA jack (50Ω) Power and control connections: solder terminals on pc board

Size: 4 in wide, 3 in deep, 1.25 in high. Operating Power: +13.6Vdc +-10% at approx. 50mA, depending on audio level indicates when lights have been activated at any intensity.

A second LED indicates when the squelch is open.

The R317 Receiver has an audio output; however, this is an fm receiver, not am, to provide excellent squelch carrier detection; therefore, even though you can listen to the channel, it will not detect am signals as an ordinary aircraft receiver will. You will be able to hear if there is a signal or any interference on the channel.

INSTALLATION.

Mounting.

Some form of support should be provided under the pc board, generally mounting the board with standoffs to a chassis.

The receiver board relies on the mounting hardware to provide the ground connections to the ground plane on the board; so metal standoffs and screws should be used for mounting.

Electrical Connections.

The antenna connection is made with a coaxial connector. All other connections are made at solder terminals on the pc board. Table 2 identifies the terminals used for these connections. The view of the pc board at the rear of the manual identifies the solder terminals on the pcb module.

Power and control signals should be connected to the unit with #22 solid hookup wire. Be careful not to route the wiring close to the components on the left hand side or rear of the pc board, which contains sensitive rf circuits which could pick up noise or be detuned from the wiring.

Be sure to solder wires only on the <u>bot</u>tom of the board. A short circuit can be created by soldering on the top.

Antenna Connections.

The antenna connection should be made to the pc board with an RCA plug of the lowloss type made for rf. We sell good RCA plugs with cable clamp. See A5 plug on website.

If you want to extend the antenna connection to a panel connector, we recommend using a short length of RG-174/u coax with the plug and keep the pigtails very short.

We do **not** recommend trying to use direct coax soldered to board or another type of connector. The method designed into the board results in lowest loss practical. When soldering the cable, keep the stripped ends as short as possible.

Power Connections.

The receiver operates on +13.6 Vdc \pm 10%. Current drain is about 50 mA. A well filtered power supply should be used. There is a voltage regulator on the board.

Be sure that the power source does not carry high voltage or reverse polarity transients on the line, since semiconductors in the receiver can be damaged. The positive power supply lead should be connected to the receiver at terminal E3, and the negative power lead should be connected to the ground plane of the board through the mounting hardware or soldered to E4 ground terminal on the board. Be sure to observe polarity to avoid damage!

Optional 12Vdc Power Adapter.

The A40 adapter is rated for 12Vdc at 200 mA load. It is a filtered dc power source but is not regulated. Since there is a voltage regulator on the receiver board, a regulated power supply is not necessary, as long as it is a well-filtered supply.

The adapter actually puts out close to 18Vdc with no load and drops to about 15-16Vdc with the load a receiver presents.

To install the adapter, clip the ends of the leads off and strip them about ¼ inch. The lead with the small grooves molded into it is positive, and the smoother lead is negative.

The stripped leads can be soldered to the + power input and ground terminals of the pc board. Be sure to observe polarity to avoid damaging the receiver module. Because it is difficult to tell the ribbed lead from the smooth lead, double check before applying power to the radio to avoid damage.

Control Outputs.

The R317 has three output transistors used to turn on one or more relays. These are called Output A, Output B, and Output C, normally corresponding to 3, 5, and 7 clicks of the mic button. Each transistor can sink as much as 50mA at voltages up to +15Vdc. In other words, the transistors switch ground on and off and can be used to ground the (-) end of a relay input.

◆ CAUTION: Be careful not to exceed the voltage or current capabilities of the transistors. Also, be very careful about transients generated by inductive loads, such as relays. All mechanical relay coils must have a diode connected across the coil to absorb transients from inductive kickback, which can reach several hundred volts when the coil is switched off. See application diagrams, which follow, for examples of how to connect the diode, which basically must conduct any energy of reverse polarity; so the diode is connected

backwards from regular polarity of the power source. Therefore, the diode does not conduct unless there is a reverse voltage. NOTE THAT SOLID STATE RELAYS DO NOT HAVE A COIL; SO THEY DO NOT NEED A DIODE. SUCH RELAYS ARE PREFERRED BECAUSE THEY DO NOT PRESENT A DANGER TO THE RADIO.

The relay should be mounted in an electrical cabinet for safety. If you use a solid state relay, it should be mounted on a metal surface for proper heatsinking. For instance, our A95 relay may be operated with a load up to 4Amp at room temperature with no heatsink. For operation at elevated temperatures or for load currents over 4 Amp (up to 10 Amp), the relay needs to be heat sunk to a large metal surface, and a good size electrical cabinet should provide ample surface for that.

To provide heatsinking for the relay, it must be mounted on a bare metal surface. If necessary, a large aluminum plate can be installed in the cabinet to provide bare metal for heatsinking. Before screwing the relay to the heatsink surface, spread a very thin layer of heatsink compound on the metal relay base to transfer the heat to the heatsink.

CAUTION: Installer is responsible to ensure that proper heatsinking is provided. Warranty does not cover damage to relay which might result from improper installation.

To allow pilot control of runway lights (PCL), the three output transistors are turned on by clicking the microphone button in the aircraft, as explained later under Operation. Three clicks in five seconds turns on Output A, five clicks turns on Output B, and seven clicks turns on Output C. The outputs can be used to control relays to turn on the ac power for the lights. Think about how you want the lights to operate before wiring the outputs. There are ways to provide different options, depending on the wiring. The three outputs can be used to control relays for three levels of lighting. (More information in Operation section.)

Figure 2 shows two ways to turn on large ac loads with the receiver. The preferred method is to use a modern solid state relay which can be controlled with a small dc current and switch large ac loads. Solid state relays can be obtained from Hamtronics as an accessory. Figure 2A shows how to wire a solid state relay, with the negative side of the control input switched by the output of receiver.

The older method of switching large loads

Table 2. Connections.			
Function	Terminal		
Ground	Mtg Screws & E4		
+13.6 Vdc Power	E3		
Speaker	E2		
Relay Out A (3 clicks)	E7		
Relay Out B (5 clicks)	E8		
Relay Out C (7 clicks)	E9		
(E1, E5, & E6 normally not	used)		

is to use a small dc relay to turn on a large ac power contactor. This method is shown in figure 2B. Make sure that the smaller relay can be operated with less than 50mA of current, and be sure to place a reverse polarity diode across the coil to prevent inductive kickback from damaging the receiver. This diode can be almost any type, including 1N4148, 1N914, 1N4001.

OPERATION.

General.

The R317 has a microcontroller which is responsible for watching the squelch to determine what is happening on the air. Green LED D4, on the left, indicates when a signal is detected. Red LED D5, on the right, is used to indicate when any one, two, or three of the outputs are turned on by the receiver.

Squelch Setting.

The squelch control, which is the small trim pot on the left side of the board, sets the threshold at which signals will be detected. Green LED D4, on the left, indicates when a signal is detected. The proper way to set the squelch threshold is to turn the pot ccw until the LED comes on and then turn it cw just past the point where the LED turns off again. Of course, do this when no one is transmitting. If you have a speaker connected, you can also listen to determine when the squelch is open.

There may be installations where this default setting is too sensitive. If you get false triggering of the relay, try setting the squelch control a little more clockwise. Since aircraft normally have line of sight communications with the airport, most times a receiver does not need maximum sensitivity.

Option Switch.

Ten position dip switch S1 is used to program the microcontroller for two functions. Switch section 1 provides selection of a timer option, and sections 2-10 set the channel frequency.

Switch 1 selects an option to allow changes to be made by the pilot after initially turning on lights. If this switch is off, the re-

ceiver accepts only the first valid command until the timer expires, eg, 15 minutes. If the switch is on, the receiver will accept a new command while the timer is running, either another intensity or extending the current intensity.

Switches 2 - 10 are used to set the channel frequency. A detailed explanation appears later in the manual in alignment procedures.

Pilot Control of Lighting.

If a pilot clicks his push-to-talk button three, five, or seven times within five seconds, runway lights can be activated with Outputs A, B, and C, respectively. Depending on wiring, this can turn on runway lights at up to 3 intensity levels.

The receiver is designed to meet FAA standards, which basically say the following:

The decoder must energize 1, 2, or 3 relays upon the receipt of a series (7 pulses maximum) of electrical pulses (microphone clicks) within a 5 second period, hold the relays energized for 15 minutes, and deenergize the relays after 15 minutes.

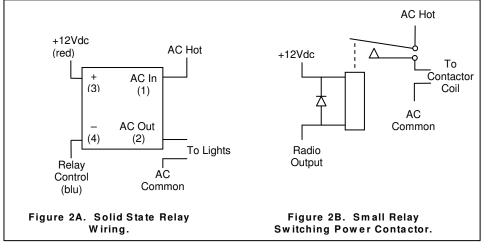
Further, a 5.0 second gate period must be started by the first pulse received. At the third pulse, the first relay must be energized. At the fifth pulse, the second relay must be energized. At the seventh pulse, the third relay must be energized.

If 2 or 3 relays are energized and a new series of pulses are received, at the third pulse, all relays except the first, must be deenergized and the timer reset for a full 15 minutes. At the fifth pulse, the second relay must be energized. At the seventh pulse, the third relay must be energized.

This option for allowing changes to be made after the initial setting is selected with dip switch #1, as previously explained.

When you install the system, carefully plan how you want the lights to respond to any possible condition. With the proper combination of programming and wiring the outputs to relays, you can make the lighting system operate smoothly and safely. Following are factors to be considered.

The three outputs can be used to control



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three different intensities of lights by turning on different electric circuits to the lights. More often, though, only a single intensity is used, especially with newer styles of lights, and any one of the three outputs can be used for the single relay to turn on those lights. Thus, by selecting which output you wire to the relay, you can require 3, 5, or 7 clicks to activate the lights.

The receiver has the option of allowing changes to the command after an initial command is executed. If the switch is on, subsequent commands will be carried out, otherwise, they will be ignored until the time delay is completed for turning off the lights. If you do not allow changes and someone, even unintentionally, sends a command, they cannot carry out another command for 15 minutes or whatever the time delay is set for.

Red LED D5 on the front of the receiver will illuminate anytime a command is in effect, that is, whenever one of the outputs is activated. Note that multiple outputs can be turned on at once. Output A (and the red LED) always comes on when the first three clicks are received. Output B comes on if 5 or more clicks are received, and Output C comes on if 7 or more clicks are received within the 5 second window.

If you have problems turning on lights.

A few users have commented that they have trouble turning on lights sometimes or that the lights turn off early. Here are a few things to consider.

The number of clicks is important. You must send exactly the correct number of clicks within 5 seconds. Requiring 5 or 7 clicks is a bit harder to send accurately than 3 clicks; so most airports use 3 clicks.

Dip switch position 1 may be turned on to permit changes to be made by the pilot after initially turning on lights. If this switch is off, the receiver accepts only the commands sent within the 5 second window beginning with the first click. After one or more outputs are turned on, no changes can be made for 15 minutes.

The receiver may also pick up signals a pilot is sending to a nearby airport if they use the same frequency you do. So always consider that a command might be coming from someone other than a pilot using your airport. It is good to use a unique channel frequency for your receiver.

If you are picking up signals from pilots far away, it may be that your receiver is too sensitive. Because aircraft have line of sight to the airport, signals can be received over a great range. Your antenna may be too effective (if you use a big antenna), or you may need to adjust the squelch sensitivity in the receiver to prevent weaker signals from activating the receiver. Refer to the section on Squelch Setting above.

FREQUENCY SETTING.

The channel frequency is determined by frequency synthesizer circuits, which use the DIP switch in conjunction with programming in the microcontroller to set the frequency. The microcontroller reads the DIP switch information and does mathematics, applying data to the synthesizer ic. Following is a discussion of how to set the dip switch to the desired channel frequency.

NOTE: If the frequency is changed more than about ± 2 MHz, a complete alignment of the receiver should be performed, as described in later text. Optimum operation only occurs if the synthesizer is adjusted to match the frequency switch setting and all the tuned amplifier circuits are peaked for the desired frequency. It is anticipated that most customers will continue to use the alignment done at the factory for the frequency they specified. There is no reason to do anything unless you need to change frequencies. Be careful not to disturb the DIP switch if you don't need to change frequencies.

To determine what channel frequency to use, the microcontroller adds the frequency information from the dip switch to the "base" frequency. The actual "base" frequency is selected and programmed at the factory depending on the frequency range needed; so if you do not know what it is, please ask.

Dip switch settings are binary, which means each switch section has a different weighting, twice as great as the next lower section. Sections have weights such as 25 kHz, 50 kHz, 100kHz, etc., all the way up to 12.775 MHz.

When done, you might want to record the switch settings in table 3 for future reference.

We make it easy by publishing a long table of possible settings on our website. Refer to the following link and be sure to type in the underscore characters...

http://www.hamtronics.com/dipswitch_R123 _R317.htm

The table online has two sections to it. The first set of listings is for a 120MHz base frequency, which our vhf receivers use. The second section can be used for this receiver, since it can be applied to any base frequency.

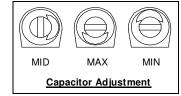
Look up the frequency, and it will give you all the binary switch settings.

ALIGNMENT.

A complete alignment is needed whenever the frequency is changed by more than about 2 MHz. Alignment ensures that the frequency synthesizer is optimized at the center of the vco range and that all stages are tuned to resonance.

Equipment needed for alignment is a sensitive dc voltmeter, a stable and accurate signal generator for the channel frequency, and a regulated 13.6Vdc power supply with a 0-200 mA meter internally or externally connected in the supply line.

The slug tuned coil should be adjusted with the proper hex tuning tool to avoid cracking the powdered iron slugs. Variable capacitors should be adjusted with a plastic tool having a small ceramic or metal bit. (See A1 Tuning Tool on our website.)



Note: Meter indications used as references are typical but may vary widely due to many factors not related to performance, such as type of meter and circuit tolerances.

a. Set the SQUELCH pot fully counterclockwise and the VOLUME pot just a little clockwise.

b. Connect speaker and +13.6 Vdc. You should hear white noise.

c. Connect voltmeter to TP1 (insert probe tip in pad on board). Adjust vco coil L1 for +2Vdc. (Although the vco will operate over a wide range of tuning voltages from about 1V to 5V, operation is optimum if the vco is adjusted to 2V.)

d. Connect voltmeter to TP2 (insert probe tip into pad). Adjust doubler variable capacitor C21 for a peak. Note: the peak will be small.

e. Adjust buffer variable capacitor C24 for a peak. This will be just a slight peaking (increase) of the voltage.

f. Adjust C32 and C33 for a peak. Then, re-peak C21, C24, C32, and C33 to ensure they are all at maximum.

g. Connect stable signal generator to TP-2. Set generator to exactly 10.7000 MHz. Use a frequency counter or synthesized signal generator so the frequency is accurate. Set level just high enough for full quieting. At 20 μ V, you should notice some quieting, but you need something near full quieting for the test (about 200 μ V).

h. Connect dc voltmeter to Discriminator pad E5. Adjust discriminator transformer T3 for +2.0Vdc.

• Be careful not to turn the slug tight against either the top or bottom because the winding of the transformer can be broken.

i. Connect signal generator to J1 using a coax cable with RCA plug. Adjust signal generator to exact channel frequency, and turn output level up fairly high to get some quieting.

Note: There are two methods of adjusting the mixer and front end. One is to use a voltmeter with test point TP-3. The voltage at this point is proportional to the amount of noise

detected in the squelch circuit; so it gives an indication of the quieting of the receiver. With SQUELCH control fully ccw, the dc voltage at TP-3 varies from -0.5 Vdc with no signal (full noise) to +0.9 Vdc with full quieting signal. The other method is to use a regular professional SINAD meter and a tone modulated signal.

In either case, a weak to moderate signal is required to observe any change in noise. If the signal is too strong, there will be no change in the reading as tuning progresses; so keep the signal generator turned down as receiver sensitivity increases during tuning.

If you use TP-3 with a voltmeter, the signal can be modulated or unmodulated. If you use a SINAD meter, the standard method is a 1000 Hz tone with 3 kHz deviation.

j. Connect dc voltmeter to TP-3. Set signal generator for relatively weak signal, one which shows some change in the dc voltage indication at TP3. Alternately peak RF amplifier and mixer variable capacitors C29, C30, and C31 until no further improvement can be made. When properly tuned, sensitivity should be about 0.3μ V for 12 dB SINAD.

● T1 and T2 adjust the crystal filter for minimum distortion. These are adjusted at the factory and should not be disturbed. If you must adjust them, inject a signal exactly on channel frequency with a 1000Hz tone and 5kHz deviation. Adjust alternately for minimum distortion.

Oscillator Trimming.

If you suspect that the TCXO needs adjustment, which normally it does not, proceed as follows.

a. First, perform steps g.and h. of the Channel Frequency Alignment procedure to be sure discriminator is set to frequency.

b. Set the service monitor for the exact channel frequency and inject a signal into the front end at J1 sufficient for good quieting.

c. Connect dc voltmeter to E5 as indicated for discriminator alignment above.

d. Use a 0.4 x 0.9mm ceramic tuning tool to adjust the small variable capacitor in the TCXO for +2V.

THEORY OF OPERATION.

The R317 is a frequency synthesized vhf fm receiver, the design of which was chosen because of its vastly superior squelch action compared to an am receiver. However, since am audio is not detected, the receiver does not allow listening to aircraft transmissions, although you can listen to hear if there is any interference. It is optimized only for control, not for monitoring audio in the normal sense. Refer to the schematic diagram for the following discussion.

Low noise dual-gate mos fet's are used for RF amplifier Q5 and mixer Q6. The output of the first mixer is coupled through a 10.700 MHz crystal filter to the second mixer, which is in U4.

U4 provides IF amplification, a 2nd mixer to convert to 455 kHz, an fm detector, and squelch. Ceramic filter FL5 provides additional adjacent channel selectivity at 455 kHz.

The output of the fm detector at pin 9 of U4 is applied to an active filter stage, which is peaked at 10,000 Hz, looking for noise when there is no signal. The noise output is detected by D3/D4 and drives the squelch detector input at pin 12. A variable dc voltage from SQUELCH pot R32 is also applied to pin 12 through a summing circuit to allow squelch threshold adjustment.

The COS (carrier operated squelch) signal from pin 13 drives the IRQ interrupt input on microcontroller U1 to indicate when a signal is detected. It also turns switch Q7 on and off to illuminate green LED D4 to indicate when a signal is present to allow the Squelch pot to be properly set.

The injection frequency for the first mixer is generated by vco (voltage controlled oscillator) Q2. The injection frequency is 10.700 MHz above the receive channel frequency. The output of the vco is doubled in Q3 and buffered by Q4 to minimize effects of loading and voltage variations of following stages from modulating the carrier frequency. The buffer output is applied through a double tuned circuit to the input of mixer Q6.

The frequency of the vco stage is controlled by phase locked loop synthesizer U2. A sample of the vco output is applied through the buffer stage and C2 to a prescaler in U2. The prescaler and other dividers in the synthesizer divide the sample down to 5kHz.

A reference frequency of 10.240 MHz, generated by a temperature compensated crystal oscillator (TCXO), is divided down to 5 kHz. The two 5kHz signals are compared to determine what error exists between them. The result is a slowly varying dc tuning voltage used to phase lock the vco precisely onto the desired channel frequency.

The tuning voltage is applied to carrier tune varactor diode D1, which varies its capacitance to tune the tank circuit formed by L1/C16/C17. C13 limits the tuning range of D1. The tuning voltage is applied to D1 through a third order low pass loop filter, which removes the 5kHz reference frequency from the tuning voltage to avoid whine.

Serial data to indicate the desired channel frequency and other operational characteristics of the synthesizer are applied to synthesizer U2 by microcontroller U1. Everything the synthesizer ic needs to know about the band, division schemes, channel selection, reference frequency, and oscillator options is generated by the microcontroller. Information about the base frequency of the band the receiver is to operate on and the channel within that band is calculated in the controller based on information programmed in the eprom on the controller and on channel settings done on dip switch S1. The microcontroller sends several bytes of serial data to the synthesizer, using the data, clock, and latch enable lines running between the two ic's.

Microcontroller U1 also provides the intelligence to control runway lights. It senses squelch openings at interrupt pin 1, and its three outputs drive switching transistors Q8, Q9, and Q10. These transistors are capable of driving external relays and may be used in other ways as described in the Installation section. Care must be used to avoid reverse polarity, overvoltage, and transients, all which can damage the transistors.

+13.6Vdc power for the receiver is applied at E3. U6 is a 5V regulator to provide stability and C57 and C58 eliminate noise. Additional filtering for the vco and buffer stages is provided by capacitance amplifier Q1, which uses the characteristics of an emitter follower to provide a very stiff supply, eliminating any possible noise on the power supply line.

TROUBLESHOOTING.

General.

The usual troubleshooting techniques of checking dc voltages and signal tracing with an RF voltmeter probe and oscilloscope will work well in troubleshooting the R317. DC voltage charts and a list of typical audio levels are given to act as a guide to troubleshooting. Although voltages may vary widely from set to set and under various operating and measurement conditions, the indications may be helpful when used in a logical troubleshooting procedure.

Current Drain.

Power line current drain normally is about 38 mA with volume turned down or squelched and up to 100 mA with full audio output.

If the current drain is approximately 100 mA with no audio output, check to see if voltage regulator U6 is hot. If so, and the voltage on the 5V line is low, there is a short circuit on that bus somewhere and U6 is limiting the short circuit current to 100mA to protect the receiver from damage. If you clear the short circuit, the voltage should rise again. U6 should not be damaged by short circuits on its output line; however, it may be damaged by reverse voltage or high transient voltages.

Audio Output Stage.

Note that audio output ic U5 is designed to be heatsunk to the pc board through the ground pins on the ic; that is why a socket is not used.

If audio is present at the VOLUME control but not at the speaker, the audio ic may have been damaged by reverse polarity or a transient on the B+ line. This is fairly common with lightning damage. If no audio is present on the VOLUME control, the squelch circuit may not be operating properly. Check the dc voltages, and look for noise in the 10 kHz region, which should be present at U4-pin 11 with no input signal. (Between pins 10 and 11 of U4 is an op-amp active filter tuned to 10 kHz.)

RF Signal Tracing.

If the receiver is completely dead, try a 10.700 MHz signal applied to TP-3 using coax test lead. Set level just high enough for full quieting. At 1 μ V, you should notice some quieting, but you need something near full quieting for the test.

You can also connect the 10.700 MHz test lead through a blocking capacitor to various sections of the crystal filter to see if there is a large loss of signal across one of the filter sections. Also, check the 10.245 MHz oscillator with a scope or by listening with an hf receiver or service monitor.

A signal generator on the channel frequency can be injected at various points in the front end. If the mixer is more sensitive than the RF amplifier, the RF stage is suspect. Check the dc voltages looking for a damaged fet, which can occur due to transients or reverse polarity on the dc power line. Also, it is possible to have the input gate (gate 1) of the RF amplifier fet damaged by high static charges or high levels of RF on the antenna line, with no apparent change in dc voltages, since the input gate is normally at dc ground.

Synthesizer Circuits.

Following is a checklist of things to look for if the synthesizer is suspected of not performing properly.

a. Check the output frequency of the vco buffer with a frequency counter.

b. Check tuning voltage at TP1. It should be about +2.0Vdc. Actual range over which the unit will operate is about +0.5Vdc to about +4.5Vdc. However, for optimum results, the vco should be tuned to allow operation at about +2.0Vdc center voltage.

c. Check the operating voltage and bias on the vco and buffer.

d. Check the TCXO at pin 1 of the synthesizer ic. A scope should show strong signal (1.5 Vp-p) at 10.240 MHz.

e. The data, clock, and latch enable lines between the microcontroller and synthesizer ic's should show very brief and very fast activity, sending data to the synthesizer ic. Because this happens very fast, it can be difficult to see on a scope. Use 1mSec/div, 5Vdc/div, and normal trigger.

Microphonics, Hum, and Noise.

The vco and loop filter are very sensitive to hum and noise pickup from magnetic and electrical sources. Some designs use a shielded compartment for vco's. We assume the whole board will be installed in a shielded enclosure; so we elected to keep the size small by not using a separate shield on the vco. However, this means that you must use care to keep wiring away from the vco circuit. Having the board in a metal enclosure will shield these sensitive circuits from florescent lights and other strong sources of noise.

Because the frequency of a synthesizer basically results from a free running L-C oscillator, the tank circuit, especially L1, is very sensitive to microphonics from mechanical noise coupled to the coil. You should minimize any sources of vibration which might be coupled to the receiver, such as motors.

Excessive noise on the dc power supply which operates the receiver can cause noise to modulate the synthesizer output. Various regulators and filters in the receiver are designed to minimize sensitivity to wiring noise.

To varying degrees, whine from the 5kHz reference frequency may be heard on the signal under various circumstances. If the tuning voltage required to tune the vco on frequency is very high or low, near one extreme, the whine may be heard. This can also happen even when the tuning voltage is properly near the 2.0 Vdc center if there is dc loading on the loop filter. Any current loading, no matter how small, on the loop filter causes the phase detector to pump harder to maintain the tuning voltage. The result is whine on the signal. Such loading can be caused by connecting a voltmeter to TP1 for testing, and it can also be caused by moisture on the loop filter components.

Typical DC Voltages.

Tables 4-6 give dc levels measured with a sensitive dc voltmeter on a sample unit with 13.6 Vdc B+ applied. All voltages may vary considerably without necessarily indicating trouble. The charts should be used with a logical troubleshooting plan. All voltages are positive with respect to ground except as indicated.

Typical Audio Levels.

Table 7 gives rough measurements of audio levels. Measurements were taken using an oscilloscope, with no input signal, just white noise so conditions can be reproduced easily.

Table 4. Typical Test Point Voltages			
TP1	Tuning V.	Normally set at 2V	
TP2	Inj Level	approx. 0.3 – 0.6V	
TP3	Noise det	With SQUELCH control fully ccw, varies from -0.3 Vdc with no to +0.9 Vdc full quieting.	
TP4/I	E5 DISC	Varies with frequency of input signal. Voltage at this point normally is ad- justed for +2Vdc with a signal exactly on fre- quency. Can vary a little without being a problem.	

Table 5. Typical Xstr DC Voltages					
Xstr	Stage	E(S)	B(G1)) C(D)	G2
Q1	dc filter	4.1	4.8	5	-
Q2	VCO	0.9	1.6	3.8	-
Q3	doubler	0	0.7	2.4	-
Q4	buffer	0	0.7	2.4	-
Q5	RF ampl	0	0	4.6	2.3
Q6	Mixer	0	0	4.9	0.3
Q7	sq. open	0	0	5	-
	sq. closed	0	0.65	0.14	-

Table 6. Typical IC DC Voltages			
U2-1	2.4	U4-1	5
U2-2	2.4	U4-2	4.4
U2-3&4	5	U4-3	4.8
U2-5	0 – 5V	U4-4	5
	(2Vtuned)	U4-5	3.8
		U4-6	3.8
U2-7	5	U4-7	3.8
U2-8	1.6	U4-8	5
U2-9	0	U4-9	2 (aligned)
U2-10	0	U4-10	0.8
U2-11	0	U4-11	2
		U4-12	0.6 (with
U5-1	1.4	squelch	i just closed)
U5-3	0.01	U4-13	0 (sq open)
U5-5	6	7.5 (squelch closed)	
U5-6	13.6	U4-14	0
U5-7	7	U4-15	0
U5-8	1.4	U4-16	1.8

Table 7. Typical Audio Voltages			
Audio Test Point	Normal Level		
U4-9 (Discriminator)	3V p-p audio		
E5 (Disc Output)	2V p-p audio		
E1 (Repeater Output)	1V p-p audio		
U4-11 (noise ampl)	3V p-p noise		
CW lug of VOL cont.	400mV p-p audio		
U5-3 (af ampl input)	0 to 200mV p-p		
U5-5 or E2 (speaker	0 to 7V p-p audio		
ampl output)			

PARTS LIST FOR R317 RECEIVER.

Note: Resistors and capacitors are 0805 or 0603 smt type unless noted otherwise.

Values shown are for 430-450 MHz range. Factory changes some values for other frequencie.

* Polarity for LED's: long lead is anode, same as electrolytic caps.

** Polarity for varicap diode D1: bar end is cathode, opposite end (anode) goes on pad next to grounding via.

*** C24, C29, C31, & C32 each have 1pf capacitor tack soldered across pads on rear of board.

Ref Desig	Value (marking)
C1	0.1µf
C2	2pf
C3	100 pf
C4	0.1µf
C5	100µf electrolytic
C6	0.15µf mylar
C7	0.01uf
C8	0.001µf
C9-C10	100µf electrolytic
C11	0.1µf
C12	390pf
C13	5pf
C14	390pf
C15	100µf electrolytic
C16	12pf
C17	47pf
C18	7pf
C19	220pf
C20	100pf
C21	4.5pf var cap
C22	2pf
C23	100pf
C24 ***	4.5pf var cap
C25	220pf
C26	5pf
C27-C28	100pf

c20 ***		DO DO	101/
C29 ***	4.5pf var cap	R8-R9	10K
C30	4.5pf var cap	R10	180Ω
C31 ***	4.5pf var cap	R11	27Ω
C32 ***	4.5pf var cap	R12	10K
C33	4.5pf var cap	R13	3.9K
C34	.0047µf	R14	470Ω
C35-C37	0.001µf	R15	47Ω
C38	7pf	R16	470Ω
C39	4pf	R17	10K
C40	7pf	R18	3.9K
C41	0.001µf	R19-R20	100K
C42	1µf electrolytic	R21	27Ω
C43	0.1µf	R22	2.2K
C44-C45	0.001µf	R23	330K
C46-C47	0.01µf	R24	22K
C48	0.1µf	R25	27Ω
C49	4.7μf electrolytic	R26	47Ω
C50	100µf electrolytic	R27	270Ω
C51	0.1µf	R28	47K
C52	68pf		
C53	220pf	R29	1K
C54-C56	0.1μf	R30	2MEG
C57	100µf electrolytic	R31	47K
C58	1µf electrolytic	R32	100K trim pot
D1	BB132 varactor diode **	R33	68K
D2-D3	MMBT3904 (used as diode)	R34	100K
D2 D3	Green LED *	R35	510K
D4 D5	Red LED *	R36	4.7K
FL1-FL4	10.7MHz crystal filter	R37	680Ω
FLI-FL4	(matched set of 4)	R38	1K
FL5	LT455DW ceramic filter	R39	22K
J1	RCA Jack	R40	100K
		R41	100K trim pot
J2	6 pin header	R42	47K
L1	1½ t. slug tuned (brn)	R43	10Ω
L2	0.22μH RF choke	R44	47K
1214	(red-sil-orn-orn)	R45	10K
L3-L4	2¾ t. air wound coil	R46	100Ω
L5	3¾ t. air wound coil	R47	470Ω
L6	4¾ t. air wound coil	R48-R50	3.3K
L7-L8	2¾ t. air wound coil	T1-T2	10.7MHz IF xfmr
L9	4¾ t. air wound coil		(T1005)
L10	2¾ t. air wound coil	Т3	455kHz IF xfmr
Q1	MMBT3904		(T1003)
Q2-Q4	MMBT5179	U1 🍧	MC9S08PA4 μP
Q5-Q6	BF998 MOS FET	U2 🍑	LMX1501A PLL
Q7-Q12	MMBT3904	U3 🍑	10.240 MHz TCXO
R1	27Ω	U4	MC3361BPD IF ampl
R2	15K		
R3	150K	U5	LM386N-1 AF output
R4	10K	U6	78L05ACD regulator
R5	1K	Y1	10.245 MHz crystal
R6-R7	27Ω		

