(M) MOTOROLA

Mobile Froducîs Division

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## Foreword

## 1. Scope of Manual

This manual is intended for the use of experienced technicians familiar with this general type of equipment. In it you should be able to find all the information you will need for installing and servicing the equipment it covers. It is current as of the publication date, and incorporates changes that have occurred since then in the form of instruction manual revisions (WMR's). (WMR's that cover production or engineering changes to the circuitry usually include corrected schematics and circuit board diagrams.)

## 2. Model and Kit Identification

Each Motorola product has an identifying model number stamped on its nameplate. In most cases, assemblies and kits that make up the product also have identifying kit numbers stamped on then. Schematics and circuit board diagrams for such kits show this same identifying number prominently in the lower left-hand or right-hand corner.

## 3. Service

Motorola's national service organization maintains one of the finest nation-wide installation and maintenance programs available to users of communication equipment. The administrative staff of this organization consists of national, area, and district service managers, all of whom are Motorola employees dedicated to giving our customers the best possible service. The organization has about 900 authorized Motorola Service Stations (MSS's) throughout the United States, each manned by one or more trained, FCC-licensed technicians.

Motorola selected each one of these independently owned and operated MSS's to service its customers. They offer Motorola maintenance either by the job (priced by time and material), or on a service contract at a fixed periodic fee. To buy a service contract for your Motorola equipment, contact your Motorola Service Representative or write to:

National Service Manager<br>Motorola Communications and Electronics, Inc.<br>1303 E. Algonquin Road<br>Schaumburg, Illinois 60196

## 4. Ordering Replacement Parts

When ordering replacement parts (components, kits, or chassis) or equipment information, include the complete identification number. If the component part number is not known, include in your order the number of the chassis or kit of which it is a part, and enough component description to identify the desired part.

In orders for crystal and channel elements, specify the crystal or channel element type number, crystal and carrier frequency, and the model number of the radio in which the part is used.

In orders for active filters, Vibrasender and Vibrasponder resonant reeds, specify type number and frequency, and identify the owner/operator of the communications system in which these items are to be used; also include any serial numbers stamped on the components being replaced.

## Replacement Parts Ordering

## MAIL ORDERS

Send written orders to the following addresses;

Replacement Parts, Test
Equipment, Crystal Service Items:
Motorola, Inc.
Communications Parts Division
Attention: Order Processing
1313 E. Algonquin Road
Schaumburg, IL 60196
Federal Government Orders:
Motorola, Inc. Communications Parts Division
Attention: Order Processing
1701 McCormick Drive
Landover, MD 20785

International Orders:
Motorola, Inc.
Communications Parts Division
Attention: International Order Processing
1313 E. Algonquin Road
Schaumburg, IL 60196

## TELEPHONE ORDERS

Replacement Parts/Test Equipment
call: 1-800-422-4210
or Federal Government orders, 1-800-826-1913

Crystal Service Items
call: 1-800-323-1570
or Illinois residents,
1-800-445-4564

## TELEX/FAX ORDERS

Replacement Parts/Test Equipment
Telex: 280127
FAX: 312-576-6285

Crystal Service Items
Telex: 433-0067
FAX: 910-277-0799

Federal Govemment orders
FAX: 301-925-2473 or 301-925-2474

## Customer Service

Replacement Parts/Test Equipment
call: 1-800-537-7007
Crystals
call: 1-800-323-0234
Parts Identification
call: 312-576-7418

## National Data Services

1711 West 17th Street, Tempe, AZ 85281
call; 602-994-6472
TWX: 910-951-1334

## GENERAL SAFETY INFORMATION

The United States Department of Labor, through the provisions of the Occupational Safety and Health Act of 1970 (OSHA), has established an electromagnetic energy safety standard that applies to the use of this equipment. Proper use of this radio will result in exposure below the OSHA limit. The following precautions are recommended:

DO NOT operate the transmitter of a mobile radio when someone outside the vehicle is within two feet ( 0.6 meter) of the antenna.

DO NOT operate the transmitter of a fixed radio (base station, microwave, and rural telephone RF equipment) or marine radio when someone is within two feet ( 0.6 meter) of the antenna.

DO NOT operate the transmitter of any radio unless all RF connectors are secure and any open connectors are properly terminated.

In addition,
DO NOT operate this equipment near electrical blasting caps or in an explosive atmosphere.
All equipment must be properly grounded according to Motorola installation instructions for safe operation.
All equipment should be serviced only by a qualified technician.
Refer to the appropriate section of the product service manual for additional pertinent safety information.
INSTALLATION SAFETY WARNING
Consider the occupants' safety when you choose a location for the radio. Do not mount the radio overhead or on a sidewall unless you take special precautions.

If someone were to remove the radio and fail to replace it properly, road shock could bump the radio loose, and the falling radio could in some circumstances cause serious injury to the driver or a passenger.

If you must mount the radio overhead or on a sidewall, give it the added protection of a retaining strap. Custom-made straps are available from Motrola National Parts. Order kit number HLN4698A (for Mitrek and MaraTrac) or HLN4697A (for SYNTOR. SYNTOR X, or SYNTOR X 9000).

## WARNING

For vehicles equipped with electronic anti-skid braking systems, see "ANTI-SKID BRAKING PRECAUTIONS" Publication, Motorola Number 68P81109E34.

## WARNING

To gain full access to the Common Circuits Board for servicing, the regulator heat sink screw must be removed. When operating the radio with the regulator heat sink screw removed, care should be taken to avoid the exposed hot flange.

## WARNING

It is mandatory that radio installations in vehicles fueled by liquefied petroleum gas conform to the following standard.

National Fire Protection Association standard NFPA 58 applies to radio installations in vehicles fueled by liquefied petroleum (LP) gas with the LP-gas container in the trunk or other sealed-off space within the interior of the vehicles. This standard requires that:

1. Any space containing radio equipment shall be isolated by a seal from the space in which the LP-gas container and its fittings are located.
2. Remote (outside) filling connections shall be used.
3. The container space shall be vented to the outside.

## FCC Requirements

The Federal Communications Commission (FCC) requires that you obtain a station license for your radio equipment before transmitting. No operating license or permit is required. The station licensce is responsible for ensuring that the transmitter power, frequency, and deviation are within limits defined by the station license.

The licensee of the station is at all times responsible for the proper operation and maintenance of the current station authorization. You must measure the power input and record the results:

- when the transmitter is first installed
- when the transmitter is changed in any way that may increase the power input
- at least once a year.

You must check the frequency and deviation of the transmitter:

- when it is first installed
- when the transmitter is changed in any way that might affect the carrier frequency or modulation characteristics.
- at least once a year.


## Service

To purchase a service contract for your Motorola equipment, or to purchase additional manuals, contact:

National Service Manager<br>Motorola Communications Group<br>1301 E. Algonquin Road<br>Schaumburg, Illinois 60196

## Safe Handling of CMOS Integrated-Circuit Devices

Many of the integrated-circuit devices used in communications equipment are of the CMOS (Complementary Metal Oxide Semiconductor) type. Because of their high open-circuit impedance, CMOS IC's are vulnerable to damage from static charges. Everyone involved in handling, shipping, and servicing them must be extremely careful not to expose them to such damage.

CMOS IC's do have internal protection, but it is effective only against overvoltages in the hundreds of volts, such as those that could occur during normal operations. Overvoltages from static discharge can be in the thousands of volts.

When a CMOS IC is installed in a system, the system's circuit elements distribute static charges and load the CMOS circuits. This decreases the vulnerability of the IC's to static discharge, but improper handling will probably cause static damage even when the IC's are so installed.

To avoid damaging CMOS IC's, take the following precautions when handling, shipping, and servicing them.

1. Before touching a circuit module, particularly after having moved around in the service area, touch both hands to a bare metal earth-grounded surface. This discharges any static charge you may have accumulated.

## Note

Wear a conductive wrist strap (Motorola Part No. RSX-4015A) to minimize the buildup of static charges on your person while you are servicing CMOS equipment.

## WARNING

When wearing a conductive wrist strap, be careful near sources of high voltage. By grounding you thoroughly, the wrist strap also increases the danger of lethal shock from accidental contact with such a source.
2. Whenever possible, avoid touching any electrically conductive parts of the circuit module with your hands.
3. Check the INSTALLATION and MAINTENANCE sections of the service manual and the notes on the schematic to
find out whether or not you can insert or remove circuit modules with power applied to the unit, and act accordingly.
4. When servicing a circuit module, avoid carpeted areas, dry environments, and the wearing of static-generating clothing.
5. Be sure that all electrically powered test equipment is grounded. Attach the ground lead from the test equipment to the circuit module before connecting the test probe. Similarly, disconnect the test probe before removing the ground lead.
6. When you remove a circuit module from the system, lay it on a sheet of aluminum foil or other conductive surface connected to ground through 100,000 ohms of resistance.

## WARNING <br> If the aluminum foil is connected directly to ground, you may get a shock if you touch it and another electrical circuit at the same time.

7. When soldering, be sure the soldering iron is grounded.
8. Before connecting jumpers, replacing circuit components, or touching CMOS pins (if this becomes necessary during the replacement of an integrated--circuit device), be sure to discharge any static buildup on your person (see Procedure 1, above). Because you can have a voltage difference across your body, you should use only one hand if you must touch the board wiring or any of the pins on the CMOS device.
9. When replacing a CMOS integrated-circuit device, leave the device in its metal rail container or conductive foam until you are ready to insert it into the pronged circuit module.
10. Connect any low-impedance test equipment such as a pulse generator to CMOS device inputs after you have applied power to the CMOS circuitry. Similarly, disconnect such low-impedance equipment before turning off the power.
11. Wrap CMOS modules in conductive material when transporting them from one area to another, even within the same room. Use wrapping material similar to that in which replacement modules are wrapped when they arrive from the factory. (You can also use aluminum foil.) Never use nonconductive material for packaging these modules.





## SYNTOR X 9000 UHF Radio Option Chart

| W12 | UHF Pre-amp |
| :--- | :--- |
| W20 | Telephone Interconnect |
| W70 | Omit Antenna, UHF |
| W71 | Omit Microphone |
| W87 | Omit Speaker |
| W90 | Omit Accessories, Smartnet, UHF |
| W101 | 22'Negative Ground Cable |
| W109 | Handset with hang-up |
| W116 | External Alarms |
| W123 | Antenna, 3.5 dB gain, UHF 406-512 |
| W124 | Antenna, 5 dB gain, UHF 406-512 |
| W125 | External option housing |
| W239 | Noise cancelling microphone |
| W268 | SECURENET code storage battery (secure-capable only) |
| W269 | Siren/Public Address |
| W304 | SECURENET proper code detect |
| W305 | 16 system/8 subfleet/64 modes |
| W306 | 15 system/16 subfleet/8 modes |
| W354 | Trunked DEK (8) |
| W355 | Trunked and MDC-1200 DEK (8) |
| W370 | MDC-1200 DEK (8) |
| W373 | Trunked DEK (16) |
| W374 | Trunked and MDC-1200 DEK (16) |
| W391 | SECURENET with Physical Security (secure-capable only) |
| W412 | MDC-1200 Selective Call |
| W470 | Emergency footswitch |
| W496 | 10' Negative ground |
| W496 | 10' Negative Ground, SECURENET |
| W589 | Public Address |
| W591 | Auxiliary Switch Panel |
| W674 | Security Housing Cable |
| W688 | Emergency pushbutton, hidden |
| W709 | 25 system/8 subfleet/ 32 modes |
| W793 | SECURENET, DVI-XL encryption |
| W795 | SECURENET, DES-XL encryption |
| W797 | SECURENET, DVP-XL encryption |
| W814 | MDC-1200 PTT ID/Emergency |
| W820 | Unlimited Private Call/Call Alert |
| W821 | Wide area coverage, AMSS |
| W822 | Dynamic regrouping |
| W826 | Omit Emergency Alarm/Call |
| W829 | 8 systems/16 subfleets/64 modes |
| W838 | Spare DVP-XL encryption |
| W839 | Spare DES-XL encryption |
| W840 | Spare DVI-XL encryption |
| W941 | MDC-1200 DEK (16) |
| W946 | Conventional phone/DTMF |
| W995 | Zone/Mode control unit |
|  |  |

## SYNTOR X 9000 UHF Performance Specifications

General

| Number of Modes | Models available in 32 mode contiguration. 64 modes optional. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Channel Resolution | Muitiples of 5.0 kHz or 6.25 kHz . |  |  |  |  |
| Squelch Options | Private-Line and Digital Private-Line coded squelch are standard and available in the same radio unit. Carrier Squelch and multiple coded squelch are optional. |  |  |  |  |
| Primary Power | $\pm 12$ VDC with a DC-isolated floating ground system. Radio supplied for operation with negativeground vehicles. Optional Cable kit permits operation with positive ground vehicles. |  |  |  |  |
| Radio Unit Dimensions | $2.65^{\prime \prime} \mathrm{H} \times 11.5^{\prime \prime} \mathrm{W} \times 16.0^{\prime \prime} \mathrm{L}(63.5 \mathrm{~mm} \times 292 \mathrm{~mm} \times 406 \mathrm{~mm})$ |  |  |  |  |
| Radio Unit weight | Approximately $22.5 \mathrm{lb}(10.2 \mathrm{~kg}$ ). Shipping weight approximately $37.5 \mathrm{lb}(17 \mathrm{~kg})$. |  |  |  |  |
| Metering | A single scale 0-50 microampere meter or Motorola portable test set can be used to measure all circuits essential to checking and adjustments. |  |  |  |  |
|  | Maximum Battery Drain (inc. std. accessories) |  |  |  |  |
| Model (series) | Frequency ( MHz ) | Minimum RF Power Output | Standby @ $13.8 \mathrm{~V}$ | Receive at Rated <br> Audio @ 13.8V | Transmit @ <br> Rated Power |
| T74KEJ/T74KXJ | 406-420 | 100W | 1.2A | 3.5A | 31 A |
| T74KEJ/T74KXJ | 450-470 | 100W Variable to 50 W | 1.2A | 3.5A | 31 A |
| T64KEJ/T64KXJ | 470-512 | 78W Variable to 39W | 1.2A | 3.5A | 31 A |
| T34KEJ/T34KXJ | 450-512 | 30 W Variable to 15 W | 1.2A | 3.5A | 12A |

## Transmitter

| Output Impedance | 50 ohms. |
| :---: | :---: |
| Spuious and Harmonic Emissions | More than 70 dB below carrier (for EIA spec. RS152B). |
| Frequency Stablility | $\pm .0002 \%$ of reference frequency form $+30^{\circ} \mathrm{C}$ to $+60^{\circ} \mathrm{C}$ ambient ( $+30^{\circ} \mathrm{C}$ reference). |
| Maximum Frequency Separation | 20 MHz without degradation for $450-470$ radios, 14 MHz without degradation for $406-420$ radios. 18 MHz without degradation for $470-512 \mathrm{MHz}$ ( 3 ranges). |
| Modulation | 15F2 and 16F3, $\pm 5 \mathrm{kHz}$ for $100 \% @ 1000 \mathrm{~Hz}$. |
| Audio sensitivity | $0.080 \mathrm{~V} \pm 3 \mathrm{~dB}$ of $60 \%$ maximum deviation @ 1000 Hz . |
| FM Hum and Noise EIA Method Companion Receiver |  |
| Audio Response | $+1,-3 \mathrm{~dB}$ of $6 \mathrm{~dB} /$ octave pre-emphasis characteristic from 300 to 3000 Hz . |
| Audio Distortion | Less than $2 \%$ @ $1000 \mathrm{~Hz}, 60 \%$ maximum deviation. |
| FCC Designation | T74FDJ: ABZ89FT4633-Licensable under FCC rules Parts 22, 74, and 90 fo r15F2, 16F3, and 16 F9 emission. T64FDJ: ABZ89FT4666 <br> T34FDJ: ABZ89FT4687 |

## Control Unit

| Dimensions (excluding mounting bracket) | $6.5^{\prime \prime} \mathrm{W} \times 3.375^{\prime \prime} \mathrm{H} \times 1.687^{\prime \prime} \mathrm{D}(166 \mathrm{mmm} \times 87 \mathrm{~mm} \times 43 \mathrm{~mm})$ |
| :--- | :---: |
| Weight | $1 \mathrm{lb}(455 \mathrm{~g})$ |
| Current Drain | 300 mA |

## Speaker

| Dimensions (excluding mounting bracket) | $5^{\prime \prime} \times 5^{\prime \prime} \times 2.5^{\prime \prime}(127 \mathrm{~mm} \times 127 \mathrm{~mm} \times 63 \mathrm{~mm})$ |
| :--- | :---: |
| Weight | $1.5 \mathrm{Ib}(680 \mathrm{~g})$ |

## SYNTOR X 9000 UHF Performance Specifications (continued)

## Receiver



## 1. Radio Features

## 1. 1 GENERAL

The SYNTOR X 9000 UHF radio including Systems 9000 options, provide the following features:

- microcomputer control
- broad-band operation
- frequency synthesis
- programmable time-out timer
- Private-Line and Digital Private-Line coded squelch
- Talkaround
- operator select Channel Scan operation
- mode select Channel Scan operation
- wide operating temperature range (from $-30^{\circ} \mathrm{C}$ to $+60^{\circ} \mathrm{C}$ )
- rugged construction that meets MIL-810D environmental specification related to rain, dust, salty atmosphere, shock, and vibration
- all solid-state, compact, modular design that simplifies radio maintenance and troubleshooting

Some of these features are discussed in the following paragraphs. More detailed information about the features and options are included in the appropriate SYNTOR X 9000 Two-Way Radio Operator's Manual.

### 1.2 CONVENTIONAL FEATURES

SYNTOR X 9000 Radio Systems operate in the conventional mode for compatibility with conventional repeater systems. Digital Private-Line (DPL) or carrier squelch (CSQ)
signalling is available. DPL coding is automatically selected (when available) by the Mode selector.

Talkaround is available in the conventional (nontrunked) mode for mobile-to-mobile communications. In conventional repeater systems, the transmit and receive frequencies are different. When Talkaround is selected, the transmitter frequency changes to the receiver frequency. All mobiles that need to communicate directly must select talkaround.

## 1. 3 MICROCOMPUTER CONTROLLED SYSTEM

Most major radio operations are controlled by an 8-bit microprocessor, a Read Only Memory (ROM) that contains the operating program, and associated support and control circuitry. This sophisticated microcomputer system is designed to simplify mobile operation.

### 1.4 BROAD BAND OPERATION

The SYNTOR X 9000 UHF radio operates over a broad band of frequencies. This band of authorized frequencies is in multiples of 5 kHz or 6.25 kHz in the following ranges.

$$
\begin{aligned}
& 406-420 \mathrm{MHz} \text { (Range 1) } \\
& 450-470 \mathrm{MHz} \text { (Range 2) } \\
& 470-488 \mathrm{MHz} \text { (Range } 3 \text { ) } \\
& 482-500 \mathrm{MHz} \text { (Range } 4 \text { ) } \\
& 494-512 \mathrm{MHz} \text { (Range 5) }
\end{aligned}
$$

The radio operates in these ranges without degradation in performance and without special "dual exciter" or "dual front end" circuits that operate on widely separated frequencies. Frequencies can be changed or added without retuning or realigning the radio.

## 1. 5 FREQUENCY SYNTHESIS

Specific radio frequencies are generated electronically by using a frequency synthesizer rather than individual crystals or channel elements. This simplifies multiple-frequency operation since frequencies can be changed or added by reprogramming the radio. The frequency synthesizer reacts in milliseconds in priority mode scanning.

### 1.6 IMPROVED TRANSMITTER•AND RECEIVER PERFORMANCE

The SYNTOR X 9000 UHF radio receives and transmits over 14 MHz (Range 1), 20 MHz (Range 2), or 18 MHz (Ranges 3-5) bandwidths without degradation. Its frequency stability is rated at +2 ppm , its transmit audio distortion less that $2 \%$. Receiver sensitivity (without a pre-amplifier) is rated at 0.35 microvolt (EIA SINAD) over the full 14 MHz (Range 1), 20 MHz (Range 2), or 18 MHz (Ranges 3-5) bandwidthṣ.

## 1. 7 PROGRAMMABLE TIME-OUT TIMER

The time-out timer causes the transmitter to stop transmission after the pre-programmed time interval. This prevents repeater or channel tie-up because of prolonged keying of the transmitter.

## 1. 8 PRIVATE-LINE OR DIGITAL PRIVATE-LINE CODED SQUELCH

The Private-Line or Digital Private-Line coded squelch is programmed as required. This feature allows mobile units to receive only the messages that use their individual system code. This reduces an operator's listening fatigue as well as the probability of missed or misunderstood messages.

### 1.9 REPEATER TALKAROUND CAPABILITY

Repeater talkaround allows direct communication between two mobile units or between a mobile radio and a portable unit. Use the Mode select rocker or a separate pushbutton [Dir] to select talkaround operation.

## 1. 10 CHANNEL SCAN OPERATION

The [Scan] button activates a pre-programmed set of Channel Scan parameters. This simplifies Channel Scan operation since it requires only one button to be used by an operator.

## 1. 11 OPERATOR-SELECT CHANNEL SCAN

Operator-select Channel Scan allows you to manually select channels for scanning. This suits operators who prefer manual Channel Scan operation to a pre-programmed scan list.

### 1.12 PRE-AMPLIFIER

The optional pre-amplifier improves the 12 dB SINAD receiver sensitivity from 0.35 microvolt to 0.2 microvolt, with a 5 dB decrease in intermodulation protection.

## 2. Electrical Characteristics

The basic SYNTOR X 9000 radios come fully equipped for operation. The units operate from a negative-ground,

12-volt DC source. A standard control unit, speaker, microphone with a hang-up bracket, antenna with a 14 -foot cable, and a 17-foot negative-ground cable kit are included.

## 2. 1 CIRCUIT BLOCKS

The SYNTOR X 9000 radio can be grouped into physical blocks: personality board, memory module, common circuits board, transmitter power amplifier, radio frequency (RF) board, directional coupler board, and internal casting. The internal casting includes a voltage-controlled oscillator (VCO), mixer, filter board (or optional pre-amplifier).

## 2. 2 FUNCTIONAL DESCRIPTION

The radio can be functionally divided into five parts: (a) microcomputer, (b) control unit, (c) frequency synthesizer, (d) receiver, and (e) transmitter. The microcomputer circuits are contained on the personality board. The frequency synthesizer circuits are contained on the personality board, RF board, and internal casting. The receiver circuits are contained on the personality board, RF board, and internal casting. The transmitter circuits are contained on the common circuits board and power amplifier. A brief description of each functional segment is provided below; further description is provided in the section associated with the circuit in question.

### 2.2.1 Microcomputer

The personality board contains the microcomputer system and code plug. The microcomputer consists of an eight-bit microprocessor, a read only memory that contains the operating program, and associated supporting and control circuitry. The microcomputer controls all operations of the radio from lighting the control panel indicators to frequency selection.

## 2. 2.2 Control Unit

The control unit has two circuit boards. One is the controller board and the other is the display board. The display board contains switch contacts and an 11 character, 14 segment display. The display is driven by a driver that receives serial data from the microprocessor on the control board.

The microprocessor contains the operating software. The EEPROM contains re-programmable customer information.

The display board contains the following:

- vacuum fluorescent (VF) display
- VF display driver
- backlight and indicator LEDs
- switch contacts

The controller board contains the following:

- microprocessor and EEPROM
- serial data link receiver and transmitter
- +5 volt regulator
- watchdog timer
- vehicle interface ports (VIPs)


## 2.2 .3 Frequency Synthesizer

The frequency synthesizer uses a phase-locked loop (PLL) consisting of a reference oscillator, a voltage controlled oscillator (VCO), a programmable divide by $3-\mathrm{or}-4$ pre-scaler, a multiplex divider, a sample-and-hold phase detector, a VCO buffer, and a loop adaptive filter.

For frequency generation control, the -microcomputer reads the proper information from the memory module and then applies it to the multiplexed-input divider via four data lines. This information is contained in six four-bit words.

A multiplexing sequence passes the six words to the divider. The divider divides the reference oscillator and VCO frequencies and generates four bits. Two of these bits (C0 and $\mathrm{C} 1)$ control a " C " counter inside the 3 -or- 4 pre-scaler. The other two bits (S0 and S1) are used by the sample-and-hold phase detector to control the loop adaptive filter. Once the mode of operation and the channel are selected, the six fourbit words stay the same. However, any mode change makes the microcomputer address different memory locations in the memory module. Consequently, the six four-bit words supply different information to the divider via the four data lines.

Microphone audio from the personality board is applied to the IDC circuitry along with the PL/DPL encode signals (if used). The IDC circuits process the audio to ensure the proper level of audio drive is supplied to the frequency synthesizer. In Private-Line/Digital Private-Line radios, the low-frequency PL/DPL encode signals from the personality board are combined with the microphone audio signal and routed to the VCO and the synthesizer reference oscillator via the deviation and compensation circuits.

### 2.2.4 Receiver

Incoming RF signals go through the filter board (or optional pre-amplifier), via the antenna relay. The filter output passes through a six-pole preselector filter then goes to the first mixer stage. The selectivity of the two filters prevents high-level out-of-band signals from degrading receiver performance.

The radio does not use receiver channel elements to generate the first mixer injection frequency. Rather, the frequency synthesizer supplies a high-side (Range 1) or low-side (Range 2-5) injection frequency that is applied to the first mixer via a three-pole injection filter.

The second mixer uses the 53.9 MHz signal and a 43.2 MHz signal from an injection tripler to generate a 10.7 MHz IF. The receiver uses two four-pole 10.7 MHz crystal filters to attenuate signals outside the predetermined receiver bandpass range. After filtering and amplification, the 10.7 MHz signal passes to the limiter/detector stage.

The squelch circuit gives the microcomputer two signals (CHANNEL ACTIVITY and SQUELCH TAIL). In the absence of an RF carrier, SQL TAIL is low and CHAN ACT is high. When an RF carrier appears, these signals switch to SQL TAIL high and CHAN ACT low. This tells the microcomputer to enable the audio stages. The faster CHANNEL ACTIVITY line is used as a preliminary indicator during Channel Scan operation, while the SQUELCH TAIL line protects the audio signals against fading.

### 2.2.5 Transmitter

The RF output generated by the frequency synthesizer at the required transmit frequency is applied to the controlled stage of the transmitter.

## 3. Radio Identification Label

The radio identification label identifies information needed for servicing the radio. Each field of information is explained by the following. The numbered items refer to Figure 1.
(1) DATE: this field identifies the date the trunking information was printed.
(2) SERIAL NUMBER (SN): this field identifies the radio's serial number.
(3) MODEL: this field identifies the radio's model number.
(4) FACTORY ORDER NUMBER (FO): this field identifies the factory sales order number.
(5) CONV: this area indicates the conventional mode information.
(6) MODE: this field identifies the specific conventional user mode number.
(7) RX: this field identifies the receive channel frequency in MHz.
(8) TX: this field identifies the transmit channel frequency in MHz .
(9) RX CODE: this field identifies the receiver PL, DPL or CSQ tone assignment.
(10) TX CODE: this field identifies the transmitter PL, DPL or CSQ tone assignment.
(11) T/A: this field identifies the transmit talk around frequency in MHz
(12) TOT: this field identifies the time-out timer value.
(13) PR1: this field identifies the first priority scan selection.
(14) PR2: this field identifies the second priority scan selection.
(15) SQL DATA: This field identifies the squelch data selection.
(16) SCAN: this field identifies the modes scan list.
(17) RADIO NAME: this field identifies the radio name assigned at time of order processing.
(18) RADIO SERIAL NUMBER (RSN): this field identifies the original radio serial number when replacement codeplugs have been ordered.


Figure I. SYNTOR X 9000 UHF Radio Identification Label

## Mobile Products Division



GPW-2538-A
Figure 1. Typical Systems 9000 Control Unit

1. General

The SYNTOR X 9000 mobile radio system consists of:

- remote mountable radio
- control unit (conventional or dual operation)
- microphone
- speaker
- antenna
- interconnecting cable -

The mobile units come with Systems 9000 control units that meet the basic requirements for conventional or trunking operation.

The Systems 9000 Control Unit includes the following controls and indicators:

- Power on/off slide switch
- DIM button for display brightness
- Rocker switch volume control
- Rocker and keypad mode-select control
- Channel BUSY indicator light
- XMIT (transmit) indicator light
- Priority channel indicator light
- Nonpriority channel indicator light
- Squelch button to set volume and monitor
- channel activity
- Option control buttons and indicators


## 2. Radio Operation

## 2. 1 ALERT TONES

The following alert tones aid the operator by indicating unique system conditions:

- Illegal Mode- A low pitched tone that indicates an invalid button position has been selected.
- Time-Out Timer alert (optional) - A low pitched continuous tone that indicates your present transmission will soon be disabled.


## 2. 2 TO RECEIVE

Perform the following steps to adjust your radio for operation.
(1) Slide the power ON/OFF switch to the left until it locks in position. The Control Unit display comes on showing "SELF CHECK" for two to three seconds, then displays the current selected mode. If the radio system fails its diagnostics on power up, an error code displays. See the Maintenance and Troubleshooting section of this manual. If the failure is critical, the radio ceases operation.
(2) Select a mode on which to operate.
(3) For modes with PL/DPL, turn squelch on.
(4) Adjust the volume level to a comfortable listening level during an incoming signal.

## 2. 3 TO TRANSMIT

With the radio switched on, perform the following steps to transmit on your radio system.
(1) Select the desired channel with the [Mode] rocker.
(2) Lift microphone off-hook. Press and hold the microphone PTT button.
(3) When the red transmit indicator lights, hold the microphone about two inches from your lips, speak slowly into the microphone in a normal voice, state your FCC call sign, and continue with your message. Release the microphone PTT button to receive.

## 3. Mode Select

Use the [Mode] rocker switch to scroll forward and backward through the list of programmed modes. Modes can be field programmed with user defined names. Mode names may have up to 11 characters. However, if you allow three digits for a mode number and eight digits for the mode name, both name and numeric mode association is possible.

## 4. Channel Scan

The Channel Scan feature allows you to scan a previously defined list of conventional modes for activity. If no activity exists, the display shows your selected mode. When a scanned mode becomes active, the display shows the active mode; the appropriate priority (PRI) or non-priority (NONPRI) indicator lights; and the radio unmutes.

Press the [Scan] button to turn Channel Scan on or off. With scan on, the previously selected scan list enables, and the red indicator lights.

## 4. 1 MODE SLAVED SCAN

On mode select scan radios, the scan list is pre-programmed and may not be modified. When scan activity occurs, the currently active mode number or name displays, the appropriate priority (PRI) or non-priority (NON-PRI) indicator lights and the radio unmutes.

Press the [Scan] button to turn Channel Scan on and off. The internal scan list is enabled for the selected mode when scan is on, and the Channel Scan indicator lights.

## 4. 2 OPERATOR SELECTABLE SCAN

On models with Operator Selectable Scan, you may review the scan list and/or modify it by holding the [Scan] button until an alert tone (beep) sounds and the red indicator blinks. Enter your new scan list by using the [Mode] rocker to locate the mode name, or by selecting a mode number with the keypad. Once the desired mode displays, press the [Sel] button to add it to the list.

Press the [Sel] button once to add the new mode as a nonpriority list member (NON-PRI lights), press [Sel| a second time to add the new mode as a second priority list member (PRI lights), or press [Sel] three times to add the new mode as a first priority list member (PRI blinks).

You may remove modes from your list or review your scan list. Press the [Del] button to remove modes from your scan list. Review the scan list by pressing the $[\mathbf{R c l}]$ button.

Press the [Home] button to exit the Scan list entry mode and return to normal operation.

## 4. 3 DYNAMIC PRIORITIES

The Dynamic Priority feature allows you to modify the priority of a scanned mode using the [Sel] button. Press [Sel] during mode activity to temporarily assign a NON-PRI mode to second (PRI lights) priority.

Restore the scan list to the normal priority assignments by turning Scan off and on, changing modes, pressing [Rcl], or turning the radio off and on.

## 4. 4 NUISANCE DELETE

A NON-PRI mode in the scan list that becomes too active or you no longer desire may be temporarily deleted by the [Del] button during mode activity.

Press the [Rcl] button, turn Scan off and on, change modes, or turn the radio off and on to restore a temporarily deleted mode to your scan list.

Priority modes may not be temporarily deleted.

## 4. 5 TALKBACK SCAN

Talkback Scan allows you to transmit on the last active received mode, regardless of the selected mode on the control unit.

MOTOROLA

## Mobile Products Division



Figure 1. Installation Planning
GPW-3285-A

## 1. Pre-Installation Tests

Although the factory aligns the equipment accurately, mishandling in transit may disturb some of the adjustments. In any case, FCC regulations require the checking of transmitter frequency and deviation at the time of installation. Therefore a pre-operational check is mandatory. To make a complete check, follow the sequence of tests presented below. The tests are described in more detail in the Maintenance and Troubleshooting Section of this manual.
(1) Check the highest transmit frequency (highest repeater frequency) and adjust as required. This adjustment also corrects any receive frequency errors caused by the reference oscillator.
(2) Measure the transmitter power output at the highest transmit frequency, and make adjustments as required.
(3) Measure the transmitter deviation at the highest transmit frequency (highest repeater frequency) and make the necessary adjustments.
(4) Measure the transmit frequencies.
(5) Measure the receive frequencies.
(6) Measure the 20 dB -quieting signal levels.
(7) Mcasure the PL or DPL sensitivity in PL/DPL modes. Repeat Steps 4 through 7 for each mode.
(8) Check the VSWR of the antenna after installing it in the vehicle.

## 2. Installation Planning

See Figure 1 for information on the antenna location, opcrator's controls, radio location, control and power cable routing, transmitter control power lead, receiver control power lead, primary power connections. and other accessories.

## WARNING

For vehicles equipped with electronic anti-skid braking systems, see the "Anti-Skid Braking Precautions," Motorola publication number 68 P 81109 E 34 . This document is available free of charge.

## 2. 1 ANTENNA LOCATION

The best location for the antenna is at the center of the vehicle roof. A good alternate location is at the center of the trunk lid. Be sure that the antenna cable can be acceptably routed to the radio before mounting the antenna. See the antenna instruction manual for details.

## CAUTION

Antennas must be installed at least two feet ( 0.6 meter) from vehicle operators and passengers unless shielded by a metallic surface.

## 2. 2 RADIO LOCATION

In most vehicles, the best location for the radio unit is the floor of the trunk compartment. When considering location, make sure to protect the radio from dirt and moisture. Make sure there is sufficient space around the radio to allow adequate cooling and permit removal of the unit.

## 2. 3 OPERATOR'S CONTROLS

Recommended mounting surfaces for the control unit, microphone hang-up clip, and speaker are the following: under the dashboard, on the transmission hump, or on the center console. The speaker may be mounted on the firewall.

Adjustable trunnions are supplied for mounting the control unit and the speaker, allowing a number of mounting positions. The installation must not interfere with the operation of the vehicle or its accessories, nor disturb passenger seating or leg room. The control unit and the microphone hang-up clip must be within convenient reach of the user(s).

## TRUNK COMPARTMENT

CAUTION
A good chassis connection via the black primary power cable is essential for radio operation and to prevent damage to the radio and cable kit. Connection to the vehicle frame is desir-


[^0]Figure 2. Cabling Interconnection Diagram


Figure 3. Power Control Isolation Detail

## 2. 4 CONTROL AND POWER CABLE ROUTING

Many vehicles have wire troughs in the door sills. If the vehicle has this feature, use the troughs to provide maximum protection for the cable and to simplify the cable installation.

In vehicles without wiring troughs, route the control and power cables where they are protected from pinching, sharp edges, and crushing. One suggested route is along one side of the drive shaft hump under the carpet. Use grommets where the cable passes through holes in metal panels.

## 2. 5 PRIMARY POWER CONNECTIONS (RED)

The best power connection point for the battery hot primary power lead is at the battery hot terminal. Points that connect directly to the battery terminal with sufficient cur-rent-handling capabilities may also be used. Make certain that the point chosen remains close to 13.6 volts; some systems switch to a higher-than-normal voltage during starting.

## 2. 6 TRANSMITTER CONTROL POWER LEAD (ORANGE)

Connect this lead to the ignition switch (recommended) or directly to a battery hot supply. Sce Figure 2.

## 2. 7 RECEIVER CONTROL POWER LEAD (GREEN)

Connect this lead to a battery hot supply (recommended) or to the ignition switch. See Figures 2 and 3.

## 2. 8 RADIO CHASSIS PRIMARY POWER CABLE (BLACK)

The radio chassis primary power cable should connect to a good ground point on the vehicle chassis. See Figure 2.

## 3. Cable Routing

## Note

Cables routed near metal edges or through holes may be damaged. Be sure to use rubber grommets, if necessary, to protect the cables.
(1) Determine the radio's location in the trunk compartment and leave enough slack cable to permit the plug to be easily connected or disconnected from the radio.
(2) Work from the trunk space forward. In some cars there is enough room below the fiberboard trunk partition to admit the cables. If this is not the case, make an opening through the partition. Remove the back seat.
(3) If the vehicle has wire troughs, run the cables in the wire troughs. Otherwise, route the cables under the floor covering alongside the drive shaft hump. Pull the cables into the back seat area, under the floor mats, under the front seat, and under the front mats, exiting up under the dash at the firewall. Pull the control unit end of the multi-conductor cable to the approximate location of the control unit. Route the red power cable into the engine compartment through any convenient hole in the firewall.


Figure 4. Fuse Installation

## parts list

HLN4952A Fuse Kit for Green and Orange Leads $\quad$ MXW-2273-A

| REFERENCE <br> SYMBOL. | MOTOROLA <br> PART NO. | DESCRIPTION |
| :--- | :--- | :--- |
|  | $14-82882 A 01$ | insulator, fuse hoder body |
|  | $14-828883 A 01$ | insulator, fuse holder cap |
|  | $29-00136968$ | lug |
|  | $29-00824456$ | ring tongue lug |
|  | $29-00865065$ | ring tongue lug |
|  | $41-82885 A 01$ | compression fuse spring |
|  | $42-82884 A 01$ | fuse clip |
|  | $65-00020404$ | 3 amp fuse, 250V, (quantity 2) |



Figure 5. Fuseholder Assembly and Parts List
(4) Pull the red power cable into the engine compartment. A cable fuse kit comes with a ring tongue lug on one end and an in-line fuseholder on the other. Each cable includes a small section of heat-shrinkable tubing. Trim any excess length of red cable. Slide the heat-shrinkable tubing over the red power lead from the radio. Slide the strapped portion of the red cable into the end of the in-line fuseholder and crimp the joint using a Burndy Model Y10B (indent " $U$ " crimp). If this tool is not available, solder the joint. See Figure 4.
(5) Slide the heat-shrinkable tubing over the connection and shrink the tubing with a Motorola Model ST 697 Heat Gun or equivalent heated air source. Remove the fuse from the fuscholder and reconnect the holder. Fasten the ring-tongue lug on the end of the cable to the battery's ungrounded terminal or to some point directly connected to the ungrounded terminal of the battery (such as the starter solenoid). Move the in-line fuseholder to a convenient location on one of the sheet metal parts of the engine compartment. Center punch and drill a $9 / 64^{\prime \prime}\left(.140^{\prime \prime}\right)$ hole through the mounting surface. Then
mount the bracket with the $\# 10-16 \times 1 / 4$ self-tapping sheet metal screws. Do not install the fuse until the entire radio installation is complete.
(6) The control unit power cable kit contains two separate wires, one orange and the other green. The orange wire is 66 inches long and the green wire is 106 inches long. A fuse kit hardware bag comes with the radio. This bag contains crimpon type ring tongue lugs and crimp-on type spade lugs. The spade lugs allow connection to hot leads at the fuse block of the vehicle and the ring tongue lugs permit attachment to screws of terminals. Determine from Table 1 which radio functions are to be switched through the vehicle ignition switch. A typical system allows the receiver to operate with the radio switched on while the ignition is off, but the transmitter does not operate unless the ignition is on. In this case, connect the orange wire to the accessory terminal of the ignition switch and the green wire to the ungrounded terminal of the battery or starter solenoid.

NOTE:
RADIO FITS TRAY VERY TIGHTLY FOR GOOD ELECTRICAL PERFORMANCE DURING VIBRATION. TO INSTALL RADIO, SET IT IN TRAY AND PUSH IT TOWARD REAR OF TRAY UNTIL IT ENGAGES REAR TABS FULLY. CHECK THAT FRONT TABS HAVE ENTERED OPENING IN RADIO AND THAT HANDLE PROJEC. TIONS WILL ENGAGE THEM. PUSH HANDLE CLOSED TO LOCK.


Figure 6. Radio Mounting Tray

## CAUTION

Do NOT connect either lead to the ungrounded terminal of the battery at this time.
(7) If either wire is to be connected in the engine compartment, pass the end of the wire through the same firewall hole that the red power cable uses. At this point, install a fuse in both wires.
(8) The following procedures apply to both the green and orange wires. See Figure 5 for more information. Cut the wires about 10 inches from the end. Strip the insulator from both sides so that about $1 / 8$ inch of the wire is exposed. On the end still connected to the cable kit, install the plastic insulator fuse holder cap. On the same wire, crimp one of the metal fuse clips onto the exposed wire and apply solder for a good connection. On the 10 -inch loose wire, crimp another metal fuse clip onto the exposed wire and apply solder. Install the fuse (both are three-amp) into the fuse clips on both sides. Slide the spring on the wire to the fuse. Then slide the plastic insulated fuse-holder over the loose end of the wire so that the spring is inside the fuseholder. Now, twist the fuseholders until they lock together.
(9) On the loose ends of the green and orange wires, strip the insulator and crimp either the spade or ring tongue lug on the wire. Solder the crimped connection.
(10) Do not dress the wires at this time. Go to the next procedure.

## 4. Radio Installation

(1) Choose a location where the mounting screws are not directly above the fucl tank, fuel line, or other vital parts. Permanently install the mounting tray of the radio to a flat surface with a four-point mounting scheme or, if on an uneven surface, with a three-point mounting scheme. (Four-point mounting is strongly recommended over three-point, especially in vehicles subject to extreme vibrations.) The raised shelf in some car trunk compartments makes a good mounting place. Place the radio at one side to allow space for luggage. Leave at least eight inches in front of the radio so that the handle can be opened and the programming cable can be plugged into the radio. Locate the radio so that the black ground lead in the trunk can reach a good chassis ground point in the trunk. Determine the radio`s final position, unlock the radio, open the handle and lift the radio assembly away from the mounting tray (pull forward and upward to release the radio assembly). Use the mounting tray as a template to mark the location for drilling four mounting holes in the trunk floor. Use a \#11 drill (.191). Mount the mounting tray as illustrated in Figures 6 and 7.
(2) When mounting the radio securely to the trunk floor in some vehicles, the front panel may press against the floor or floor cushioning. Also, some vehicles make it necessary to mount the radio directly over the fuel tank. Always make a preliminary check to see how far the screws will extend below the trunk floor. Do not puncture the fuel tank. If either condition exists, insert one of the thick spacer washers between the bottom of the mounting tray and the thin spacer washer at each of the four mounting holes. The washers help to keep the radio level, especially when the floor is covered with a "spongy" mat such as soft rubber. Replace the radio assembly by sliding the radio onto the tray at about the halfway point. Push straight back until the tray tabs enter the two window areas on the radio front and engage the handle tabs. Close by pushing the handle until it locks. The handle locks the radio to the mounting tray and conceals the top cover release button. Push the multi-conductor plug onto the male connector and rotate the thumbscrew clockwise to fully seat the connector. Reverse the procedure for removing the radio.
(3) Thoroughly clean the trunk floor surface before proceeding. Connect the black ground cable lug to a convenient location on the trunk floor. Center punch and drill a $3 / 16^{\prime \prime}\left(.187^{\prime \prime}\right)$ hole through the mounting surface. Use the supplied \#14 x $3 / 4$ " self-tapping screw and $1 / 4$ " lock washer to mount the cable lug. See Figure 8.


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Figure 7. Radio Mounting Tray Installation Detail


Figure 8. Radio Ground Connection

## CAUTION

A good ground connection of the black cable is essential for radio operation and to prevent damage to the radio and cable kit. Grounding to the vehicle frame is desirable. On some late-model automobiles, the ground connection between the vehicle chassis and engine block is inadequate for good mobile radio operation. DO NOT compensate for this problem by connecting the radio ground directly to the battery. Connect a flexible metal ground strap between the engine block and a vehicle chassis point common to the radio ground. Be sure the strap is heavy enough to carry maximum transmitter supply current.
(4) All cables (including the antenna lead-in) should be dressed out of the way as much as possible to prevent damage. Mount the radio so the heatsink has the largest available air supply for cooling.

## 5. Microphone Installation

The microphone bracket must be within arm's reach of the operator. Measure this distance before actually mounting the microphone bracket. Since the bracket has a positivedetent action, the microphone can mount in almost any position. See the microphone instruction manual for more information.

After installation, connect the microphone plug to the receptacle on the control unit. Make sure that the clip on the control unit firmly engages the plug. Connect the microphone cable " S " hook to the proper hole in the strain relief clip on the rear of the control unit.

## 6. Speaker Installation

## 6. 1 GENERAL

The speaker kit includes a trunnion bracket that allows the speaker to be mounted in a variety of ways. With the trunnion bracket, the speaker can mount permanently on the dashboard or in accessible firewall areas. The trunnion allows the speaker to tilt for best operation.

### 6.2 INSTALLATION WITH TRUNNION BRACKET



Figure 9. Standard Speaker Mounting
(1) Remove the trunnion bracket by loosening the two wing screws.
(2) Remove the three paper retainers and screws from the trunnion bracket.
(3) Remove the wall-mount bracket from its taped position on the hanger bracket. (Retain for future use.)
(4) Select a mounting position. If space limitations require the removal of the hanger bracket, remove the Phillips screw and slide the bracket out of the speaker housing. You need not disassemble the speaker housing to remove the hanger bracket.
(5) Using the trunnion bracket as a template, mark the location of the three mounting holes.
(6) Center-punch and drill a 0.101 -inch (\# 38 drill) hole at each location.
(7) Mount the trunnion bracket with the supplied screws.
(8) Remount the speaker in the trunnion bracket and tighten the two wing screws.
(9) Plug the speaker lead into the control unit, making sure that the plug is solidly seated.
(10) Tie up surplus lead cable.

## 7. Control Unit

## 7. 1 MOUNTING CONSIDERATIONS

Examine the vehicle to find a suitable mounting location within the operator's reach. Although the trunnion mounting bracket can mount on a plastic dashboard, all four trunnion mounting screws should penetrate the dashboard's supporting metal frame. If that is not possible, use a metal backing plate (not supplied) to strengthen the installation. The location should be convenient to the operator for viewing the display and operating the buttons and on-off switch, but vehicle operation should not be impaired and the driver's vision must not be obstructed.

If necessary, pull more cable into the dashboard area. Be sure all wires are clear of the instrument panel where holes are to be drilled.

### 7.2 INSTALLATION

(1) Mark the mounting location (see Figure 9) using the trunnion bracket as a template; drill four 5/32" holes. If mounting into a plastic surface, use a metal backing plate.
(2) Attach the trunnion bracket using all four \#10-16 $\times 5 / 8$ " self-tapping screws supplied in the mounting kit.

## Note

When the control unit is installed, it must not wobble or feel "spongy" when you press buttons. Use all four mounting screws and be sure they are tightly screwed into metal-either a dashboard support bracket or a backing plate.
(3) Plug in the radio cable connector and microphone cable connector in the proper location on the back of the control unit (sec Figure 11). A "click" sounds when the connector snaps into place. Now connect the microphone cable " $S$ " hook into the hole in the cable strain relief bracket on the back of the control unit.
(4) Plug in the Vehicle Interface Port (VIP) connector (see Figure 11) into the remaining location on the back of the control unit.
(5) Install the control unit to the trunnion bracket using the two wing screws. Rotate the control unit to the desired vertical position and tighten the wing screws.

## 8. Vehicle Interface Port (VIP)

## 8. 1 GENERAL

The Vehicle Interface Port (VIP) allows the control unit to operate outside circuits and to reccive inputs from outside the control unit. There are three VIP outputs which are used for relay control. There are also three VIP inputs which accept inputs from switches. See the cable kit section for typical connections of VIP input switches and VIP output relays.

### 8.2 OUTPUT CONNECTIONS

The VIP output pins are on the back of the control unit below the area labeled "VIP." Use these connections to wire control relays. One end of the relay should connect to switched $\mathrm{B}+$, while the other side connects to a software controlled ON/OFF switch inside the control unit. The relay can be normally-on or normally-off depending on the VIP outputs' configuration. The control unit has 3 VIP output connections.

| VIP OUTPUT | SWITCHED B + | ON/OFF SWITCHED |
| :---: | :---: | :---: |
| NUMBER | PIN NO. | PIN NO. |
| 1 | 18 | 2 |
| 2 | 19 | 1 |
| 3 | 35 | 34 |

The function of these VIP outputs can be field programmed in the control unit. Typical applications for VIP outputs are external hom/lights alarm and horn ring transfer relay control. For further information on VIP outputs, see the control unit programming manual.

## 8. 3 INPUT CONNECTIONS

The VIP input pins are on the back of the control unit below the area labeled "VIP." These connections control inputs from switches. One side of the switch connects to ground while the other side connects to a buffered input to the control unit. The switch can be normally-closed or normally-open depending on the VIP inputs' configuration. The control unit has 3 VIP input connections.

| VIP OUTPUT <br> NUMBER | GROUND <br> PIN NO. | ON/OFF SWITCHED <br> PIN NO. |
| :---: | :---: | :---: |
| 1 | 20 | 4 |
| 2 | 21 | 3 |
| 3 | 36 | 37 |

The function of the VIP inputs can be defined by field programming the control unit. Typical applications for the VIP inputs are for a foot switch or a horn ring switch. For further information on VIP inputs, see the control unit programming manual.


Figure 10. VIP Connector Detail


GPW-3006-A
Figure 1I. Control Unit Installation Exploded View

## 9. Power Connections (See Figures 1 and 2.)

(1) Replace the fuse in the in-line fuseholder of the red power cable coming from the radio in the trunk. Connect the green (and/or orange) fused wire(s) coming from the control unit to the ungrounded terminal (or source) of the battery.
(2) Pull all excess cabling into the trunk. Clamp the cables to the vehicle body or chassis with the cable clamps supplied. Drill $1 / 8^{\prime \prime}$ mounting holes and then attach the clamps with four \#8 x $3 / 8^{\prime \prime}$ tapping screws and four $1 / 4$ " lockwashers. Finally, be sure all in-line fuses are installed.

## 10. Antenna Installation

A diagram and complete installation instructions are supplied with each antenna ordered. See those installation instructions for pertinent information.

## 11. Conclusion of Installation

(1) Be sure the control unit and microphone PTT switches are off. Install the 40 -amp fuse in the red primary power cable
in-line holder. Install the 3 -amp fuse in the orange cable inline holder. Install the 3 -amp fuse in the green cable in-line holder.

## Note

If alternator or other noise is present in the received signal or in the transmission, see Motorola publications Number 68P81109E33 "Reducing Noise Interference" in Mobile Two-Way Radio Installations."
(2) Turn the radio on at the control unit and verify proper operation of all controls and indicators. Radio operation in some installations requires turning on the ignition. See Table 1. Perform a complete operational check of the radio.
(3) Dress the control and power cables out of the way to prevent damage (pull any excess cable into the trunk area) and secure them where necessary with the clamps and screws supplied. Replace the rear seat if it was removed for installing the cables.

Table 1. Radio Functions Connections

| Conductor | Green | Orange | Green | Orange | Green | Orange |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Connected to battery | $\bullet$ | $\bullet$ | $\bullet$ |  |  |  |
| Connected to <br> ignition switch |  |  |  | $\bullet$ | See Note | $\bullet$ |
| Ignition switch <br> controls | No ignition switch <br> control | Xmtr ignition switch <br> controlled | Complete radio ignition <br> switch controlled |  |  |  |

In any application, trim and strip wires. Crimp on ring lug for battery connections. For ignition switch connections, crimp on ring or spade lug (whichever is required).
Note: In cases where alternator whine or interference is a problem, isolate the green fead with a relay (Motorola Part No. 59-00813674).

Maintenance and
Mobile Products Division


GPW-4274-A
Figure 1. Typical SYNTOR X 9000/9000E Radio (Top View)

Table 1. Test Equipment

| General type | Application | Recommended Model | Minimum Specification |
| :---: | :---: | :---: | :---: |
| AC-DC VOM | DC Voltage measurements, general | Motoroia T1009A | Measurement range: $0-15 \mathrm{~V}$ dc Sensitivity: 20,000 ohms/volt |
| DC Multimeter | DC voltage readings requiring an input resistance meter | Motorola S1063B | Measurement range: $0-15 \mathrm{~V}$ dc Input resistance: 11 megaohms |
| AC Voltmeter | Audio voltage measurements | Motorola S1053C | Measurement range: 100 mV ac input resistance: 1 megaohm |
| RF Voltmeter | RF voltage measurements | Motorola S1339A | Measurement range: $100 \mu \mathrm{~V}-3 \mathrm{~V}$ from $1 \mathrm{MHz}-900 \mathrm{MHz}$ Inputs:50 ohm and high impedance |
| Oscilloscope, Dual-Trace | Waveform observation | Motorola R1004A | Vertical sensitivity: $5 \mathrm{mV}-10 \mathrm{~V}$ /division Horizontal time base: $0.2 \mu \mathrm{sec}-$ $0.5 \mathrm{sec} . /$ division |
| RF Wattmeter | Transmitter output power measurement | Motorola T1039 with appropriate element and T1013 RF dummy load | Measurement range: 0-50 watts |
| Frequency Meter | Transmitter frequency measurement | Motorola R1200 Service Monitor with high stability osciltator (X suffix) option. Frequency calibration recommended every 6 months or less. | Measurement range: $806-870 \mathrm{MHz}$ Frequency resolution: 10 Hz |
| Deviation meter | Transmitter modulation deviation measurement | Motorola R1200 Service Monitor with SLN6350 Deviation Meter. | Measurement range: $0-10 \mathrm{KHz}$ deviation <br> Frequency range: $806-870 \mathrm{MHz}$ |
| RF Signal | Receiver alignment and troubleshooting | Motorola R1200 Service Monitor with attenuator. | Frequency range: $806-870 \mathrm{MHz}$ <br> Output level: $0.1 \mu \mathrm{~V}-100,000 \mu \mathrm{~V}$ <br> Must be capable of at least $\pm 3 \mathrm{kHz}$ deviation when modulated by a 1 kHz tone |
| Audio Signal Generator | Audio circuit troubleshooting | Motorola S1067B | Frequency range: $20 \mathrm{~Hz}-20 \mathrm{kHz}$ Output level: 50 mV - 1 V |
| -Double- <br> Balance Mixer | Receiver front-end adjustment | Mini-Circuits Laboratory Model ZAD-4 | - |
| -Logic Probe | Check various digital devices | Motorola RLT-4014 | - |
| Radio Test set | Meter readings at circuit metering points for alignment and troubleshooting | Motorola S1056 Portable Test Set with a TEK-37 or TEK-37A Test Set Adapter or a Motorola TEK-5 Meter Panel with a TEK-40 Cable. | - |
| -Tuning Tool Kit | Receiver and transmitter alignment | Motorola TRN4513A | - |
| -DC Power Supply | DC power for shop service | Motorola R1011AA | $\begin{aligned} & 120 \mathrm{vdc} \\ & 0-40 \mathrm{~A} \end{aligned}$ |
| PL Tone Generator* | Tone coded "Private-Line" decoder troubleshooting | Motorola S 5133 B | Frequency range: $10 \mathrm{~Hz}-9999 \mathrm{~Hz}$ Output level: 0-3V rms |
| $\begin{aligned} & \text { DPL Test } \\ & \text { Set }^{\star \star} \end{aligned}$ | "Digital Private-Line" encoderdecoder troubleshooting | Motorola SLN6413A | - |

## Note

All the test equipment listed above, with the exception of those marked with (•), can be replaced with the Motorola R2001 System Analyzer

## CAUTION

In positive-ground systems, the case of the TEK-5 Meter Panel and portions of the S1056B Portable Test Set are hot with respect to the vehicle chassis due to the nature of the positive-ground installations. Take necessary precautions that the test equipment does not contact the vehicle chassis.


GPW-4199-B
Figare 2. Typical SYNTOR X 9000/9000E Radio (bottom vicw)
2. Radio Alignment and Adjustments

## 2. 1 INTRODUCTION

The following four adjustments can be made to the SYNTOR X 9000 radio:

- oscillator frequency
- deviation
- compensation
- transmitter power

Perform all adjustments through the holes that are directly accessible on the RF board. (See Figure 1). Readjustment of the receiver is not recommended since the factory ad-
justs the receiver to allow a wide passband for all frequencies within the radio model's range.

## Note

See the list of recommended test equipment provided in this section of the manual.

## 2. 2 OSCILLATOR FREQUENCY

Note
Perform the oscillator frequency adjustment before setting or checking the deviation adjustment.
(1) Use the mode rocker to set the radio on a carrier squelch transmit mode when adjusting the oscillator frequency.
(2) Use the portable test set to key the transmitter without modulation.
(3) Adjust the reference oscillator warp control (Figure 1) until the proper indication is obtained on the frequency meter.
(4) Use the mode rocker to scroll to all the remaining positions and check the proper transmitter frequencies. (No further oscillator frequency adjustments are required.)

### 2.3 DEVIATION

## Note

Check deviation on all transmit channels when setting deviations; especially if wide transmit separations (more than 5 kHz ) are required.
(1a) For PL or DPL radios only: Use Table 2 to determine the target closest to, but less than the customer's PL or DPL transmit frequency. Use the deviation adjust potentiometer, to set deviation on the selected transmit frequency.

Table 2. Deviation Adjustment Target Frequencies

| RANGE | FIRST | TARGET (MHz) |
| :---: | :---: | :--- |
| 1 | 412.8 | 420 |
| 2 | 459.6 | 470 |
| 3 | 478.7 | 488 |
| 4 | 490.7 | 500 |
| 5 | 502.7 | 512 |

(1b) For radios without PL or DPL: Use Table 2 to determine the target closest to, but less than the customer's transmit frequency. Use the deviation adjust potentiometer, to set deviation on the selected transmit frequency.
(2) Check the deviation on all transmit frequencies to ensure that it does not exceed 5 kHz on any of them.

## 2. 4 COMPENSATION

## Note

The compensation adjustment potentiometer is set at the factory and does not normally require readjustment.

Use this compensation adjustment procedure when any of the following conditions occur.

- if DPL transmit (encode) performance is poor
- if the VCO reference oscillator or common circuits board is replaced
- if the compensation potentiometer is replaced or inadvertently adjusted.


### 2.4.1 Radios with PL or DPL

This procedure balances the transmit audio signal fed to the VCO and reference oscillator. This insures good DPL waveform fidelity and flat modulation response.
(1) Turn the deviation potentiometer (Figure 1) one-half turn clockwise.
(2) Set the mode selector switch to the PL/DPL customer transmit frequency closest to the radio's first target frequency in Table 2.
(3) Connect the center lead of the shielded cable of an AC voltmeter to the modulation compensation test point and connect the shield to the radio ground(A-). Set the voltmeter to the 1 mV range.
(4) Modulate the PL or' PPL and adjust the compensation potentiometer until a null indication is obtained on the voltmeter. Cover the hole with tape to prevent accidental adjustment of this control.
(5) Go to section 2.3, step la.
2.4.2 Radios without PL or DPL
(1) Set the compensation potentiometer to its midpoint.
(2) Go to section 2.3, step 1 b .

## 2. 5 POWER MEASUREMENT

## Important

The following information is to insure accurate measurement of RF power. These instructions should be followed before performing any transmitter power tests. See the Transmitter section of this manual for information about the operation of the VSWR protection circuitry.
See the list of recommended test equipment in this section of the manual. Use only the recommended equipment for making these adjustments to avoid erroneous results. All transmitter adjustments can be performed from the top of the radio.

Connect the wattmeter to the radio antenna connector using a type N -to UHF coaxial adapter cable.

## Note

This is the only place that a coaxial adapter cable is acceptable.
Use connectors with a plastic insulating dielectric for the coaxial adapter cable. Connectors using bakelite as the insulating dielectric, or low cost adapters intended for citizens band service, should NOT be used.

The coaxial cable to adapt the UHF antenna connectoron the radio to the type $N$ connector on the wattmeter should be of a high quality type. Cable types such as RG400/U (part \#30-84173E01) or RG142 B/U (part \#30-83278B01) are recommended.

Careful set-up of the measuring system is well worth the extra time and effort. These techniques are recommended for other Motorola radios.

### 2.5.1 Audit Power Output

After completion of the radio installation you must audit the power output of your radio. Each radio installation may affect the transmitter's power output due to variations in antenna loading. The factory sets each radio to its specific power output using a calibrated 50 ohm load. Your antenna might not present the same load impedance to the radio transmitter, causing changes to system performance.

### 2.5.2 Verify Power Output

## Note

SYNTOR $X$ radios operate over a greater portion of the spectrum than most antennas are resonant. Motorola offers a wideband antenna for each band of SYNTOR X model radios. Contact the nearest Motorola center for assistance.

Verify your system has the correct antenna for the frequency range of your radio. Perform the following steps to verify the power output of your radio.
(1) Connect a 50 ohm power meter in series with the coax leading to the antenna.
(2) Measure the VSWR of the radio system for each channel.
(3) Verify power output on the transmit frequency with the lowest VSWR is a least specified output in the instruction manual.

## Note

Do not make adjustments to the power output if the measured VSWR is greater than 1.5:1 (2.0:1 for Lowband). Check your antenna for proper installation and ensure it is designed for your operating frequency.
(4) If measured power output using a 50 ohm is within $5 \%$ of the recommended power, make NO adjustments to the radio.
(5) If measured power output using an antenna is within $10 \%$ of the recommended power, make NO adjustments to the radio.

Should the measured power output differ from expected levels outlined above, see the Power Set Procedure in this manual. Reset the power output to the specified level for your radio model.

### 2.5.3 Power Set Procedure

(1) Terminate the radio with a wattmeter and a 50 ohm load.
(2) Adjust the DC power supply voltage to 16.1 volts for 100 W and 78 W models; 16.3 volts for 30 W models.
(3) Rotate potentiometers R912 and R901 fully clockwise. For 30W radios, preset R912 fully counterclockwise and R901 clockwise.
(4) Select the channel closest to the radio's first target frequency. See Table 3. Key the transmitter and adjust R912 to obtain a nominal power of 110 W for 100 W radios; 86 W for 78 W radios; or 33 W for 30 W radios. For variable power set, adjust R912 until the power is $10 \%$ over the desired power set level (e.g. 55 W for a 50W radio).
Table 3. Transmitter Power Adjustment Target Frequencies

|  | FULL-RATED |  | TARGET (MHz) |  |
| :---: | :--- | :---: | :---: | :---: |
| RANGE | POWER (W) | FIRST | SECOND |  |
| 1 | 100 | 420 | 406 |  |
| 2 | 100 | 460 | 450 |  |
|  | 30 | 460 | 450 |  |
| 3 | 78 | 488 | 470 |  |
|  | 30 | 488 | 470 |  |
| 4 | 78 | 500 | 482 |  |
|  | 30 | 500 | 482 |  |
| 5 | 78 | 512 | 494 |  |
|  | 30 | 512 | 494 |  |

(5) Select a channel close to the radio's second target frequency (Table 3). Key the transmitter and rotate R901 until the power drops slightly. Do not let the power drop below 105 W for 100 W radios; 82 W for 78 W radios; or 32 W for 30 W radios. For variable power set, do not let the power drop by more than $5 \%$ when R901 is adjusted (e.g. 53 W for a 50 W radio).
(6) Adjust the DC power supply to 13.4 volts for 100 W and 78 W models; 13.6 volts for 30 W models.
(7) Select a channel close to the radio's first target frequency (Table 3). Key the transmitter and rotate R912 for a power indication of 105 W for 100 W radios; 82 W for 78 W radios; or 32 W for 30 W radios. Check the power output on all the channels and readjust R912 until all channels indicate a power output no less than 105 W for 100 W radios; 82 W for 78 W radios; or 32 W for 30 W radios. For variable power set, adjust R912 to $5 \%$ over the desired setting (e.g. 53 W for a 50 W radio). Check power on all channels and readjust R912, if necessary, to $5 \%$ over the desired setting.

## 3. Radio Disassembly

### 3.1 GENERAL

Remove the top cover to access the solder side of the RF board, personality board, and the power amplifier deck. Remove the top cover by turning the key to release the front handle and then press the button under the handle. The top cover pops up and allows access to the boards. Remove the screw that holds the PA deck cover to access the PA deck. This procedure provides access to the metering sockets of the RF board (J2501) and the PA deck (J1101) without removing the radio from its mounting tray.

Remove the radio from the chassis by releasing the handle as described above. Slide the radio forward (about an inch) and lift it out. Disconnect the cables to remove the radio from the chassis.

## Note

Mounting screws for the common circuits board, personality board, and RF board are those with the black plastic captivators holding them to the boards.

Access the rest of the radio by removing the four screws that secure the skid plate to the bottom of the radio. Remove the skid plate to access the metering socket of the common circuits board (J951). The common circuits board is hinged so when turned on its hinge, it provides access to its component side as well as to the component side of the RF board. Remove the screws on the board and on the regulator heat sink to turn the common circuits board over on its hinge.

## CAUTION

When operating the radio with the regulator head sink screw removed, care should be taken to avoid the exposed hot flange. All serviceable mounting screws use either Posi-drive heads or TORX heads which can be damaged by using standard Phillips screwdrivers. Use the proper screwdriver.

### 3.2 COMMON CIRCUITS BOARD

To turn the common circuits board on its hinges requires the removal of three screws. However, to remove the board, you must remove the two hinge screws, unplug the cable between the common circuits board and the personality board, and unplug the wires between the common circuits board and the PA deck. When installing the board in the radio, take care to pass both the cable and the wires between the two board hinges.

## 3. 3 PERSONALITY BOARD

Remove the personality board from the radio as follows:
(1) Remove the seven screws that secure the board to the radio.
(2) Disconnect the cable from the front plug.
(3) Disconnect the 10 conductor cable from the common circuits board.
(4) Pull the board away from the radio to disconnect the connectors from the RF board.

When installing the board in the radio, be sure that the front plug gasket is properly seated. (Silicone compound, Motorola Part \#11-00834678, can be helpful in this process.)

### 3.4 RF BOARD

Remove the RF board as follows:
(1) Remove the personality board as explained in paragraph 3.3.
(2) Remove the six retention screws.
(3) Disconnect the coaxial cable between the RF board and the internal casting.
(4) Disconnect the wires located near the antenna switch.

Access to some segments of the solder side of the RF board requires the removal of shields attached to the board with screws. On the component side of the RF board, remove the two large cans by simply pulling them off the board. However, other cans on the board must be unsoldered to be removed.

Install the RF board back in the radio using care to align the board guide posts with the internal casting. Take care to match the board spring connectors with those of the internal casting.

### 3.5 INTERNAL CASTING

### 3.5.1 General

Remove the internal casting from the radio as follows:
(1) Remove three screws to allow the common circuits board to hinge.
(2) Remove four cover mounting screws from the bottom of the radio.
(3) Remove two screws from the RF board (from the other side of the radio).
(4) Disconnect the cable between the internal casting and the RF board.
(5) Disconnect the cable between the internal casting and the PA deck.
(6) Disconnect the RF board wires located near the antenna switch.

Exercise care during the reassembly operation to make the proper connections between the various connectors and to replace all the screws without omission.

### 3.5.2 First Mixer

To remove the first mixer, remove the two screws that secure the first mixer cover and gasket to the internal casting.

## CAUTION

Do not use excessive heat. Otherwise, the tap leads will come off the filter.

Carefully unsolder the two tap leads from the first mixer to the filter and remove solder between the feed through and the circuit board. Remove the two screws that hold the circuit board to the internal casting, then remove the first mixer board.

## 3. 5 .3 Low Pass Filter Board (or Optional Pre-amplifier)

With the cover off, remove the low pass filter board (or optional pre-amplifier) as follows: carefully unsolder and remove the wires from the phono connector, then unsolder and disconnect the coaxial cable from the six-pole filter. If an optional pre-amplifier is used, unsolder the feedthrough leads and remove the two retaining screws to remove the board.

$$
\begin{aligned}
& \text { CAUTION } \\
& \text { See the Special Repair Procedures for soldering } \\
& \text { iron use on hybrid substrates. It is imperative } \\
& \text { that high silver content be used when removing } \\
& \text { the two insulated wires from the smaller pre- } \\
& \text { amplifier substrate. Since the smaller substrate } \\
& \text { is not copper clad, leaching of the pads can be- } \\
& \text { come a problem. }
\end{aligned}
$$

Remove the two screws that hold the carrier to the casting. Lift it out, using the handle that forms part of the carrier.

### 3.5.4 VCO Buffer/Doubler

## Note

If the VCO assembly is replaced, it will be necessary to readjust the compensation level as explained in the Radio Adjustment Procedures in paragraph 2.
Remove the VCO buffer/doubler as follows: disconnect the coaxial cable to the VCO, disconnect the single wire to the feedthrough, disconnect the coaxial cable to the RF board, and disconnect the coaxial cable to the PA deck.

Remove the coaxial cables from the substrate, using the precautions explained in the Special Repair Procedures. Then, remove both cables from the internal casting. This may require the use of a larger soldering iron to heat the internal casting. However, never use the larger soldering iron on the substrate.

After removing the four mounting screws, the VCO buffer/doubler assembly can be removed by lifting the handle that forms part of the carrier. Lifting the carrier will simultaneously disengage the connector to the three-pole injection filter. This filter is located directly under the carrier.

### 3.6 TRANSISTOR MODULE REPLACEMENT

## Note

Transistors are replaced as part of a module assembly. There are six module assemblies in each power amplificr: low-level amplifier (control stage), predriver, driver, and three finals.
To remove the low level amplifier (control stage), unsolder the input coax, output strap, and bias pin. Use C805 as a handle to carefully pull the module up until Q802 releases
from its heatsink clip. Before installing a new module, apply a light coating of Wakefield compound to Q802. Be careful when installing the new module to avoid breaking the substrate. Align Q802 with the heatsink clip and apply pressure to Q802 until the module is firmly seated.

To remove any of the other modules, unsolder the tabs from the ceramic substrates ( 8 tabs on the predriver and driver modules; 6 on each of the final stage modules). Remove transistor mounting screw and extract the module. Before installing the new module, apply a thin coating of Wakefield compound to the mounting surface. Be sure that the module output (indicated by the beveled corner) faces in the proper direction.

## CAUTION

The transistor mounting screws must be tightened before the transistor tabs are soldered to the circuit board. Do not tighten to more than 6-7 inch pounds, or damage to the transistor may result.

Solder the module tabs to the substrate so that the connection covers the entire surface of the tab.

### 3.7 POWER DISTRIBUTION BOARD REMOVAL

Normally there is no need to remove the power amplifier assembly unless you must access the A+ distribution board. Perform the following steps to access the distribution board.
(1) Unsolder the bias pin connections (7) from the substrates.
(2) Unsolder the input and output coaxial cable.
(3) Remove the 10 transistor mounting screws.
(4) Remove the 5 hex-head screws holding the plastic carrier.
(5) Remove the amplifier.

If it is necessary to remove the $\mathrm{A}+$ distribution board, unsolder the 7 feedthrough capacitor connections and remove the 3 mounting screws.

To replace the boards, reverse the removal procedure. When replacing the power amplifier assembly, apply a thin coating of Wakefield compound to the transistor mounting surfaces. Start the transistor mounting screws to insure proper alignment, then insert and tighten the hex-head screws in the plastic carrier. Tighten the transistor mounting screws.

## 3. 8 FRONT LATCH

Remove the front latch key mechanism by inserting the key into the lock, turning the key about $45^{\circ}$ in a clockwise direction, and inserting the special removal tool (Motorola Part \#66-84909B01). Insert the tool with the point directed away from the lock while twisting it $180^{\circ}$ in a clockwise direction. This releases the key mechanism for removal.

Removal of the black plastic part requires the removal of a single screw.

## 3. 9 DIRECTIONAL COUPLER

To remove the directional coupler, remove the top cover and unsloder the two coaxial cables. Remove the mounting screws. Swing the common circuits board up, unplug the connector, and lift the carrier from the radio.

## 3. 10 ANTENNA RELAY

Disconnect the wires to the coil and the connector on the RF board to remove the antenna relay. The coaxial cable to the internal casting can be unplugged at the casting, but the cable to the transmitter PA deck must be unsoldered at the harmonic filter. The antenna relay is secured by means of a nut located outside the radio chassis. Remove the nut with a spanner nut removal tool (Motorola Part \#RSX4028A).

## 4. General System Troubleshooting Guide

## 4. 1 GENERAL

Tables 4 through 13 , provide a general system troubleshooting guide. Table 4 is divided into three sections: symptoms of malfunction, possible cause of failure, and the procedure to be adopted to clear the fault.

The failure symptoms deal with the following conditions: absence of receive audio, distorted receive audio, low audio power, radio does not squelch, radio does not unsquelch, improper squelch sensitivity, no PL/DPL decode, no regulated 9.6 V or 5.0 V , no RF power output, low RF power output, no transmitter modulation, distorted transmitter modulation, improper microphone sensitivity, transmitter frequency shift with high-level modulation, synthesizer does not lock, reference frequency ( 6.25 kHz ) heard in speaker or on transmitted audio, synthesizer locks on wrong frequency, slow synthesizer lock time, poor receive sensitivity, alternator whine.

## 4. 2 REFERENCE

Depending on the cause of failure, the following troubleshooting charts and schematic diagrams are referred to for consultation:

- Schematic diagram of the audio section of the personality board; this diagram provides various voltage levels and waveforms and is located in the Microcomputer System section of this manual.
- Squelch troubleshooting chart; this is located in the Receiver section of this manual.
- Regulator troubleshooting guide; this is located in the Common Circuits Board section of this manual.
- Synthesizer troubleshooting chart; this is located in the Synthesizer section of this manual.
- Microcomputer troubleshooting chart; this is located in the Microcomputer System section of this manual.
- Power control troubleshooting chart; this is located in the Common Circuits Board section.
- Power amplifier troubleshooting chart; this is located in the Transmitter section.
- IDC troubleshooting chart; this is located in the Synthesizer section.
- Radio alignment and adjustment procedures; this is located in the General Maintenance section.
- Receiver troubleshooting chart; this is located in the Receiver section.


## 4. 3 SYSTEM SELF CHECK

When the radio system is turned on it displays "SELF CHECK." During this time each processor does a diagnostic check. This includes checking ROM, RAM, EEPROMs, and serial bus circuitry. If no errors are detected, the display shows the selected mode. If there are any errors, they are displayed for two seconds each, after the self check display.

The error code is divided into two parts separated by a "/." The first part indicates the location of the error. The second part indicates the type of error. While the problem is not necessarily located on the board indicated by the location code, the troubleshooting guide for that board should be used to initially locate the problem. See Tables 5 through 13 for interpretation of these codes.

There are two types of errors. The first type does not stop the system from operating. This error occurs if an option board is not communicating on the serial bus. In this case the display indicates "ERROR ___." This specifies the error. When this display appears, the operator is alerted by a beep. The system continues to operate without the option.

The second type of error inhibits the operation of the system. This occurs if the radio's EEPROM is corrupted. Since the data needed to operate the radio is stored in the EEPROM (frequencies and PL codes) the system cannot work if that data is invalid. This type of error is indicated by a display of "FAIL ___." If there is a single error of this type, the display shows it indefinitely. If there are multiple errors, and at least one of them is of this type, each error display is shown for two seconds and the display cycles through them.

A special case exists for error "FAIL 01/90." This error indicates the control unit did not receive a message from the radio. If this error occurs, the control unit resets the system after all the error displays are shown in an effort to correct the failure.

| SYMPTOMS | POSSIBLE CAUSE | PROCEDURES |
| :---: | :---: | :---: |
| No Receive Audio | Red or green lead fuse | Check the fuses. |
|  | Audio PA malfunction | See audio section of personality board schematic diagram. |
|  | Regulator malfunction | See regulator troubleshooting chart. |
|  | Synthesizer not locking | See synthesizer troubleshooting chart. |
|  | Quad detector malfunction | See receiver section schematic diagram. |
| Distorted Receive Audio | Audio PA malfunction | See audio section of personality board schematic diagram. |
|  | Quad detector malfunction | See receiver schematic diagram. |
|  | IF malfunction | See receiver schematic diagram. |
| Low Audio Power | Audio PA malfunction | See audio section of personality board schematic diagram. |
|  | Red lead fuse | Check fuse. |
|  | Quad detector malfunction | See receiver schematic diagram. |
|  | IF malfunction | See receiver schematic diagram. |
| No Regulated 9.6 V or 5.0 V | Short on circuit board | - |
|  | Regulator malfunction | See regulator troubleshooting chart. |
| No RF Power Output | PA enable switch | See microcomputer schematic diagram. |
|  | Keyed 9.4V switch | See microcomputer schematic diagram. |
|  | Synthesizer out-of-lock | See synthesizer troubleshooting chart. |
|  | Red or orange lead fuse | Check fuse. |
|  | Power control malfunction | See power control troubleshooting chart. |
|  | PTT circuit malfunction | See troubleshooting serial data link and control unit. See the control unit and personality board schematic diagram. |
|  | PA malfunction | See PA troubleshooting chart. |
| No Power Control Low RF Power Output | Power control malfunction | See power control troubleshooting chart. |
|  | Power control malfunction | See PA troubleshooting chart. |
|  | Antenna relay malfunction | See antenna relay test procedure. |
| No Transmitter Modulation | IDC malfunction | See IDC portion of the personality board schematic diagram. |
|  | Microcomputer malfunction | See microcomputer schematic. |
| Distorted Transmitter Modulation | IDC malfunction | See IDC portion of synthesizer board schematic diagram. |
|  | Reference oscillator malfunction | See IDC portion of synthesizer board schematic diagram. |
|  | VCO malfunction | See IDC portion of personality board schematic diagram. |
| Improper Microphone Sensitivity | IDC malfunction | See IDC portion of synthesizer board schematic diagram. |
|  | VCO malfunction | See IDC portion of synthesizer board schematic diagram. |
|  | Reference oscillator malfunction | See IDC portion of personality board schematic diagram. |
| Transmitter Frequency Shift with High-Level Modulation | IDC malfunction | See IDC portion of personality board schematic diagram. |
| Synthesizer does not Lock | Is radio scanning? | Out-of-lock LED lights if radio is scanning. |
|  | Synthesizer malfunction | See synthesizer troubleshooting chart. |
|  | Microcomputer malfunction | See microcomputer schematic. |
| Reference Frequency ( 6.25 kHz ) on transmitted audio or in speaker | Adaptive filter malfunction | See synthesizer troubleshooting procedure. |
| Synthesizer locks on wrong frequency | Synthesizer malfunction | See synthesizer troubleshooting chart. |
|  | Microcomputer malfunction | See synthesizer troubleshooting chart. |
|  | Reference oscillator Out-of-adjustment | See synthesizer troubleshooting chart. |
| Long Synthesizer lock time | Synthesizer malfunction | See synthesizer troubleshooting chart. |
| Poor receive Sensitivity | High IF malfunction | See receiver section schematic diagram. |
|  | Low IF malfunction | See receiver section schematic diagram. |
|  | Quad detector malfunction | See receiver section schematic diagram. |
|  | Pre-amp malfunction | See receiver section schematic diagram. |
|  | First mixer malfunction | See receiver section schematic diagram. |
|  | Second mixer | See receiver section schematic diagram. |
|  | Antenna relay malfunction | See antenna relay test procedure. |
| Alternator Whine | Chassis to A-short | Disconnect control cable and check for a short between chassis and A -. |
|  | Excessive whine in vehicle | See manual number 68P81109E33. |
| No PL/DPL | Microcomputer malfunction | See microcomputer troubleshooting chart. |
|  | IDC malfunction | See IDC portion of synthesizer troubleshooting chart. |

Table 5. Radio Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :--- | :--- |
| FAIL 01/81 | Reprogram EEPROM or check J501/502. If "FAIL" shows |
| FAIL 01/82 | after reprogram, replace U502. |
| FAIL 01/84 |  |
| FAIL 01/83 | Replace U501. Reprogram EEPROM or check J501/502. |
| FAIL 01/85 | If "FAlL" shows after reprogram, replace U502. |
| FAIL 01/88 | Replace U500. |
| FAIL 01/89 | Replace U500 and U501. |
| FAIL 01/8A | Replace U500. Reprogram EEPROM or check J501/502. |
| FAIL 01/8C | If "FAIL" shows after reprogram, replace U502. |
| FAIL 01/8B | Replace U500 and U501. Reprogram EEPROM or check |
| FAIL 01/8D | J501/502. If "FAIL" shows after reprogram, replace U502. |
| FAIL 01/90 | Check cable kits. See Personality and Control Unit |
| (Bus Failure) | troubleshooting charts. |

Table 6. Control Unit Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :---: | :--- |
| FAIL 05/82 | Control Unit EEPROM corrupted. See Control Unit troubleshooting in this manual. |
| FAIL 05/84 | Control Unit EEPROM blank. See Control Unit troubleshooting in this manual. |
| FAIL 05/90 | Control Unit serial bus failure. See Control Unit troubleshooting in this manual. |

Table 7. SECURENET-Capable Radio Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :--- | :--- |
| FAIL 09/90 | Option serial bus failure. See the appropriate |
| ERROR 09/10 | SECURENET instruction manual. |

Table 8. Trunking System Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :---: | :--- |
| FAIL. 10/82 | Option EEPROM corrupted. See the Trunking |
| ERROR 10/02 | troubleshooting chart in this manual. |
| FAIL 10/84 | Option EEPROM blank. See the Trunking troubleshooting chart in this manual. |
| FAIL 10/10 | Option serial bus failure. See the Trunking troubleshooting chart in this manual. |

Table 9. Siren/PA Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :---: | :--- |
| ERROR 08/10 | Optionserial bus failure. See the Systems 9000 Siren/PA option instruction manual. |

Table 10. MDC-600 PTT ID or MVS Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :---: | :--- |
| ERROR OD/10 | Option serial bus failure. See the appropriate option instruction manual. |

Table 11. MDC-600 Full-Feature Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :---: | :--- |
| ERROR OA/10 | Option serial bus failure. See the MDC-600 Full- |
| ERROR $0 B / 10$ | Feature option instruction manual. |

Table 12. MDC-1200 Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :---: | :--- |
| FAIL OA/82 | Option EEPROM Corrupted. See the MDC- 1200 Signaling option instruction manual. |
| FAIL OA/84 | Option EEPROM blank. See the MDC-1200 Signaling option instruction manual. |
| ERROR OA/10 | Option serial bus failure. See the MDC-1200 Signaling option instruction manual. |

Table 13. DTMF Troubleshooting Display Codes

| DISPLAY SHOWS | DESCRIPTION OF PROBLEM |
| :---: | :--- |
| ERROR OE/10 | Option serial bus failure. See the DTMF Option instruction manual. |
| ERROR OE/02 | Option EEPROM failure. See the DTMF Option manual. |

## 5. Antenna Switch Test Procedure

The antenna switch connects the antenna to the receiver via the receive reed, coaxial cable, and phono plug when the radio is in the receive mode. The antenna switch connects the antenna to the transmitter via the transmitter reed, coaxial cable, harmonic filter, and directional coupler when in the transmit mode.

### 5.1 TEST EQUIPMENT

A regular analog VOM is required for checking continuity paths or short circuits. See the list of recommended test equipment provided in Table 1 located in this section.

## 5. 2 PROCEDURE

This procedure consists of the following two tests:

- receive signal path test
- transmit signal path test

As an initial step, disconnect the coaxial cable from the PA deck input. This allows the antenna switch to change from one condition to the other (i.e., from receive to transmit or vice versa) without causing the generation of PA output power.

### 5.2.1 Receive Signal Path Test

(1) Disconnect the receive cable plug from the internal casting socket. Using an ohmmeter, verify that continuity exists between the plug center pin and the antenna connector center pin. Verify that no continuity exists be-
tween the plug center pin and the plug shield (and/or radio chassis).
(2) Place the radio on a conventional mode or into the trunking test mode and key the radio. Under this condition, the receive reed opens. Verify that no continuity exists between the antenna switch center pin and the receive cable plug center pin.

## 5.2 .2 Transmit Signal Path Test

(1) Verify that the coaxial cable is still disconnected from the PA deck input.
(2) Remove the PA shield.
(3) Key the transmitter and verify that continuity exists between the directional coupler input and the antenna switch center pin. If no continuity exists, check other points along the transmit signal path to locate any possible open circuits (see Figure 3).
(4) Verify that the transmitter path to the radio chassis is not less than 100 K ohms.

## Note

Field servicing of the antenna switch assembly or the microstrip harmonic filter is NOT recommended. A defective unit must be replaced.
(5) Key the transmitter and verify that continuity exists between the harmonic filter output and the antenna switch center pin. If continuity does not exist between these two points during transmitter keyed conditions, or if continuity exists during the receive mode, then the antenna switch assembly is defective and must be replaced.


Figure 3. Transmit Signal Path





## 1. Ceramic Microstrip Substrates

You should not attempt to repair the ceramic microstrip substrates of the radio. If a module has a faulty component, replace the whole module. Not only are repairs to the substrates and replacements of substrate components difficult to make without damaging the module, but also the factory uses special fixtures in building and testing the radio to make certain that each module operates properly. Field repairs to the microstrip substrates negate that initial factory adjustment.

The ceramic materials of the radio have properties similar to those of glass, and sharp blows and heat affect them the same way they affect glass. Therefore, if you must solder anything to ceramic microstrip modules, use as little heat and pressure as possible. You must also use solder with a high percentage of silver to avoid leaching the capacitors and noncopper runners.

## 2. Chip Capacitors

The radio uses many chips capacitors as circuit elements. They are extremely sensitive to heat and must not be re-used. Be very careful when making repairs to circuits near these components. Heat from a soldering iron being applied to a nearby component may "leach" the end metalization (terminals) of a chip capacitor. Figure 1 shows what a leached capacitor looks like.

To remove a chip capacitor, apply heat to both connecting terminals simultaneously, either with two soldering irons or a single iron with a special tip (Motorola \#ST-1160). When the connecting solder melts, lift the chip. Figures 2 and 3 illustrate this removal technique.


Figure 1. "Leached" Chip Capacitor

## 3. Replacing Transistors in the Power Amplifier

To remove the power transistors, remove two transistor mounting screws or one stud nut (accessible from the chassis bottom). Unsolder and remove the clamped mica capacitors, then unsolder an remove the transistors. Special soldering iron tips STI 160 and ST1 161 (available form Motorola parts offices) make it easier to remove capacitors and transistors.

When replacing RF power transistors, you must take the following steps. First, use a soft cloth or paper towel to remove all thermal compound and residue from both the chassis and the transistor. Then apply a thin film of Wakefield thermal compound to the bottom of the transistor mounting flange. Replace the transistor in the center of the printed circuit board cutout, tightening the mounting hardware to a maximum of 7 inch-pounds. With a low power soldering iron ( $40-60 \mathrm{~W}$ ), solder the leads, using enough solder to completely cover the lead and solder pad. Make sure that the solder is flowing frecly both over and under the lead before
removing the heat. If a lead tends to spring away from the circuit board, use the tips of a pair of pliers to hold the far end of the lead down against the board until the solder hardens. After


Figure 2. Capacitor Removal with Two Soldering Irons
replacing the transistors, replace the clamped mica capacitors, being sure to position them exactly as they were with respect to the transistor body.


Figure 3. Capacitor Removal with Special Soldering Tip

## 1. General

This section covers the Microcomputer System section of your radio.

## 2. Theory of Operation

### 2.1 INTRODUCTION

The SYNTOR X 9000 personality board consists of two major sections; the digital section, and the analog section. The digital section is notated by the 500 series part designators. The analog section is notated by the $100,200,300$, and 400 series part designators.

## 2. 2 DIGITAL SECTION

The digital section communicates with the control head and the options over a serial bus link to receive and transmit information. This section also monitors parallel inputs from the radio. The digital section microprocessor uses both serial bus inputs and radio parallel inputs, to decide response to and control of the system. The digital section controls the radio since it controls the parallel outputs.

The outputs are controlled to perform various functions including:

- audio routing
- synthesizer programming
- transmitter enables
- audio volume level control
- PL and DPL detection
- PL and DPL generation
- squelch level control
- alert tone generation

The major blocks in the digital section are:

- U500- microprocessor
- U501- program ROM
- U502- customer system/mode EEPROM
- U503- synthesizer programming latch
- U504- audio control latch
- U506- address decoder
- HY500- watchdog timer hybrid
- U505 and supporting circuitry-serial bus transceiver


### 2.3 ANALOG SECTION

The personality board analog section contains all the non-RF analog circuitry in the radio, with the exception of the voltage regulators and the RF power control. The analog section circuitry is grouped by circuit designators as follows:

- 100 series transmit audio circuitry
- 200 series receive audio circuitry
- 300 series circuitry common to receive and transmit
- 400 series audio power amplifier

The analog section provides various audio and subaudio filtering, summing, and amplifying functions that include:

- receive audio switching
- transmit audio switching
- microphone pre-emphasis and deviation limiting
- VCO compensation adjustment
- discriminator de-emphasis filtering
- received PL/DPL filtering and detection
- PL/DPL D/A converter and filtering (PL/DPL gencration)
- RF carrier detect/undetect (squelch)
- digitally controlled audio attenuator
- audio power amplifier
- option receive and transmit summing/buffering

The major blocks of the analog section are:

- U300- custom switched capacitor filter IC
- 4 MHz , crystal controlled oscillator (clocks U300)
- U301- quad opamp; microphone pre-emphasis/ limiter: option RX and TX summer/buffer: bias voltage buffer
- HY300-audio switching hybrid
- HY301- squelch hybrid
- U302- pre-amplifier (digitally controlled attenuator)
- 400 series designator parts- audio power amplifier
- jumper selections


## 3. Detailed Circuit Description

## 3. 1 DIGITAL SECTION

### 3.1.1 Microprocessor System

The microprocessor (U500) with the program ROM (U501), the programmable EEPROM (U502), address decoder (U507), and output latches (U503 and U504) make up the microprocessor system.

The heart of the system is the high-speed CMOS microprocessor that runs at 1.2288 MHz . The processor uses Y500, a 4.9152 MHz crystal, for its time base. This oscillator is internally divided by four at the processor to obtain its operating frequency of 1.2288 MHz .

### 3.1.2 Address Decoding (U506)

The microprocessor controls the address lines. A14 and A 15 output WR, to gain access to U501, U502. U503, and U504. The processor does this through the address decoder U506. The three inputs to U506 on Pins 2, 14, 3, 13, and 15 control U506 outputs to Pins 6.7.9, and 11. These signals, zero to five volt logic levels, are active low. When U506-6 is low, the processor is accessing U502 (EEPROM). When U506-7 is low, the processor is accessing U501 (program PROM). When U506-9 is low, U504 is accessed, and with U506-11 low, U503 is accessed.

## 3. 1. 3 Program Memory (U501)

The program that the processor executes is contained in the 16 k by $8 \mathrm{UV}-E E P R O M$. By manipulating the remaining 14 address lines (A13-A0), the processor can read the instructions stored permanently in the EEPROM. The address lines A14 and A 15 are used for address decoding.

### 3.1.4 Customer Mode EEPROM (U502)

All radio mode information is stored in U502 (EEPROM). The standard EEPROM is 2 k by 8 in a 24 -pin package. This package is inserted in the rear 24 pins of the IC socket (Pins 1, 2, 27, and 28 are left open). The board design accepts an optional 8 k by 8 EEPROM that is a 28 -pin part. The EEPROM is reprogrammable, and is read from like the program memory IC (U501). It is also written to by the EEPROM programming mode, described later.

### 3.1.5 Synthesizer Programming Latch (U503)

The synthesizer programming latch is an eight-bit static latch whose outputs store the digital value (high or low) of its inputs when a low to high transition occurs on U503-11. To load data into the synthesizer, the latch stores correct data (D3\#D0) from the customer mode EEPROM, and the corresponding address (A2\#A0) with the strobe output high (U503-19). Then the latch stores the same address and data with the strobe output low. This clocks the four bits of data into the synthesizer. For valid programming to occur, this process is repeated for five sets of data with five different addresses. The synthesizer is continually updated to avoid corrupted data passing on a power supply transient condition. The update rate is approximately every 20 milliseconds.

### 3.1.6 Audio Control Latch (U504)

The audio control latch operates in the same manner as the synthesizer programming latch (U503). In addition, the audio control latch provides signals for five audio routing paths, both squelch level controls, and a control line for audio volume programming.

## 3. 1.7 Watchdog Timer Hybrid (HY501)

The watchdog timer hybrid performs three functions. This hybrid circuit controls the system reset line, monitors the internal microprocessor reset line, and senses the system reset line.

The first function is performed on power-up of the radio system. The hybrid outputs a reset pulse approximately 30 milliseconds long to allow the crystal oscillators in the system to stabilize. The pulse is high on system reset (HY500-10).

Secondly, the watchdog timer monitors its in put. The synthesizer strobe from U503-19 should toggle every 20 milliseconds. If the strobe pulse fails to toggle, the watchdog timer times out and initiates a 30 -millisecond reset pulse. This is a failsafe in the event the radio's microprocessor gets lost due to a power supply transient.

The third function performed by the watchdog timer hybrid is its sensing of the system reset line. This line is bidirectional. If another processor in the system gets lost due to a transient, that processor initiates a reset pulse to recover. If the system reset line is pulsed, the watchdog timer stretches the pulse to a 30 -millisecond reset pulse.

### 3.1.8 Serial Bus Transceiver (U505 and supporting circuitry)

Communication between processors in the system is handled by the serial bus at a data rate of 9600 bits per second. The signals generated are bus + . bus - , and busy. Bus + and bus - carry the same serial data. Bus - is bus + inverted (bus + high, bus - low). In using this pair of signals, the comparator U505 can differentiate between noise and valid data. In normal radio transmission, the radio microprocessor reads the line busy in (U500-9). If found to be HI, the processor pulls
busy out high (busy in active LO, busy out active HI), and transmits as message out of TX data (U500-13). To further avoid a collision on the serial bus, the radio processor reads serial RX data (U500-12) as it transmits. If the processor does not read back the same data that it sent out, some error occurred and the radio processor attempts to re-transmit the message. When receiving a transmission, (example: control head transmitting), the radio processor would sense busy in (U500-9) going LO and process the incoming message from serial RX data (U500-12).

### 3.1.9 EEPROM Programming

The EEPROM (radio mode information) is programmed by communication over the serial bus. Special commands are sent to and from the radio microprocessor from the IBM PC programmer interface.

> Note
> An IBM PC and Control Head/Radio Programming Software Version 3.0 (or later) are required to program this radio.

The EEPROM is equipped with an input called "writeenable" that is active LO (LO writes to the EEPROM). This input is at U502-23 for a 2 k by 8 EEPROM or at U502-27 for an 8 k by 8 EEPROM. To protect the contents of the EEPROM from being inadvertently written over, the writeenable line is held in active by the microphone HI audio input.

The line is protected to eliminate the possibility of corrupting the EEPROM data during power supply transients or other temporary battery supply conditions that could possibly alter the data. The microphone HI audio input is normally biased up to 9.6 volts while receiving, and pulled to approximately 4 volts when transmitting to power the active element microphone cartridge. When connected to either of the programmers, the microphone input is shorted to ground and allows access to the EEPROM write-enable line.

The microphone line is input to the digital section by R530 pulling the base of Q513 HI and forcing Q513 to pull the base of Q514 LO. With Q514 conducting, the input writeenable (U502-23 for 2 k by 8 and U502-28 for 8 k by 8 ) is held HI by Q514. Note that CR502 and CR503 protect the writeenable line in the same manner. The diode CR 502 protects the EEPROM write line the instant the radio loses power (switched off) since this signal senses when the 9.6 volt supply falls off. The diode CR 503 protects the EEPROM when the system is being reset due to power supply transients.

### 3.1.10 Power Down Sequence

With the power off, the radio microprocessor is put in its sleep mode. This mode requires to cut back the current drain on the unswitched five-volt regulator from 15 milliamps to a few micro-amps. The unswitched five-volt regulator remains powered up while the radio is off so that the radio microprocessor retains its memory and powers up in the last
mode used. The radio processor retains the last mode, volume level, squelch level, and other operator-selected functions.

This eliminates the need for resetting all the controls every time the radio is turned on. For the radio processor to remember its last configuration, inputs are required that allow the processor to store this information be fore power is shut off to its memory and supporting circuitry (switched five volts turning off). The inputs NMI and STBY are generated to tell the processor that power is coming down.

The signals NMI and STBY are generated by the transistor circuits involving Q516 and Q517. Both signals are active LO, so when NMI is LO, the processor is put in the sleep mode (standby). The transistor Q5 16 remains off while the 9.6 -volt supply is powered up. This is done through R542 that pulls the base of Q5 16 HI . When the 9.6 volt supply begins to fall off (radio is turned off), Q516 begins to conduct, since its emitter is connected to the unswitched five-volt supply (this supply remains powered). As Q5 16 begins to conduct, the base of Q517 is pulled HI , and the collector is pulled LO. The collector is connected to U500-8, the NMI input to the processor. The signal STBY is generated by the $\mathrm{R}-\mathrm{C}$ circuit made by R547 and C521. This signal goes LO approximately 500 microseconds after the NMI signal goes LO. The STBY input is at U500-7.

### 3.1.11 Test Mode

The radio test mode allows finer audio volume steps to be input to the audio preamp. In standard operation, you can set volume in 30 discrete steps. These steps increment the audio level by approximately 3.2 dB . In the test mode, increments are approximately .4 dB . This allows setting the volume closer to rated audio, more accurately setting the audio volume level, and measuring receive parameters such as RX audio distortion, received FM hum and noise, squelch sensitivity, and other receive parameters.

Enter the test mode by shorting the two pins of jumper J 500 , and turn the radio on. The radio processor reads this input (U500-21). By shorting this input, the processor reads this port LO, enters the test mode, and enables the finer volume increments. Jumper J500 3 also disables the watchdog timer. This is useful for troubleshooting. If a malfunction causes the watchdog timer to time out, the timer sends out reset pulses until the system recovers. By shorting J500, the reset pulses stop and the system resumes operation. This allows you to troubleshoot and find the source of a problem with out resetting the system.

### 3.2 ANALOG SECTION

The analog section of the personality board consists of four groups of circuitry. They are transmit audio, receive audio, common circuitry, and the audio power amplifier.

### 3.2.1 Transmit Audio Circuitry

To handle hardware options more efficiently, there are three possible paths for audio to pass through while transmit-
ting. The first, the normal microphone path, follows the standard pre-emphasis curve of +20 dB per decade from 300 Hz to 3 kHz , and rolls off sharply at frequencies above 3 kHz .

The second two transmit-audio routing paths are available for hardware options. Both of these paths are accessed through the option TX buffer at J301-12 or J1-3. The input at J301-12 provides for options internal to the radio, and J1-3 provides for options in the external options box. This input is the null port of the opamp U301-1. The input allows summing of multiple option outputs without interference.

The first transmit audio route is TX splatter. This port, when enabled, displays a flat response from 300 Hz to 3 kHz , and rolls off sharply at frequencies above 3 kHz .

The other transmit route available to the options is TX flat. This port shows a flat response from approximately 2 Hz to above 6 kHz , and does not roll off sharply.

## 3.2 .2 Microphone Transmit Audio

The microphone path enters the radio through J1-27. The resistors R 101 and R102 with the capacitor C108 provide DC bias for the active microphone element. This signal is available as an input to the options at J301-11.

Microphone HI, after entering the radio, goes to Cl 00 . This capacitor blocks DC, and sets the pre-emphasis required to an $18-\mathrm{kHz}$ high-pass corner. The high-pass filter provides the required $+20 \mathrm{~dB} /$ decade pre-emphasis response. The microphone path is switched in or out by the transmission gate on HY300. The signal is input at HY300-6 and output at HY300-4. The control line to turn the microphone path on is at HY300-11, and microphone mute is active HI. HY300-6 and HY300-4 are the summing node of the opamp unless the path is open (HY300-11 HI).

The microphone signal is amplified by U301 by a factor of 24 (at 1 kHz ), so the nominal 80 mV input from the microphone almost sends the opamp output into clip. A slightly stronger signal causes the output to clip. The signal can never be greater than the output swing of the opamp. The output of the opamp is attenuated by the deviation potentiometer R108. This adjustment is used to set deviation of the overall system to below 5 kHz .

After the microphone signal has been pre-emphasized, limited, and the level set through R108, the signal enters the splatter filter at U300-11. The splatter filter provides the sharp roll-off required to frequencies above 3 kHz . The output of the splatter filter (at U300-13) travels to the compensation potentiometer R111. The compensation potentiometer is used to adjust the sensitivity of the VCO modulation port to equal the reference modulation port.

The VCO modulation port response has a high-pass response, and the reference modulation port has a low-pass response. The compensation potentiometer sets the sensitivity of the VCO modulation port so that the overall response of the VCO is flat.

The correct tuncup procedure is to set the compensation potentiometer (R111) first, and then set the deviation potentiometer (R108).

Then the audio signal travels through the series FET (Q101) to the RF board where it is input to the VCO circuitry to modulate the RF carrier during transmit. The series FET (Q101) provides isolation to the VCO mode line during the VCO's receive mode of operation.

### 3.2.3 Option Transmit through Splatter

This option path is one of two paths that a hard ware option is able to route audio to be transmitted. The path is enabled by the latch U504 from Pin 6. In normal operation, the port is enabled when the option sends a command over the serial bus. The radio processor then enables the port and keys the radio. The option (for example PTT-ID) enables its audio port to send an audio signal into TX audio. This audio signal is amplified by the opamp U301-A. The output of U301-A at U301-3 appears at the switch input on U300-9. The switch on U300 functions as an alog transmission gate.

The switch control is at U300-10, and closes the switch when this input is low. The output of this switch is at U300-14. Once routed through this switch, the signal is input to the same limiter opamp used by the microphone path (U301-D). The signal is amplified to almost clip the output at nominal levels (just as the microphone path), but it is not preemphasized. The output of the opamp follows the same path as the micro phone path: through the deviation limit potentiometer, through the splatter filter, and then to the VCO modulation port through the compensation potentiometer.

## 3. 2.4 Option Transmit Flat

This is the second of the TX audio paths available to the hardware options. It is enabled by commands over the serial bus in the same manner as the option transmit through splatter path. This port is enabled by the output of the latch U504-5.

This audio port is named the flat TX port due to the extended response it provides. The flat TX port displays a flat frequency response from approximately 2 Hz to above 6 kHz . This response is required for digital signaling schemes such as the SECURENET option.

The audio for this path is input from the option the same as the TX splatter path (through U301-A). In this case, the splatter port is not enabled (the switch on U300-14 is open), and the flat port is enabled. The switch enables when the control at U300-22 is high. The audio input to the switch is at $\mathrm{U} 300-21$, and the output is at $\mathrm{U} 300-15$. The IC provides +7.5 dB of gain from input to output, and also sums with the IC's internal D/A converter.

The D/A converter is used to generates PL and DPL transmit signals with the data lines D3 through D0 at Pins 32, 31,30 and 29 of $U 500$. These outputs of the processor drive the inputs of the D/A on U300 at Pins 25, 26, 27, and 28. The D/A on U300 requires the reference voltage at U300-1 to function properly. The reference voltage is a resistive divider,
formed by R307 and R308, and provides the required 1.3 volts DC to this input. The output of the D/A is at U300-15. As discussed in the option TX flat section, the D/A is summed with the TX flat path.

PL and DPL are used only when the micro phone path or the option TX through the splatter path are enabled. The only signal present at U300-15 is a TX flat signal or a PL/DPL, but not both. The output of U300-16 is normally 500 mV above the analog ground voltage ( Vag ) at $\mathrm{U} 300-7$. The output, when generating PL or DPL, swings symmetrically about this normal voltage (Vag +500 mV ). The output at $\mathrm{U} 300-15$ follows the same paths as those described in the TX flat path section, and the signal is input to both the VCO modulation input and the reference modulation input to the RF board.

The output of the TX flat $s$ witch (U300-15) is routed to two different inputs to the VCO. The first is the VCO modulation port, and the second is the reference modulation port.

The TX flat signal routing to the VCO modulation port is from the output of the TX flat switch (U300-15). The signal is attenuated by R116 and R117. The attenuated signal is input to U300-8. The input is summed internally with the splatter filter input, and is output at U300-13. This summing node allows PL or DPL to be summed with normal audio from the micro phone path, and, in this case, allows the TX flat audio to reach the VCO modulation port. The output of U300-13 travels to the VCO modulation port via the compensation adjust potentiometer. The TX flat signal routing to the reference modulation port is through resistive attenuators. The jumpers JU101, JU102, JU103, and JU104 select the proper attenuation required for low-band, VHF, UHF, and $800-\mathrm{MHz}$ bands respectively. The TX flat signal passes through the DC blocking capacitor C105, and then to the reference modulation port. The transistor Q100 shunts the reference modulation port to ground when the radio is powered up, and allows the VCO to lock more quickly when first powered up.

Due to the high deviation required by $S E C U R E N E T$, the transistor Q100 is removed from the circuit by removing JU100 on SECURENET model radios. If not removed from the circuit, the transistor Q100 begins to conduct, and distorts the signal.

### 3.2.5 Receive Audio Circuitry

There are four paths in the receive audio circuitry for audio output through the speaker. These paths are the discriminator path, the option through reccive audio filter path, the option through flat response path, and the alert tone path.

The discriminator path is the recovered audio out put from an RF signal at the antenna input. This path exhibits a
$=-20 \mathrm{~dB}$ /decade response from 300 Hz to 3 kHz . The response falls off sharply with frequencies below 300 Hz and above 3 kHz.

The Personality Board provides two inputs in the receive audio path for hardware options for the receive audio string. First is RX through received audio shaping that follows the
same response as the discriminator path, -20 dB /decade from 300 Hz to 3 kHz . Second is the RX flat that displays frequency response from 200 Hz to 10 kHz . The final path in the receive audio string is the alert tone path. This path allows the radio microprocessor to sound alert tones through the speaker.

### 3.2.6 Discriminator Audio

The discriminator audio path is input to the personality board from the RF board via P601-3. The discriminator path is then input to the transmission gate hybrid (HY300) through C201. C201 provides DC blocking. The input to HY300 is at HY300-7, and the output is at HY300-8. The control line for dise mute is controlled by the output of U500-26. The control line is input to $\mathrm{HY} 300-11$, and is active HI ( HI mutes the audio). The output of $\mathrm{HY} 300-8$ inputs to the receive audio shaping filter on U300. The receive audio shaping filter input is at $U 300-20$, and is not switched. An input between 300 and 3 kHz always causes an output at U300-17. The filter provides the standard de-emphasis response of -20 dB /decade from 300 to 3 kHz . The received audio shaping filter provides band-pass filtering. The pass band is approximately 270 Hz to 3.5 kHz . The filter exhibits a loss of -3 dB at 1 kHz .

The radio microprocessor decodes received PL or DPL. and determines if the proper code is present. The radio bases this decision on its input from the comparator on U300. The discriminator output from the RF board ( $\mathrm{P} 601-3$ ) is input to the PL/DPL filter on U300 through C200. Input to the PL input filter is at U300-19. The PL filter has a low pass response, and changes its response when the selected mode is a PL mode or a DPL mode. The PL filter, when input PL/DPL is low (PL response), rolls off at approximately 250 Hz . When on a DPL mode (U300-23 is high), the PL filter rolls off at approximately 150 Hz . The output of the PL filter (U300-16) is averaged by R205 and C209 for PL. and R205 and C210 for DPL . The DC averaged signal is input to the negative input of the comparator on U300. The negative input is at U300-4 and the positive input is at U300-5. The PL filter output connects to the positive input of the comparator. This causes the output of the comparator (U300-3) to swing high when a positive going signal is output from the discriminator. The comparator output swings low when the discriminator output has a negative going signal. The output of the comparator attenuates by R208 and R209, and is read by the processor input at U500-24.

The output of the receive audio shaping filter inputs to the audio preamp (U302) through the audio summing node via R200. The audio summing node consists of R200, R201, R202, R203, and C202. The summing node provides attenuation for the receive audio shaping path, RX flat path. and the alert tone input. The summing node inputs to the audio preamplifier U302-15. The preamp is a digitally-controlled, variable gain buffer whose gain can vary from -70 to +18 dB . The gain is controlled by U500 and U503 through the control lines. UCS data. UCS write-enable, and UCS clock. The preamp gain is programmed with a serial data stream that controls the volume. The serial data appears on the UCS data line. and is clocked in bit by bit by the UCS clock when writeenable is low. The preamp has another control to force its out-
put to mute at U302-13. The mute line is an output of U500-25, and is active LO (LO mutes the preamp). The output of U302 next feeds into the audio power amplifier through C 400 that blocks DC . The audio power amplifier is a class A/B amplifier stage, and runs approximately 200 milliamps of bias to the collectors of final output transistors (Q400 and Q401) while idling with no audio input. The audio power amplifier provides +34 dB of gain and presents an output impedance of 8 ohms to drive an 8 -ohm speaker. At the nominal battery voltage of 13.8 volts, the power amp delivers over 15 watts of power with total harmonic distortion below $3 \%$.

### 3.2.7 Option Play through Receive Audio Shaping

The first option path available to the hardware options is RX through receive audio shaping filter or RX-RAS. The internal options access the RX audio ports through J30I-10, and the options residing in the external options box access the RX audio ports through $\mathrm{J} 1-33$. Both RX audio ports, RXRAS and RX flat, are enabled in the same manner as TX audio ports, by commands over the serial bus.

The RX audio signals are input through J301-10 and/or $\mathrm{J} 1-33$, and are summed and buffered by the option RX buffer opamp U301-C. The input is the null port at U301-8, and allows options access without interference. The output of the option RX buffer is connected to two inputs to HY300.

The input at HY300-9 is the input for RX-RAS. The control input for RX-RAS is at HY300-2, and comes from the output of U504-2. The control is active low (HI when the switch is open). With the control low, the RX-RAS enables, and the signal output drives the input of the receive audio shaping filter. The signal path follows the same path as the discriminator audio path discussed carlier.

## 3. 2 .8 Option Play Flat Response

The option play flat response is input to the option RX buffer, the same as the option play through RAS. The option RX buffer output (U301-10) connects to the RX flat switch (HY300-9). This switch is controlled by U504-5, and is active low ( HI when the switch is open). The control line input to the hybrid is at HY300-13. When enabled (closed), the RX option buffer connects directly to the audio summing node by R201. The summing node sets the correct attenuation for the input to the audio pre-amplifier. The remainder of the path is the same for the discriminator audio path.

### 3.2.9 Alert Tones

The alert tones are generated by the radio microprocessor by toggling its output at U500-15. This output is AC coupled by C208, and is summed directly into the audio summing node through R202.

### 3.2.10 Power Amplifier

The power amplifier is biased to 5.0 volts at its positive input by resistors R400 and R401. The dual output opamp U 400 drives the pre-driver transistors (Q403 and Q402). The outputs of the opamp are approximately 2.1 volts apart. and U400-4 is higher than $\mathrm{U} 400-1$. The banded transistor pairs, Q403 and Q402, are graded NPN pairs and graded PNP pairs respectively. The pairs are graded to match base to cmitter voltage drops. This transistors Q403-A and Q402- A form a current mirror into transistors Q403-B and Q402-B. The current is fixed through Q403-A and Q402-A by resistor R406.

When unmuted transistor Q404 is conducting, the bias current is higher than when muted. The mirrored current through Q403-B and Q402-B provides the base drive for the final output 6 transistors. The DC feedback for the opamp U400 comes from the tap between R407 and R408. The feedback DC biases the entire feedback winding of the transformer (Pins 7, 8 of T400). The transformer input windings (Pins 1, 6: Pins 2, 5) are driven by the final output transistors Q401 and Q400 respectively. The output winding of the transformer is routed from $\mathrm{J} 1-37$ and $\mathrm{J} 1-22$ in the radio, through the cable kit, into the control head, and finally to the speaker.

## 3. 3 SUPPORT CIRCUITRY COMMON TO RECEIVE AND TRANSMIT

Supporting circuitry appears throughout the analog section of the personality board. All of the 300 series designators provide functions such as supply by-passing, etc. Two of the supporting sections are worthy of special note, the $4-\mathrm{MHz}$ oscillator and the analog ground buffer opamp.

### 3.3.1 $4-\mathrm{MHz}$ Oscillator

The linear crystal oscillator provides the switched capacitor filter IC (U300) with its clocking rate. The oscillator provides a $4-\mathrm{MHz}$ sine wave (distorted) at an amplitude of approximately 700 mV peak-to-peak to the clock input (U300-24). The oscillator uses Q300 and Y300 to produce the signal.

### 3.3.2 Analog Ground Voltage Buffer

The opamp U301-B is a unity gain voltage follower. The opamp output buffers the output of the Vag reference output (U300-7). IC U300 biases internally to approximately half of its 9.6 -volt supply. To reduce audio transients when switching an audio path in or out, the buffered analog ground voltage biases all audio circuitry except the audio power amplifier. The analog ground voltage is presented to the internal hardware options via J301-8, so the options can use this DC potential to bias their analog circuitry.



# parts list 

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## parts list



NOTE:
VIP: INPUTS ARE PROGRAMMABLET.THIS MEANS VIP IN
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NOIE: VIP OUTPUTS ARE PROGRAMMABLE ONE CONTACTOF
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 Negative Ground Cable Wiring Diagrams
10/88

STANDARD CABLING






U300 BLOCK DIAGRAM



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parts list






## 1. General

The SYNTOR $X$ frequency synthesizer generates directly the first receive injection frequency and transmitter carrier. In the receive mode, the synthesizer locks on a frequency in Range 1 that is 53.9 MHz higher or a frequency in Ranges 2-5 that is 53.9 MHz lower than the receive frequency.

In the transmit mode, the synthesizer locks on the transmit output frequency. The synthesizer has a phase-locked loop (PLL) that operates at the output frequency and consists of a $14.4-\mathrm{MHz}$ reference oscillator, low-noise voltage-controlled oscillators (VCO), a high-speed programmable di-vide-by- 3 -or- 4 variable-modulus prescaler, a low-speed programmable divider, a sample-and-hold phase detector, and an adaptive loop filter. The $14.4-\mathrm{MHz}$ reference oscillator output is applied, via an injection tripler, to the second mixer of the receiver, where it serves as the low-side second injection frequency. The synthesizer circuits are on the common circuits board and RF board, and in the RF internal casting.

## 2. Theory of Operation

## 2. 1 INTRODUCTION

The PLL synthesizer is a single negative-feedback loop that uses the relationship between the phase of the input signals as the controlling variable. The output of a high-accuracy, temperature-compensated crystal reference oscillator (U608) is divided down in frequency by the reference divider (part of U602). The reference divider puts out a high-stability $6.25-\mathrm{kHz}(5.00-\mathrm{kHz}$ for some customer frequencies) squarewave signal that is routed from the reference divider to the phase detector (U603-2) to serve as the reference frequency input.

The loop frequency input of the phase detector (U603-23) receives the negative feedback for the PLL. This comes from the VCO, at a frequency proportional to the voltage on the VCO's steering line (P650-2).

The VCO, an FET RF oscillator (Q1401), multiplies the frequency up to the transmit frequency or the receive injection frequency ( 53.9 MHz below the designated frequency).

A programmable N divider divides the VCO frequency down to the loop frequency as follows:

$$
f_{(100 p)}=F_{(V C O)} / N
$$

where: $^{f_{(l o o p)}}=N$ divider loop frequency output
$f_{(v c o)}=$ VCO output frequency

$$
\mathrm{N}=\text { integer }
$$

The loop frequency and the reference frequency are applied to the phase detector (U603-23 and U603-2, respectively), whose function is to generate a DC output voltage proportional to the phase difference between these two frequencies. Phase is the controlling variable, since there may be small phase errors in the locked loop, but frequency errors cannot occur. The AC output voltage of the phase detector (PHASE DET OUT at U603-15) goes via the loop adaptive filter to the VCO steering line, thus completing the feedback loop. The loop filter controls the PLL closed loop response and removes noise from the phase detector output.

If the VCO output frequency goes high, the N divider loop frequency output also goes high, thus causing a leading phase displacement at the phase detector loop input. Since the reference signal phase does not change, the internal circuits of the phase detector detect this condition and lower the DC voltage output U603-15. This signal goes to the VCO steering line via the loop adaptive filter, causing a reduction in frequency. This compensates for the original frequency difference.

## 2. 2 LOOP PROGRAMMING AND CONTROL

For frequency generation and control, the microcomputer reads the programming information from the personality board memory module, combines it with the synthesizer control information, and multiplexes this information to the programmable divider (U602). The programming information, contained in six four-bit words, goes to the multiplex programmed divider via four data lines (D0, D1, D2, and D3) and via three data word address lines (A0, A1, and A2).

Address lines A0, A1, and A2 in the multiplexing sequence tell the divider which of the six four-bit words the microcomputer is sending on the data lines.

Of the bits sent to the divider, one selects either the transmit or the receive VCO operation. This bit is transferred from the divider (U602-19) to the transmit-receive VCO band switching network, which supplies $\mathrm{TX}+9.4 \mathrm{~V}$ to the VCO transmit switching circuitry via P650-3. Another bit determines the frequency range of the VCO. This bit is transferred from the divider (U602-20) to the range shift network. which gives the proper range shift information to the VCO's via $P 650-5$ and $P 650-6$. Sixteen bits program the A and B counters, which are inside the programmable divider. Two bits program a reference divider. Two latched bits ( $\overline{\mathrm{CO}}$ and $\overline{\mathrm{C} 1})$ go from the multiplex programmed divider to the programmable variable-modulus prescaler (U602-15 and U602-16, respectively) to control its operation during the divide cycle. Two other latched outputs from the divider, $\overline{\mathrm{S} 0}$ and $\overline{S 1}$, are used by the sample-and-hole phase detector to control the loop adaptive filter. When set high, $\overline{\mathrm{SI}}$ indicates a change in frequency. In this case, a seventh word clears the frequency change indication by setting $\overline{\mathrm{SI}}$ low, thus generating a control pulse. $\overline{\mathrm{SO}}$ switches between the transmit and receive loop filters (high for transmit filter).

The six four-bit words on the data lines remain the same once the condition of synthesizer operation and the frequency have been selected. Any change in radio mode makes the microcomputer address different memory locations in the memory module. Consequently, the six four-bit words may send different information to the divider via the data lines. The microcomputer notifies the divider, via the STROBE line, when the binary information on the data and address lines can be read into the divider and latched in without any chance of error.

### 2.3 DIVIDER

The programmable N divider works by "dual-modulus prescaling." It uses two dual-modulus prescalers, a divide-by-3-or- 4 prescaler (with its own internal programmable C counter) and a divide-by-63-or-64 prescaler. The divide-by- $63-$ or- 64 prescaler, with programmable counters A and B , is inside divider U602. The output frequency of each prescaler is first divided by one divisor to obtain a fixed number of counts, then divided by a second divisor to obtain a different number of counts. The total division performed by this system may be set to an integral value N by the programming of counters A, B, and C. This system of division allows the basic division function of programmable divider U602 to be expanded to a higher operating frequency with no loss of resolution.

Each output frequency requires that a different value of N be programmed into the programmable counters. On the posi-tive-going loop pulse edge, the divide-by-3-or-4 prescaler starts dividing by four and continues to do so until the C counter reaches zero. At this time, the prescaler enters into the divide-by- 3 mode. Once the loop pulse goes low, the C counter is preset to the value determined by the $\overline{\mathrm{C} 0}$ and $\overline{\mathrm{Cl}}$
bits. This causes a new cycle to begin on the positive-going edge of the next loop pulse.

The divide-by-63-or-64 variable-modulus prescaler works in a similar fashion. When a loop count begins, it initially divides by 64 for the number of times programmed into the A counter. When the A counter counts to zero, the loop pulse goes low and the prescaler changes to the divide-by-63 mode. It stays in this mode until the B counter reaches zero. At this time the loop pulse goes high and the cycle repeats.

Another programmable divider acts on the $14.4-\mathrm{MHz}$ reference oscillator input frequency at U602-2 to produce one of two reference frequencies: 5 kHz or 6.25 kHz . One word of the frequency select data contains two bits (D0 and DI) that select one reference frequency, as shown in Table 1.

Table 1. Reference Frequency Selection

| D0 | D1 | REFERENCE FREQUENCY |
| :--- | :--- | :--- |
| 0 | 0 | unused |
| 1 | 0 | 6.25 kHz |
| 1 | 1 | 5.00 kHz |

The frequency select data also contains bits TX and $\overline{\text { RANGE. Bit } \overline{R A N G E} \text { selects the VCO range shift window }}$ for the selected operating frequency. (Refer to the VCO paragraph for details on the range shift windows.) When the VCO bit is latched into the divider, $\overline{\text { RANGE }}$ is forwarded from U602-20 as a RANGE SHIFT signal to the range shift switching network. It is then routed via the feedthrough plate to the VCO. An NPN transistor on U600 compensates for the differing modulation characteristics of the VCO windows. When the RANGE SHIFT signal is low (at U602-20), the transistor turns on, sending a lower-amplitude audio signal to the VCO. (The VCO requires less audio input to fully modulate the RF signal when U602-20 is low than when it is high.)

## 2. 4 PHASE DETECTOR

Phase detector U603 compares the reference and loop frequency outputs of the divider circuit and uses this information to generate a DC output signal that controls the VCO frequency. The phase detector also monitors the FREQUENCY CHANGE line ( $\overline{\mathrm{S} 1}$ ) and the LOW BANDWIDTH SELECT line ( $\overline{\mathrm{SO}})$ and uses this information to generate control signals for the adaptive filter.

The phase detector output signal level is controlled by the length of time between the positive transition of the reference signal and the positive transition of the loop signal. When the reference signal goes high (at U603-2), ramp generator Q603 turns on, maintaining a constant current through C630. This constant current generates a linear rise (ramp) in the voltage at U603-24. The rise of the ramp voltage halts when the LOOP signal (at U603-23) switches to a high level, causing Q603 to turn off.

The positive transition of the loop signal, in addition to halting the ramp generator, resets an internal sample timing circuit. The ramp voltage is held constant for a time determined by sample timing capacitor C631. During this time, the two hold capacitors (C632 and C633) are charged to a level
determined by the ramp voltage. At the end of the sample time, the ramp capacitor is discharged in preparation for the next cycle.

The accumulated charge on the hold capacitors controls the conduction of a push-pull output driver. The output driver consists of an internal NPN transistor and an external PNP transistor controlled by the signal at U603-17. The PHASE DETECTOR OUTPUT signal at U603-15 is coupled, via the adaptive filter, to the VCO, where it controls the generation of injection frequencies.

The phase detector also generates control signals for the adaptive filter. It decodes the FREQUENCY CHANGE signal at U603-5 and the LOW BAND WIDTH SELECT signal at U603-3 to generate four control signals that are coupled to the adaptive filter. These four control signals are: ADAPT,
 -8 , respectively).

When operating channels are being changed in the receive mode or the mode is being changed from transmit to receive, the FREQUENCY CHANGE pulse at U603-5 causes the ADAPT line to go high and the $\overline{\mathrm{ADAPT}}$ line to go low. Since the LOW BAND WIDTH SELECT line is low, the RSW line is driven high, the TSW is driven low, and the adaptive filter is forced into the receive-adapt mode. The $\overline{\mathrm{ADAPT}}$ line returns to a high level and the ADAPT line returns to a low level after approximately 2.4 milliseconds under phase detector control, forcing the adaptive filter to enter into the normal receive mode.

When the PTT pushbutton is pressed, the FREQUENCY CHANGE pulse causes the ADAPT line to go high and the $\overline{\mathrm{ADAPT}}$ line to go low. Since the LOW BANDWIDTH SELECT line is high, the TSW line is driven high, the RSW is driven low, and the adaptive filter is forced into the transmitadapt mode. The ADAPT and ADAPT lines switch states after approximately 12 milliseconds under control of the phase detector, and the adaptive filter is forced to enter into the normal transmit mode.

While the ADAPT line is high during the transmit-adapt mode, the power amplifier is disabled. (This line connects to the personality board via J602-11.) Moreover, the ADAPT line is forced to switch to a high state when the synthesizer cannot achieve lock, thus preventing the radio from transmitting unstable or off-frequency signals.

For maximum switching speed, the microcomputer sends new data to the synthesizer at the appropriate time of the divide cycle. The phase detector forwards a SYNTHESIZER SYNC signal, from U603-4 via J602-9, notifying the microcomputer of the appropriate time to send new frequency programming information.

## 2. 5 ADAPTIVE FILTER

### 2.5.1 General

The adaptive filter is a low-pass filter in the steering line between the phase detector and the VCO. It removes noise
and variations in the steering line level to prevent unwanted modulation of the VCO.

The phase detector controls the adaptive filter through PHASE DETECTOR OUTPUT line U603-15 to operate in one of the four selectable modes, depending upon the state of the synthesizer at a given time. The modes are transmit adapt, receive adapt, transmit, and receive. The transmit adapt mode and the receive adapt mode differ only in the amount of time spent in the adapt condition, whereas the transmit mode and receive mode each require different filter characteristics. These characteristics are selected by transmission gates that switch the filter components into and out of the steering line signal path, as required.

### 2.5.2 Filter Mode Selection

Each of the four selectable modes, transmit, receive, transmit-adapt, and receive-adapt, is selected by a unique combination of states on two complementary pairs of lines. The TSW and RSW lines make up one such pair, and the ADAPT and ADAPT lines make up the other. These lines are coupled from the phase detector to the adaptive filter and are connected to the input pins of the mode-select gates (U604 A and B). The ADAPT line is also connected to transmission gates U605 and U606.

The low-input AND gates (U604 A and B) have two output lines, TRANSMIT MODE-SELECT and RECEIVE MODE-SELECT. For each filter operation mode selected, one of these output lines is switched into a high state (between +8.6 and +9.6 V ). Since these gates use low-level inputs, the output of a gate goes high whenever both of its inputs go low. Or, expressed as a Boolcan expression, the input/ output signals of, say U604A, are:

## TRANSMIT MODE-SELECT $=\overline{\mathrm{ADAPT}} \cdot \overline{\mathrm{RSW}}$

In conjunction with the ADAPT line, the out-put lines of the mode-select gates (U604 A and B) control transmission gates U605 and U606. When a selector output is forced high, the associated transmission gates turn on, passing the signals like a closed switch. Transmission gates U605A-D have ON impedances of less than 200 ohms, and gates U606A-D have ON impedances of less than 500 ohms.

## 2. 5 .3 Transmit Mode

When the synthesizer is in the normal transmit mode, the phase detector drives the TSW and ADAPT lines high and their complements, RSW and $\overline{\mathrm{ADAPT}}$, low. The output of gate U604A goes high, turning on transmission gates U605A, U606A, and U606D. The natural loop frequency of the synthesizer in this mode is approximately 15 Hz . The adaptive filter stays in this mode as long as the radio is transmitting.

In this mode, the steering line is filtered by R652 and a shunt path to ground consisting of C649, C641, C634, and R653. (The ON impedance of the transmission gates is neglected.) This signal passes to the VCO via a test jumper (JU600) and J650-2.

### 2.5.4 Receive Mode

When the synthesizer is in the receive mode, the phase detector drives the RSW and ADAPT lines high and their complements, TSW and ADAPT, low. The output of gate U604B goes high, turning on transmission gates U605C and U606C. The natural loop frequency of the synthesizer in this mode is approximately 75 Hz . The adaptive filter remains in this mode while the radio is in the receive mode.

In this mode, the steering line is filtered by R635, a shunt path consisting of R636, C640, and C641, and R637 and C654. (The ON impedance of the transmission gates is neglected.) The signal passes through the test jumper to the VCO via J650-2.

### 2.5.5 Transmit-Adapt Mode

When the synthesizer is in the transmit-adapt mode. the TSW and ADAPT lines are driven high by the phase detector, and their respective complements. RSW and ADAPT, are driven low. Transmission gates U605B, U605D, and U606D are directly turned on by the ADAPT line. The synthesizer has a high natural loop frequency in this mode, allowing it to change frequencies rapidly. The adaptive filter is switched into this mode for approximately 15 milliseconds while the radio changes from the receive mode to the transmit mode. The transmitter is inhibited in this mode by the SYNTHESIZER ADAPT line.

In this mode, transmission gate U606B by-passes the greater part of the adaptive filter. A grounded capacitor, C641, is connected to the steering line. (The ON impedance of the transmission gates is neglected.) While the filter is in this mode. C641 and C654 are being charged. The charge on C654 prevents the VCO from changing frequency during the transition from the transmit-adapt mode to the transmit mode. C654 always remains connected to the steering line. The steering line passes to the VCO through the test jumper via J650-2.

## 2. 5.6 Receive-Adapt Mode

When the synthesizer is in the receive-adapt mode, the RSW and ADAPT lines are driven high by the phase detector. and their respective complements. TSW and ADAPT, are driven low. Transmission gates U605B, U605D, and U606B are directly turned on by the ADAPT line. The synthesizer has a high natural loop frequency in this mode, allowing it to change injection frequencies rapidly. The adaptive filter switches into this mode for approximately three milliseconds while the radio changes from the transmit mode to the receive mode or from one receive frequency to another (such as when changing the operating channel of the radio).

In this mode, the greater part of the adaptive filter is shorted by transmission gate $U 606 \mathrm{~B}$, and the steering line is connected to C641. (The ON impedance of the transmission gates is neglected.) When the filter is in the receive-adapt mode, C641 and C654 are being charged. The accumulated charge on C654 prevents the VCO from changing frequencies
during the transition from the receive-adapt mode to the receive mode. C654 always remains connected to the steering line. The steering line passes to the VCO through the test jumper and J650-2.

When the frequency is changed (or if, for any reason, the loop falls out of lock), the phase detector makes the adaptive filter switch to the ADAPT mode. Consequently, the ADAPT line switches to a low state. causing the OUT-OF-LOCK indicator LED to turn on. Therefore, in normal operation of the frequency synthesizer, the OUT-OF-LOCK indicator LED turns on for a brief period whenever the frequency is being changed. During Channel Scan operation, the radio can be continuously changing frequencies at a fast rate, causing the OUT-OF-LOCK indicator LED to give a dim indication. A brightly lighted indicator LED points to the presence of an out-of-lock fault in the frequency synthesizer. Thus this indicator LED is useful for troubleshooting.

Various radio functions are deactivated each time the frequency synthesizer goes into the ADAPT mode. First the high ADAPT output disables the radio audio stages via the squelch circuits on the common circuits board. In addition, the transmitter and IDC circuits are disabled via the personality board. This fail-safe feature prevents transmitter key-up (if a loss-of-lock malfunction occurs), thus preventing the generation and transmission of uncontrolled RF signals.

### 2.5.7 Super Filter

Because the VCO requires a very pure DC sup-ply voltage, an ultra-low-pass filter (U600) supplies the VCO with a very-low-noise +8.6 output voltage. The filter removes any ripple or noise present on the +9.6 V supply line, thus preventing unwanted modulation of the VCO. A one-volt drop across the filter lowers the output voltage from +9.6 to +8.6 V .

The super filter consists of a low-pass filter. an error amplifier, and an external series-pass transistor (Q601). The +9.6 V supply is connected to U600-1 as well as to the emitter of Q601. Internally, the input from U600-1 passes through a low-pass filter to the non-inverting input of the error amplifier. C603, connected to U600-2, forms part of the low-pass filter. The output line (also connected to the collector of Q601) is fed back to the inverting input of the error amplifier through U600-4.

The error amplifier output, connected to the base of Q601 via U600-3, controls the conduction of the transistor. These connections enable the super filter to compare the output line voltage with the filtered input line voltage and to increase or decrease the conduction of Q601 to remove any ripple or noise from the VCO supply line.

The VCO supply is further filtered by C604, which is connected to ground. This filtered supply is then forwarded to the transmit-receive VCO switching network. Depending on the state of U602-19. transmit 8.4 V or receive 8.4 V is sent to the appropriate VCO through the VCO interconnect plate via J650-3 and J650-1. The filtered 8.6 V supply is also forwarded to the bandshift switching network, which selects the proper state of the Bandshift 1 and Bandshift 2 lines, depending on the state of U602-20.

### 2.5.8 Feedback Buffer

A signal at the transmit or receive injection frequency is fed back from the VCO buffer to the main board. The divider/ phase detector circuits use this frequency to monitor the oscillator frequency.

The feedback buffer, Q602, accepts an input from a tap network between the two VCO buffer stages. This input signal is forwarded via a coaxial cable and connector P/J600. The feedback amplifier output is coupled to the divide-by-3-or-4 prescaler (U601) via C607.


GPW-1056-A
Figure I. Injection Frequency vs. DC Voltage for Range 1

## 2. 6 VOLTAGE-CONTROLLED OSCILLATOR (VCO) AND BUFFER

### 2.6.1 General

The VCO and buffer amplifier, which supply the receive injection frequencies and frequency-modulated transmit injection frequencies, are mounted in separate compartments in the internal casting. The VCO output goes to the buffer input via a short coaxial cable. Both VCO and buffer are constructed on alumina thick-film substrates.

The VCO output frequency range for transmit and receive are listed in Table 2. A PIN diode switches the oscillator between the transmit and receive bands within a particular range. An additional PIN diode switch allows each range to be covered in two sub-ranges, the transmit and the receive frequency ranges.

Table 2. VCO Output Frequency Ranges

| RANGE | TRANSMIT (MHz) | RECEIVE (MHz) |
| :---: | :---: | :---: |
| 1 | $406-420$ | $459.9-473.9$ |
| 2 | $450-470$ | $396.1-416.1$ |
| 3 | $470-488$ | $416.1-434.1$ |
| 4 | $482-500$ | $428.1-446.1$ |
| 5 | $494-512$ | $440.1-458.1$ |

### 2.6.2 Oscillator Circuit

The VCO has a grounded-gate Colpitts oscillator that uses a JFET Q1401 as the amplifying element. The oscillator operates at half the desired transmit or receive injection frequency. The transmit or receive band is selected by U602 Pin 19 (BAND SHIFT) on the RF board. When Pin 19 is high, Q608 and Q609 in the RF board's TX/RX bandshifting circuit are both on. The TX/RX bandshifting circuit produces $\mathrm{RX}+8.4 \mathrm{~V}$ for Range 1 , or $\mathrm{TX}+9.4 \mathrm{~V}$ for Ranges $2-5$. The bandshifting circuit output switches on the RF PIN diode switch (CR 1408 and CR1409) on the VCO via P/J650-3 and connects the TX/RX band shift resonator in parallel with the main resonator. This changes the oscillator frequency by 26.95 MHz to half the desired TX/RX frequency.

Each of these two bands is further split up into two contiguous ranges. When U602 Pin 20 (RANGE) on the RF board is high, Q600 pulls the W/ W/ RANGE line (P/J650-6) low. This makes Q606 pull the $\overline{\mathrm{RANGE}}$ line (P/J650-5) high, and RF PIN diode CR 1407 on the VCO then switches C1412 across the oscillator resonator. This lowers the oscillator frequency for low-range operation. For high range, the situation is reversed. Within either range, the oscillator is tuned via the steering line as described in Section 2.6 .4 below.

The VCO's transmission line resonator has microstrip capacitors plated on the substrate and interconnected with wires. These are trimming capacitors for the oscillator tank circuit. They are adjusted at the factory, and do not depend on the customer's frequencies.


Figure 2. Injection Frequency vs. DC Voltage for Ranges 2, 3, 4, and 5

The oscillator signal is coupled to frequency doubler Q1404, which processes the desired transmit or receive injection frequency. After being filtered to reduce the half-car-rier-frequency component, the doubler output goes to the buffer.

### 2.6.3 Buffer

The buffer is a two-stage amplifier (Q1450) and Q1451) that sends a signal either to the LLA (Low-Level Amplifier) interface board via P 700 during transmit, or to the receive injection filter via P101 during receive. Keyed 99.4 V , coming by wire from the RF board, turns on RF PIN diode switch CRI450 and turns off PIN diode CR 1451 (by turning off Q1452). This switches the buffer outpul to P70) for the transmitter. In receive, keyed +9.4 V is low and the two PIN diodes switch roles to deliver receive injection power to P1450.

The buffer also sends a signal via P600 to the RF board in both the transmit and receive modes to drive the prescaler to send feedback to the synthesizer. Note that the +9.6 V to turn the buffer's second stage comes from the RF board via the center conductor of P600. The buffer's first stage is powered by +8.6 V coming via a wire from the RF board.

### 2.6.4 Steering Line Circuit

The steering line, in conjunction with the rangeshift and TX/RX bandshift lines, determines the operating frequency of the VCO. The steering line is driven by the phase detector (U603) and is coupled to the VCO via the adaptive filter. The phase detector supplies a DC output voltage to maintain the VCO output at the desired frequency. When the frequency is
changed, the phase detector DC output volt age shifts to change the oscillator frequency and then maintain this new frequency. Figure 1 shows the transmit and receive oscillator frequencies as functions of the steering line DC voltage.

The steering line is coupled from the RF board via J650-2 and the VCO interconnect plate. The plate contains the RF filters that shield the VCO. The steering line DC voltage level determines the capacitance of diodes CR1402, CR1403, CR1404, and CR1405. An increase in the steering line voltage causes the capacitance of these diodes to decrease and the corresponding oscillator frequency to increase. On the other hand, a decrease in the steering line voltage causes an increase in the capacitance of the diodes and a reduction in the oscillator frequency.

### 2.6.5 Modulation Line

During transmit, the transmit audio signals modulate the VCO directly, using varactor diode CR1408. The transmit audio signal is coupled, via Pin 4 of the VCO interconnect plate, to CR1408, which modulates the oscillator frequency.

### 2.7 TRANSMIT AUDIO CIRCUITS

## Note

While reading the following, refer to the IDC portion of the Common Circuits Board Schematic Diagram attached to the Common Circuits Board section of this manual.

The transmit audio circuits consist of four stages that condition the microphone audio signal for direct frequency modulation of the transmit injection signal. The greater part of the audio path is controlled by the IDC ENABLE signal that is coupled to the IDC (instantaneous deviation control) circuitry via J401-6. This signal controls transmission gate U510A, which enables the transmit audio circuits only when the radio is in the transmit mode. (Transmit +9.5 V is applied to the IDC ENABLE line.)

The MIC HI signal is coupled into pre-emphasis amplifier U502D via J401-5. This amplifier has a frequency response that enhances the audio frequencies toward the high end of the transmit audio frequency range (approximately $300-3000 \mathrm{~Hz}$ ). The amplifier output (at U502-12) is coupled to U501-1. When PTT is activated, the transmission gate control line (at U501-13) switches to a high level and the signal passes through the gate to limiter/amplifier U502A.

The limiter/amplifier clips the audio signals at seven volts peak-to-peak, thus preventing excessive audio modulation of the transmitted signal. (With lower audio input levels, this amplifier acts as a linear gain stage.) The limited transmit audio signal is coupled from U502-3 to splatter filter stage U502C.

The splatter filter is a $3-\mathrm{kHz}$ low-pass filter that removes higher-order harmonics from the audio signal. With unity gain, this filter attenuates high-frequency harmonics on the clipped audio signal from the limiter stage. The splatter filter
output passes from U502-10 to the deviation adjust potentiometer (R517).

External modulation, such as PL or DPL, passes through gates U501B and U501C. These gates are connected in series with the external modulation inputs, and can therefore disable these modulation inputs to circuits that may require such a function. Normally, these enable lines are pulled high by the HY501 resistors. The output of each gate passes to U502B via the resistors that form part of HY502.

An output of combiner U502B is coupled to the compensation adjust potentiometer R543 and the reference oscillator. PL and DPL signals frequency-modulate the reference oscillator, thus preventing the phase detector output from defeating the direct low-frequency modulation of the VCO gener-
ated by the PL/DPL signal. (The reference oscillator and phase detector form part of the synthesizer schematic diagram.)

The audio signal at the wiper of R517 is combined with the PL/DPLL signals at the compensation adjust potentiometer (R543). This combined signal then passes to the transmit VCO. The compensation adjust potentiometer, R543, is adjusted at the factory and should be readjusted only if the common circuits board, reference oscillator, or VCO is changed. R543 can be readjusted by the procedure presented in the Ra dio Alignment and Adjustments part of the Maintenance and Troubleshooting Section of this manual.

Reference Modulation Inhibit Switch Q502 is allowed to conduct while the radio is in the receive mode, effectively shorting the reference modulation signal line to ground. This prevents any noise induced on the line in receive mode from affecting the reference oscillator and, consequently, the receive injection frequency. During initial turn-on, C508 is charged through Q502. This action allows a stable receive frequency to be attained almost immediately. Q502 is turned off by TX +9.5 V during transmit, enabling the reference modulation signal line.

## 3. Synthesizer Troubleshooting Procedure

### 3.1 GENERAL

The troubleshooting chart at the end of this section gives a comprehensive procedure for troubleshooting the frequency synthesizer.

Major problems that may occur in the frequency synthesizer are:

- Synthesizer does not lock.
- Synthesizer locks on wrong frequency.
- Excessive reference frequency feeds through (spurs).
- Frequency lock is noisy.
- Switching response is slow.

Table 5 summarizes these problems and their possible causes. Tables $6,7,8$, and 9 show pin connections and voltages for the phase detector, divider, prescaler, and super filter.

The frequency synthesizer troubleshooting chart mentions an open-loop test and the checking of the divider programming. The following paragraphs describe these procedures without using a flowehart.

## 3. 2 OPEN-LOOP TEST

### 3.2.1 Introduction

This test requires a variable power supply, a frequency counter, a dual-trace oscilloscope, a DC voltmeter, and an RF voltmeter. The Maintenance and Troubleshooting Section of this manual recommends specific models of some of these.

The open-loop test consists of four procedures:

- VCO frequency test
- loop and reference waveforms check
- phase detector check
- adaptive filter check


### 3.2.2 VCO Frequency Test

(1) Remove jumper JU600 to open the STEERING LINE loop. Connect a one-kilohm resistor to the plus terminal of a $0-10 \mathrm{~V}$ adjustable power supply and connect the free end of the resistor to the VCO side from which JU600 was removed (the side not connected to C637). Connect the negative terminal to $B-$. This power supply serves as a steering line in this test.
(2) Connect a frequency counter to the divider port P600 of the internal casting. To check the VCO on transmit, press the PTT switch and monitor the frequency while slowly changing the steering voltage from 2.0 V to 9.0 V . Verify that changing the steering voltage results in the transmit frequencies listed in Table 3 for the appropriate RANGE/ $\overline{R A N G E}$ condition. The rangeshift lines to the VCO are at J650-6 (RANGE) and J650-5 (RANGE).

Table 3. VCO Output Frequencies During
Transmit (MHz)

$\left.$| Range | $\overline{\text { RANGE }}=$ high $(8.3 \mathrm{~V})$ <br> RANGE low $(0.2 \mathrm{~V})$ |
| :---: | :---: | :---: |$\quad$| $\overline{\text { RANGE }}=$ low $(0.2 \mathrm{~V})$ |
| :---: |
| RANGE $=$ high $(8.3 \mathrm{~V})$ | \right\rvert\, | $142.805-420.0$ |  |  |
| :---: | :---: | :---: |
| 2 | $406.0-412.8$ | $459.605-470.0$ |
| 3 | $450.0-459.6$ | $478.705-488.0$ |
| 4 | $470.0-478.7$ | $490.705-500.0$ |
| 5 | $482.0-490.7$ | $502.705-512.0$ |

If the rangeshift lines are normal, but the VCO fails to operate, the VCO is faulty and should be replaced. Also check the output level at the VCO divider port ( $\mathrm{P} / \mathrm{J} 600$ ) and verify that it is greater than -15 dBm for the specified steering line voltage range ( 2.0 to 9.0 V ).
(3) For receive, check the VCO as in Step 2. The VCO output frequency should be 53.9 MHz higher in Range 1 and 53.9 MHz lower in Ranges 2-5 than the receive frequency. Verify that changing the steering voltage results in the receive frequencies listed in Table 4 for the appropriate RANGE/RANGE condition.

## Table 4. VCO Outpur Frequencies During Receive (MHz)

| Range | $\begin{aligned} & \overline{\text { RANGE }}=\text { high (8.3V) } \\ & \text { RANGE }=\text { low }(0.2 \mathrm{~V}) \end{aligned}$ | $\begin{aligned} & \text { RANGE }=\text { low }(0.2 \mathrm{~V}) \\ & \text { RANGE }=\text { high }(8.3 \mathrm{~V}) \end{aligned}$ |
| :---: | :---: | :---: |
| 1 | 459.9-466.7 | 466.705-473.9 |
| 2 | 396.1-406.1 | 406.105-416.1 |
| 3 | 416.1-424.7 | 424.705-434.1 |
| 4 | 428.1-436.8 | 436.805-446.1 |
| 5 | 440.1-448.8 | 448.805-458.1 |

Also check the output level at the VCO divider port $\mathrm{P} / \mathrm{J} 600$ and verify that it is greater than -15 dBm for the specified steering line voltage range ( 2.0 to 9.6 V ). If the rangeshift lines are normal and the output level to the divider port is adequate, but the desired receive injection frequency cannot be tuned with the steering line voltage, the VCO is faulty and should be replaced.

## 3. 2 .3 Loop and Reference Waveforms Check

(1) Connect one channel of a dual-trace oscilloscope to U602-5 (REF OUT) and the other to U602-9 (LOOP OUT). Adjust the oscilloscope so that it triggers on the REFERENCE waveform. The oscilloscope trace should be in the chopped mode.
(2) Observe the LOOP waveform and verify that it is moving smoothly across the screen without any jitter when the steering line is varied from 1.0 V to 9.6 V .

Table 5. Frequency Synthesizer Problems and Possible Causes

| PROBLEM | POSSIBLE SOURCE OF TROUBLE |
| :---: | :---: |
| Synthesizer does not lock. | See the Synthesizer Troubleshooting Chart. |
| Synthesizer locks on wrong frequency. | Reference oscillator (U608) frequency off (should be $14.4 \mathrm{MHz}+29 \mathrm{~Hz}$ ). |
|  | Divider programming from microcomputer erroneous (possible defective memory module, or code plug, or microcomputer). |
| Frequency errors of 12.5 or 18.75 kHz | Divider U602 is defective. |
| can be caused by a defective prescaler or by shorted or open programming from lines the divider to the prescaler (U601-7,U601-6). | Prescaler U601 is defective. |
| Reference frequency feedthrough (spurs) excessive. | Hold capacitors C632, C633 defective (open is or leaky). |
|  | Ramp capacitor C630 defective. |
|  | Phase detector U603 defective. |
|  | Adaptive filter in ADAPTIVE mode or shorted input to output; guard band shorted to VCO steering line or other adaptive filter mode. |
| Frequency lock is noisy. | Input level to prescaler (U601-1), loop divider (U602-25), or reference divider (U602-2) is marginal. |
|  | Loose connection, cold solder joint, or faulty component. |
|  | Noisy Q603. |
|  | Defective phase detector U603. |
|  | Defective divider U602 or prescaler U601 (jittery). |
|  | Noisy 5 V or 9.6 V supplies. |
|  | Defective adaptive filter (open capacitors). |
| Switching response is slow. | Improper synchronization from microcomputer: check divider programming. |
|  | Maffunctioning adaptive filter: check U604, U605, U606. |
|  | Phase detector U603 gain too low (overdamped response) or too high (underdamped response): check R625, R626, RT600, C630, Q603. |
|  | Leaky adaptive filter capacitors or transmission gates (U605, U606, C641). |
|  | Leaky VCO varactor diodes. |

(3) Observe the REFERENCE signal and verify that its period is correct, that it has no jitter, and that one steering line voltage from 2.5 to 9.0 V does not exactly yield this period on the loop divider output. (The period depends on the customer's programming requirements. In most cases, it is 160 microseconds for a $6.25-\mathrm{kHz}$ reference.)
(4) If the conditions specified in Steps 2 and 3 are met, then check the divider buffer (Q602 and associated components), the prescaler (U601), the divider (U602), the reference oscillator (U608), and the divider programming. The prescaler can be checked by capacitively coupling a $200-\mathrm{MHz}$ frequency counter to its output and verifying that the output is approximately one-third of the input frequency (or one-sixth the desired loop output frequency). A frequency counter does not give an exact indication of one-third of the input frequency, since the prescaler is dividing by four part of the time. The difference should not exceed 50 ppm .

## 3. 2.4 Phase Detector Check

Check the phase detector (U603) by adjusting the steering line voltage for a loop period slightly longer than the reference period and then for a slightly shorter period. With a longer loop period, the phase detector output (U603-15) should switch to a high state (greater than 9 V ); with a shorter loop period, the phase detector output should switch to a low state (1.2V). If this does not happen, then check the phase detector and associated circuitry.

## 3.2 .5 Adaptive Filter Check

Check the adaptive filter for short or open circuits by removing jumper JU600 and then checking for a high voltage on the adaptive filter side when the base detector output is high. The absence of a high voltage is an indication of a faulty condition.

### 3.2.6 VCO Steering Line Leakage

## Note

Be sure to use a shielded cable with the voltmeter when making these measurements.

Check the VCO steering line leakage by removing jumper JU600 and connecting a one-megohm resistor to the VCO side. Connect the free end of the resistor to an adjustable power supply set to 9.5 V . Use a high-impedance voltmeter (impedance greater than 10 megohms) to verify that the volt-
age drop across the resistor is less than 18 mV . A higher voltage drop (greater than 18 mV ) is an indication of either a leaky VCO interconnection plate or defective VCO steering line varactors (CR1401-1404, CR1409, and CR1411-1414). To determine which is defective, re move the VCO from the RF internal casting and per form the test again. If the voltage drop is greater than two millivolts, replace the interconnection plate.

## 3. 3 DIVIDER PROGRAMMING TEST

The synthesizer troubleshooting chart refers to the divider programming test. For this test, use a dual-trace oscilloscope. The Maintenance and Troubleshooting Section of this manual recommends specific models. Table 8 gives the pin numbers and functions of the divider (U602). The timing diagram on the synthesizer troubleshooting chart shows the waveforms generated.
(1) Connect Channel 1 of a dual-trace oscilloscope to the STROBE line (U602-27) of the divider. Trigger the oscilloscope on the rising edge of the strobe signal.
(2) Connect Channel 2 of the oscilloscope to the A0 line (U602-23) of the divider.
(3) The waveforms on the oscilloscope should be similar to the example timing diagram. The pulse lengths depend on the frequency programmed into the memory module.
(4) Connect Channel 2 of the oscilloscope to the Al line (U602-24) and compare the pattern on the oscilloscope with the one in the timing diagram.
(5) Repeat the procedure until A2 (U602-26), D0 (U602-11), D1 (U602-12), D2 (U602-13), and D3 (U602-14) have been checked and verified.
(6) Verify that the prescaler C inputs are as shown in Table 8. If these indications are incorrect, look for a short circuit, repair the circuit board runner, or replace the prescaler (U601).

## Note

To check the programming in another way, use a single-trace oscilloscope with an external trigger input. Connect the external trigger to the strobe line and display the strobe signal on the oscilloscope to verify proper triggering. (See the timing diagram on the troubleshooting chart.) Each of the address and data lines can then be checked as in Steps 1 through 5, above.

Table 6. Super Filter Pin Connections and Voltages

| PIN | FUNCTION | TO/FROM | NOMINAL VOLTAGE |
| :---: | :--- | :--- | :--- |
| 1 | VCC | From 9.6 V regulator. | 9.6 V. |
| 2 | FILTER CAP. | C603. | 7.9 V. |
| 3 | EXT. DRIVER CONTROL | Q601 base. | 8.9 V. |
| 4 | 8.6 V OUT | To VCO. | 8.6 V. |
| 5 | Ground (internal NPN emitter) | From regulator. | 0 V. |
| 6 | Internal NPN collector | To VCO compensation | - |
|  |  | potentiometer R602. |  |
| 7 | Internal NPN base | From VCO bandshift, | 0.2 V, transmit high, |
|  |  | R604, R605. | 0.7 V, transmit low. |
| 8 | No connection | - | - |

Table 7. Phase Detector (U603) Pin Connections and Voltages

| PIN | FUNCTION | TO/FROM | NOMINAL VOLTAGE |
| :---: | :---: | :---: | :---: |
| 1 | High current ground. | --- | 0 V . |
| 2 | REFERENCE IN | From U602-5. | 0 V to 4.3 V square wave (200 us period). |
| 3 | LOW BANDWIDTH | From U602-17. | OV receive; 5 V transmit. |
| 4 | SYNTHESIZER SYNC. | To microcomputer. | 60 us positive pulse $0-5 \mathrm{~V}$ at loop pulse rate; equal to pin 2 if pin 11 is low. |
| 5 | FREQUENCY CHANGE | From U602-18. | 0.5 VS 11.1 us when frequency changes. |
| 6 | not connected. |  |  |
| 7 | $\overline{\mathrm{ADAPT}}$ | To adaptive filter. | 9.6 to 0.6 V single pulse, 3.0 ms ( $\mathrm{R} \times$ ) dekey; $15 \mathrm{~ms}(\mathrm{Tx})$ key. |
| 8 | TSW | To adaptive filter. | 0 V receive, 9.6 V transmit. |
| 9 | RSW | To adaptive filter. | 9.6 V receive, OV transmit. |
| 10 | ADAPT | To adaptive filter. | $0-9.0 \mathrm{~V}$ single puise, 3.0 ms ( $\mathrm{R} \times$ ) dekey; 15 ms ( $\mathrm{T} x$ ) key |
| 11 | LOCK |  | 0 V when out of lock; 8 V when in lock. |
| 12 | HOLD 1 | CS11 | 1.4 to 8 V (use high input impedance voltmeter). |
| 13 | HOLD 2 | CS12 | 1.4 to 8 V (use high input impedance voltmeter). |
| 14 | A+ | - | 9.6 V . |
| 15 | PHASE DET OUTPUT | To adaptive filter. | 1.2 to 9.5 V (depending on loop output freq.). |
| 16 | Low Current Ground | - | oV. |
| 17 | EXT PNP BASE | To PNP Q604 base. | 8.9 V . |
| 18 | VCC | From regulator. | 9.6 V . |
| 19 | RAMP BASE | To PNP Q603 base (ramp generator). | 9.1 V . |
| 20 | FILTERED 9.1V | To R624, R625, RT600, C629. | 9.1 V . |
| 21 | RAMP RES. | To R626, PNP Q603 emitter. | 8.0 to 8.7 V . <br> Rectangular wave @ reference rate. |
| 22 | SAMPLE TIMING CAP. | To C631. | 0 to 2 V sawtooth wave at loop pulse rate. |
| 23 | LOOP IN PULSE | From U602-9 via C628. | 1.4 V puise riding on 1.6 V ( 160 us, typical period). |
| 24 | RAMP CAP. | From C630 and ramp PNP Q603 collector. | Flat top ramp waveform at reference rate, top voltage 1.4 to 7 V (depending on loop output frequency). |

Table 8. Divider (U602) Pin Connections and Voltages

| PIN | FUNCTION | TO/FROM | NOMINAL VOLTAGE |
| :---: | :---: | :---: | :---: |
| $1^{*}$ | GND |  | OV. |
| 2 | REFERENCE IN | From U608 (reference oscillator). | $1.5 \mathrm{~V}+0.6 \mathrm{~V} p \mathrm{ac}(14.4 \mathrm{MHz})$. |
| 3* | 3.6 MHz OUT | To microcomputer. | $1 \mathrm{~V} p \mathrm{p}$ (3.6 MHz). |
| 4 | GND |  | OV. |
| $5 *$ | REFERENCE OUT | To U603-2 (phase detector). | 0 to 4.3 V square wave ( $4.16,5$, or 6.25 kHz ). |
| 6 | not connected | - | - |
| 7 | not connected | - | - |
| 8 | not connected | - | - |
| 9* | LOOP OUT | To phase detector \& prescaler. | 2.9 V to 4.3 V narrow pulse ( 1.4 V pp ) ( $200 \mathrm{us} \mathrm{nominal} \mathrm{period)}$. |
| $10^{*}$ | VCC | From regulator. | 5 V . |
| 11 | D0 | From microcomputer. | 0 to 5 V pulse train. |
| 12 | D1 | From microcomputer. | 0 to 5 V pulse train. |
| 13 | D2 | From microcomputer. | 0 to 5 V pulse train. |
| 14 | D3 | From microcomputer. | 0 to 5 V pulse train. |
| 15 | C0 | To prescaler. | 0 to 5 V . |
| 16 | C1 | To prescaler. | 0 to 5 V . |
| 17 | LOW BANDWIDTH | To phase detector. | 0 to 5 V . |
| 18 | FREQ CHANGE | To phase detector. | 0 to 5 V . |
| 19 | $\mathrm{VCO1}$ (TX) | To TX-RX switching. | 0 to 0.7 V . |
| 20 | VCO2 ( $\overline{\mathrm{RANGE}}$ ) | To bandshift driver. | 0 to 0.7V. |
| 21 | not connected | - | - |
| 22 | VBB | To divider. | 1.5 V . |
| 23 | A0 | From microcomputer. | 0 to 5 V pulse train. |
| 24 | A1 | From microcomputer. | 0 to 5 V pulse train. |
| 25 | PRESCALE IN | From prescaler. | $1.5 \mathrm{~V}+0.7 \mathrm{~V} p \mathrm{ac}$ (approx. $50-80 \mathrm{MHz}$ ). |
| 26 | A2 | From microcomputer. | 0 to 5 V pulse train. |
| 27* | STROBE | From microcomputer. | 0 to 5 V pulse train ( 7 pulses/train). |

*Should be checked first

Table 9. Prescaler (U601) Pin Connections and Voltages

| PIN | FUNCTION | TO/FROM | NOMINAL VOLTAGE |
| :---: | :---: | :---: | :---: |
| 1 | FIN | from VCO buffer. | -12 to 0 dBm (at half carrier or half first injection frequency) riding on 3.8 V . |
| 2 | VBB |  | 3.8 V , bypassed for RF. |
| 3 | PRESCALE OUT | to divider (U602). | $0 \mathrm{dBm}(0.6 \mathrm{Vpp})$ riding on level of 3.6 V at approximately one-third VCO frequency (+/-50 ppm). |
| 4 | GND |  | OV. |
| 5 | FV | from divider (U602). | 1.4 V p narrow pulse at reference frequency riding on 3.4 V . |
| 6 | $\overline{\mathrm{C} 1}$ | from divider level (programming bit). | 0 or 5 V ; test memory module mode $4-0 \mathrm{~V}$, mode $5-5 \mathrm{~V}$. |
| 7 | $\overline{\mathrm{Co}}$ | from divider level (programming bit). | 0 or 5 V ; test memory module mode $4-5 \mathrm{~V}$; mode $5-0 \mathrm{~V}$. |
| 8 | VCC | from regulator. | $+5.0 \mathrm{~V}+1-0.1 \mathrm{~V}$. |



$1$

Frequency Synthesizer



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HLE1080B VCO BUFFER


| Schematic, Circuit Board Diagram, and |
| :--- |
| Pants Lisis tor Frequency |
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VCO
HLE4191C RANGE 1
HLE4192B RANGE 2
HLE4193A RANGE 3
HLE4194A RANGE 4
HLE4195A RANGE 5

parts list




The receiver circuits are in the RF internal casting, on the RF board, the personality board, and the common circuits board.

## 2. Theory of Operation

## 2. 1 INTRODUCTION

The SYNTOR X radio does not use channel elements to generate the first mixer injection frequency. Instead, the radio applies the frequency synthesizer RF output to the first mixer via a three-pole injection filter. The first mixer is a balanced JFET (junction field-effect transistor) device for Range 2 ; Ranges $1,3,4$, and 5 use a single-ended mixer. Range 1 uses high-side injection while Ranges 2 to 5 generate a first intermediate frequency (IF) of 53.9 MHz using low-side injection.

The output of the frequency synthesizer's 14.4 MHz reference oscillator splits and applies part of the signal to the injection tripler. The injection tripler uses a Class C bipolar transistor amplifier to generate the required harmonics. The injection tripler output is tuned at a fixed injection frequency of 43.2 MHz . The second mixer uses the two input signals to generate a second intermediate frequency of 10.7 MHz . The second mixer also uses low-side injection.

## 2. 2 SECOND IF CIRCUITRY

The second IF circuitry uses several stages of filtering and amplification. Selective IF filtering is done with dual-resonator, mode-coupled monolithic crystals cut to a fundamental frequency of 10.7 MHz . No tuning is required in the second IF or detector circuitry.

The second mixer's output is applied to the four--pole filter (Y250 and Y251) via a matching network, and the output of the first six-pole filter is applied to a matching network, then to a high-gain (approximately 45 dB ) second IF amplifier (U250). The output of the second IF amplifier goes to a matching network, a four-pole filter (Y252 and Y253), a final matching circuit, and the limiter/detector (U251).

## 2. 3 LIMITER/DETECTOR

The limiter/detector (U251) generates a limiting function and a means for recovering audio from the frequency-modulated carricr. Audio is recovered form the second IF signal by means of a quadrature detector in the limiter/detector and an external two-pole dual-resonator crystal. The recovered audio from the limiter/detector output posses through an emitter-follower buffer (Q250), then goes to the audio stages on the personality board (via the personality board and the control unit). The detector buffer supplies approximately 650 millivolts rms to the control unit.

## 2. 4 AUDIO AND SQUELCH

Detected audio goes to the optional PL/DPL circuitry, then to the control unit for application to the volume and squelch controls. The adjustable outputs for these voltage dividers go to the radio for application to the respective audio and squelch circuits.

The incoming signals are buffered and filtered by the PL-filter/audio-shaping stages to remove any receive PL tones. These stages consist of quad operational amplifier U440 and associated circuitry up to the input of the audio driver (U441). The audio power amplifier consists of audio driver U44 I, the driver transistor pairs, and the Class B complementary audio finals, Q448 and Q449. The audio power amplifier amplifies the filtered audio signals, and the amplified audio signal is then transformer-coupled to the external speaker. The transmit time-out timer tone and any tones from option boards are also injected at the input of the audio power amplifier stage.

Squelch muting is controlled at two points: at series-connected FET Q442 in the PL filter and shunt transistor Q441
on the volume wiper line. Q442 is used for squelch muting as well as for muting in the priority Channel Scan mode while the priority channel is being sampled. The MUTE line drives not only transistor Q441, but also the audio driver enable switch, Q447. When the audio driver is disabled, the biascurrent to the audio finals is removed, thus reducing substantially the current drawn by the radio in the standby mode.

### 2.5 SQUELCH OPERATION

The squelch control on the control unit varies the signal level of the buffered detector output. This signal, a combinattion of noise and recovered audio, is shaped by the squelch circuitry. which has good squelch characteristics because of:

- a high-pass filter ahead of the first amplifier to attenuate the audio frequencies to a specific level,
- capacitors C403 and C404, which attenuate noise at frequencies above 22 kHz to leave a band of noise susceptible to detection,
- an input network to the detector that further attenuates audio and any harmonics generated by audio limiting at the output of the second amplifier/limiter.

The filtered noise routes to a positive-peak detector. which adds negative-going spikes at its output. These spikes are forwarded to the integrator and the variable squelch-tail control circuitry. The integrator compares the average DC level of the detector's output with a reference level and generates a fast-responding output signal. VO, as follows: $V$ is greater than 4.5 V for squelched, and less than 4.5 V for unsquelched.

The detector`s output also goes to Q402 via a dual-time constant network consisting of R416, CR403, and R417. If the signal is weak, or in the absence of a signal, the noise spike rate becomes high enough to keep C410 discharged below the turn-on voltage of Q 402 . The collector of Q 402 therefore has a potential of +9.6 V . When the signal level increases, Q402 turns on and its collector voltage, VO, begins to decrease. With a strong signal, the collector voltage reaches a minimum level of approximately 4 V . For a given level at the integrator output, the voltage across C411 varies directly with VO of Q402.

Q403 generates an output signal (SQUELCH TAIL) that is a delayed and inverted version of the integrator output. The microcomputer mutes the audio when the SQUELCH TAIL signal goes low $(0 \mathrm{~V})$ and unmutes the audio when the signal goes high ( 4.8 V ). The Q403 turn-on voltage at the node between R418 and R422 is approximately 4.5 V . This voltage is determined by the 9.6 V supply, R420, C411, and the dualtime constant network comprised of R418. R419, and CR404.

With loss of signal, the greater the voltage across C411. the longer it takes the node voltage (R418 and R422) to increase above 4.5 V . and thus the longer the SQUELCH TAIL signal remains high after loss of signal. Since C411 charges through R419 and CR404, the SQUELCH TAIL detect time is very short. The integrator output is inverted by Q404 and suppled as a CHANNEL ACTIVITY signal. This is a fast-responding output signal that is used only in Channel Scan operation.

### 2.6 RECEIVER METERING SOCKET

Use the receiver metering socket (J250) to monitor the performance of the receiver as follows;

- MSI (pin 1 of the metering socket) shows the IF signal frequency relative to the center frequency of the quadrature detector.


## Note

This should not be used for "warping" the radio onto frequency.

- MS2 shows the level of the IF signal at the input of the limiter/detector.
- MS3 shows the second mixer bias current. the proper injection level, and the high-level RF signals at the second mixer output.
- MS4 show the strength of the 14.4 MHz signal generated by the reference oscillator.
- MS5 shows the DC current to the first mixer.


### 2.7 MEASURING QUIETING

When making 20dB quieting measurements on a radio equipped with internal scan (W492), use the following procedure:
(1) Unsquelch the radio and set the volume control so there are 5.5 Vms of noise at the speaker.
(2) Squelch the radio.
(3) Turn the signal generator on at one of the scan frequencies. The radio should stop scanning.
(4) Adjust the RF level until there is 0.55 Vms of noise at the speaker (20dB).

## 3. Receiver Troubleshooting Procedure

This procedure leads to the cause of sensitivity loss in the SYNTOR X radio. Use equipment form the Recommended Test Equipment list in the Maintenance and Troubleshooting Section of this manual.
(1) Perform the preliminary checks of Table 1. If all the meter indications are correct, go to step 2.
(2) Apply a 20 millivolt signal to the antenna connector. If the meter indication at J250-3 rises above 35 uA , check the low IF amplifiers, filters, and quadrature detector.
voltages, and DC voltages shown on the receiver schematic diagram at the end of this section.

## Note

Troubleshooting of the low IF and detector is easier when you refer to the meter voltages, RF

If the meter indication at $\mathrm{J} 250-3$ is less than 35 uA , check the DC voltages of the high IF (Q201, Q202, Q203, and Q204).

Table 1. Receiver Preliminary Checks

| METERING SOCKET PIN | NORMAL INDICATION | IF INDICATION IS INCORRECT |
| :---: | :--- | :--- |
| J250-1 | $25 \pm 5$ uA. | Check the low IF and quad detector. See Note after step 2. |
| J250-2 | a. (without signal): $20+5 \mathrm{uA}$. <br> b. (with 20 dB quieting signal): <br> should be 2 to 5 uA <br> above first signal. | Go to step 2 of section 3. |
| J250-3 | a. $27+5$ uA. <br> b. (when Q204 base is | a. Check Q203 DC voltages. <br> b. Check Q203 and Q204 shorted: should drop DC voltages <br> 2-3uA. |
| J250-4 | Greater than 10 uA. | Check reference oscillator output level. |
| J250-5 | a. 10-20 uA Range 1, Range 2. <br> b. Shorted (injection output to <br> ground): should drop at least 20\%. | a. Check first mixer 25-40 uA for proper DC voltage. <br> b. Insufficient low filter output drive; check VCO and buffer. |

## HLE4186A/HLE4187A Preamplifier (Optional)

SHOWN FROM SOLDER SIDE


## FUNCTIONAL DESCRIPTION

The HLE4187A preamplifier consists of a five-pole high-pass filter, a PIN diode switch, a bipolar RF amplifier, and an output pad. The high-pass filter which receives an input signal from the antenna relay via J 100 , prevents out-of-band interfering signals from degrading receiver performance.

The RF amplifier consists of a bipolar device (Q125) connected in a common emitter configura tion. Q126 stabilizes the bias point of the amplifier. and the output pad (R131, R132, and R133) pre vents interaction between the amplifier and the preselector. The amplifier runs off a switched +9.4 V supply.

The PIN diode switch (CR125), enabled by the keyed 9.4 V supply, prevents power fed back through the antenna switch during transmit from overdissipating the RF amplifier


[^1]

HLN4467A RECEIVE FILTER



## parts list

|  HLN4737AHLLN4468A (with praanm) Internaa Casting (Range 2)HIN5036A/HLN5037A (with preamp) Internal Casting (Ranges 3 and 4) HLLN4940ANHLNA941A (with preamp) Internal Casting (Range 5) |  |  | M $\times$ W0388-C |
| :---: | :---: | :---: | :---: |
| heference symbo | motorola PART NO. | deschiption |  |
| fange 1 Pafts |  |  |  |
| 3100, 101 | 0984135802 | cannetior receptate <br> phono |  |
| ${ }_{\text {L100-104 }}^{\text {Lio }}$ |  |  |  |
|  | ${ }^{24.80134 F 01}$ |  |  |
|  | ${ }^{24,401313 F 02}$ | cosed blue |  |
| $\underline{1060}$ | - 24.80131345078 | coded cosad courual range |  |
| ${ }_{\text {L107 }}^{107}$ |  |  |  |
|  | 24.80134505 |  |  |
| R135 | 06-11009641 | realetor, fixed, $\pm \mathbf{5 \%}$, i/w unless otherwise stated 470 (used with HLIN4758A only) |  |
|  |  | mechatical part |  |
|  | ${ }_{15-84776 M 07}$ | casting |  |
|  |  | AGGE 2 PAATS |  |
| J100, 101 | 09964135802 | tonnector receptacie |  |
|  |  | coil, RF |  |
| 1100 | ${ }^{24860134-033}$ | coded groon |  |
|  |  | coded grean |  |
| L106 | ${ }_{2} 24.60134501$ |  |  |
| 107 1009 | ${ }^{24} \mathbf{2 4 0 1 3 4 5 0 4}$ | $\underset{\substack{\text { corsed } \\ \text { cosed bld } \\ \text { due }}}{ }$ |  |
| R135 | 06-11099C41 | resistor, fixed, $\Omega \pm 5 \%$, $1 / 4 \mathrm{~W}$ untess otherwise stated 470 (used with HLN446EA only) |  |
|  |  | echasicalal part |  |
|  | 15-84776M99 | casting |  |
| fanges 3 AND 4 PAATS |  |  |  |
| ग190, 101 | D9* 84135802 | connector receptacie phoro |  |
|  |  | coil, RF |  |
| L100 | ${ }^{24.400134516}$ | $\underset{\substack{\text { coded orange } \\ \text { coded liciect }}}{ }$ |  |
| ${ }_{\text {Li.105 }}$ | - |  |  |
| 1106 | ${ }_{24}$ | ${ }_{\text {coser }}^{\text {codes blue }}$ |  |
| L107 L108 |  | codect green |  |
| R135 | $06+1009 C 41$ | resistor, flxed, $\Omega \pm 5 \%$, $1 / 4 \mathrm{~W}$ unless otherwise stated 470 (used with HLN5037A orily) |  |
|  |  | schanical part |  |
|  | 15.84776M93 | casing |  |
| fange 5 Patis |  |  |  |
| J100, 107 | 0988413502 | connector receptacle phono |  |
|  |  | coil, RF |  |
| ${ }^{\text {L100 }}$ |  | ${ }_{\text {cole }}^{\text {codad blue }}$ coded red |  |
| Lios |  |  |  |
| L106 | 24-200 344.10 |  |  |
| ${ }_{\substack{\text { Liof } \\ \text { L108 }}}$ | 24.80134504 $24.80134 F 09$ | coded yellow coded yollow |  |
| ${ }^{\text {A135 }}$ | $0_{0-11009 C 41}$ | esistor, fixed, $\Omega \pm 5 \%, 1 / 4 \mathrm{~W}$ unless atherwise stated 470 (Used with HLN494 1 A only) |  |
|  |  | echanical part |  |
|  | 15.84776M99 | casting |  |



## Section Contents

Transmitter Text ..... W 10001 S 07
Schematic, Circuit Board Diagrams, and
Parts Lists for 15/35 Watt Power Amplifier ..... PW-2675
Schematic, Circuit Board Diagrams, and
Parts Lists for 78/100 Watt Power Amplifier ..... PW-0871

MOTOROLA

## 1. Theory of Operation

The transmitter uses microstrip design with ceramic substrate board. All the transmitter stages consist of 50 -ohm blocks with Class C amplifier circuitry. The transmitter has two major sections; the low level amplifier (LLA), and the power amplifier (PA).

The frequency synthesizer generates an RF output of 150 mW at the required transmit carrier frequency. The RF signal goes to the controlled stage of the LLA. The gain of the controlled stage and the output power of the radio change with variations in the control voltage. The controlled stage drives the LLA output stage (Q802). The IPA module has a rated output power of 2.2 watts.

The RF signal passes from the LLA to the final power amplifier via a coaxial cable. The signal then goes to amplifier stage Q803 and to stage Q804. These two stages, which are mounted on separate microstrip assemblies, can output 14 W and 45 W respectively.

For the 30W radio. Q803 functions as the driver stage and Q804 functions as the final amplifier. For the 78 W and 100 W radios, Q803 is the predriver stage and Q804 is the driver stage. The 78 W and 100 W final amplifiers contain three power transistors (Q805, Q806, and Q807) that operate in parallel.

The transmitter has temperature-sensing circuitry that protects the final power amplifier against high temperatures. This circuitry works in conjunction with the power control circuits to reduce the radio output power whenever the transistor temperature exceeds $80^{\circ} \mathrm{C}$. The voltage drop across R801 in the power control circuitry measures the current in the final PA stage. The RF drive to the PA is reduced whenever it exceeds a safe level.

The RF power output from the final amplifier module goes to the harmonic filter, then to the directional coupler. The directional coupler measures both the forward and reflected power. Information related to the forward and reflected power is relayed to the power control circuitry on the common circuits board. The power control circuits react to any change in power by changing the RF drive to restore the RF power output to its original level.

When the reflected power at the radio output connector reaches a level that can damage the final power transistors, the power control circuitry reacts by reducing the RF power output to a safe level. The reflected power should always be less than $40 \%$ of rated output power. The directional coupler RF output goes to the antenna via a harmonic filter and the antenna switch.

## 2. Transmitter Tests

## Note

See the Synthesizer section of the manual for information on transmit frequency, audio deviation, and modulation troubleshooting.

### 2.1 PRELIMINARY TEST

Connect the radio to a proper wattmeter, dummy load, and 13.4 V supply.

## CAUTION

Key the transmitter only while making adjustments. Make adjustments from the bottom of the radio and through the common circuits board.

### 2.2 CONTROL AND PROTECTION TESTS

### 2.2.1 Current Limiting

(1) Set POWER SET fully clockwise.
(2) Set CURRENT LIMIT fully counterclockwisc.
(3) Key the transmitter and observe the radio current drain. Drain should be less than 5 uA. Rotate CURRENT LIMITT clockwise. The current drain should increase to a maximum reading of less than 30 uA before you reach the maximum clockwise position.

### 2.2.2 Power Set

(1) Set CURRENT LIMIT fully clockwise.
(2) Set POWER SET fully counterclockwise.
(3) Key the transmitter and observe the wattmeter. Rotate POWER SET clockwise to set the maximum power output level. See Table 1 for correct meter readings.

Table 1. Power Set Levels

| RATED OUTPUT | SET OUTPUT TO: |
| :--- | :--- |
| 100 watts | 120 watts |
| 78 watts | 94 watts |
| 30 watts | 36 watts |

### 2.2.3 Thermal Protection

(1) Set CURRENT LIMIT fully clockwise.
(2) Rotate POWER SET until the power reading is approximately $87.5 \%$ of the maximum. See Table 2 .

Table 2. Output Levels for Thermal Protection

| MAXIMUM OUTPUT | SET OUTPUT TO: |
| :--- | :--- |
| 120 watts | 105 watts |
| 94 watts | 82 watts |
| 36 watts | 32 watts |

(3) Touch a soldering iron the RT801 (near the flange of the last final device). The power output should decrease as RT801 heats up.

### 2.2.4 Reflected Power Protection

(1) Set CURRENT LIMIT fully clockwise.
(2) Key the transmitter and adjust POWER SET for normal power.

## CAUTION

Since the following test requires transmission without a dummy load, the transmitter should be keyed only long enough to allow verification of proper operation of the equipment.
(3) Remove the 50 -ohm load from the radio. Briefly key the
transmitter and verify the output power indicates less than $50 \%$.

### 2.3 RF AMPLIFICATION TESTS

### 2.3.1 Injection

(1) Disconnect the RF drive signal to the exciter from the synthesizer (J700).
(2) Connect a 50 -ohm terminated RF milli-voltmeter to the synthesizer's transmitter injection plug ( P 700 ). Residual
RF drive to the exciter in the receive mode should be less synthesizer's transmitter injection plug ( P 700 ). Residual
RF drive to the exciter in the receive mode should be less than -5 dBm . Transmitter injection in the transmit mode should be greater than +22 dBm .

### 2.3.2 Low Level Amplifier

(1) Disconnect the LLA from the PA and re-connect it to a wattmeter and dummy load.
(2) Set POWER SET and CURRENT LIMIT to mid-rotation.
(3) Key the transmitter. The minimum output power should be greater than 2.2 watts. begrater than 2.2 wats.

Table 3. Transmitter Troubleshooting Procedures

|  | STEP | SYMPTOM | PROCEDURE | NORMAL INDICATION | NOT NORMAL | ACTION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | Suspected <br> Transmitter <br> Faiture. | Measure RF output at antenna connector. | Rated power. | Transmitter operational. | High power- perform transmitter <br> Control \& Protection Circuit <br> Troubleshooting. <br> No power-Go to 2. <br> Low power- Go to 3 . |
|  | 2 | No Output Power. | a. Set CURRENT LIMIT \& POWER SET fully clockwise. Check Meter 5 . | $>5 \cup$ A. | Go to b. | Go to 3 . |
| six |  |  | b. Measure DC voltage across antenna relay coil during TX. | 5VDC. | Go to c . | Check coil continuity (DC <br> resistance $=160$ ohms); If good, <br> troubleshoot relay drive circuitry. |
|  |  |  | c. Check reed switch continuity. | Continuous during TX. | Go to d. | Replace switch. |
| * |  |  | d. Check harmonic filter and output cable for shorts and discontinuities. | See schematic. | Go to 3. | Repair defect. |
|  | 3 | Low Output Power. | a. Measure DC level at collector of Q802. | $>11 \mathrm{VDC}$ | Go to b. | Perform Transmitter Power Control <br> \& Protection Circuit <br> Troubleshooting Procedure |
|  |  |  | b. Measure RF signal level at VCO buffer output. | $\pm 22 \mathrm{dBm}$ minimum. | Perform Power <br> Amplifier <br> Troubleshooting <br> Procedure. | Perform Synthesizer Troubleshooting Procedure. |


| STEP | SYMPTOM | PROCEDURE | NORMAL INDICATION | NOT NORMAL | ACTION |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Little or No power; (POWER SET \& CURRENT LIMIT) fully clockwise. | a. Disconnect LLA from controls synthesizer at J 700 . Check for keyed at U900-4. | 9.5 VDC . | Go to step 1b. | a. Check PA ENABLE at J300-5. <br> b. Check for synthesizer lock. <br> c. Check PA ENABLE switch (Q902). |
|  |  | b. Measure output voltage of U900D-1. | $>5 \mathrm{VDC}$. | Repair control voltage amplifiers Q900 \& Q901. | Go to step 1c. |
|  |  | c. Measure voltages to input of U900D-2 \& -3. | $\operatorname{pin} 3>\operatorname{pin} 2$ | U900 defective. | Check for shorts or opens in resistive feed circuits of J950-2 \& 3. |
| 2 | All controls inoperative. | a. Disconnect LLA from synthesizer at J700. | 3 V to 120 V . | Go to step 3b. | Repair control voltage amplifiers Q900 \& Q901. |
|  |  | b. Set all controls clockwise. Measure U900B-9 \& - 10 in TX mode. | $\operatorname{pin} 10>\operatorname{pin} 9$. | U900 defective. | Perform VSWR shutback Troubleshooting. |
| 3 | Current Limit inoperative. | Disconnect exciter from synthesizer at J700. Unsolder CURRENT SENSE (orange) from C887. Check drain current. | 10 A . | Check for short on $\mathrm{A}+$ of current sense line. | Check for fault in current limit circuit U900C and repair. |
| $\begin{gathered} \text { STEP } \\ -4 \\ \hline \end{gathered}$ | SYMPTOM <br> Reflected power (VSWR) protection inoperative. |  | PROCEDURE <br> Check and repair defect in reflected power detector |  |  |
| 5 | Thermal protection inoperative. |  | components U900B, CR902, etc. <br> Check and repair defect in thermal protection components |  |  |
|  |  |  | U900A, CR903, RT801, etc. |  |  |
| 6 | Power set inoperative. |  | Check and repair defect in forward power detector components R902, CR902, etc. |  |  |






HLE4395A LOW LEVEL AMPLIFIER（LLA）
parts list

| ¢efreme |  | Descarmon |
| :---: | :---: | :---: |
|  | （tock | mos |
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transistor substrate


HLE4409A PREDRIVER


HLN5119A LLA INTERFACE






$1700 \quad 241200002$


Power Amplifier




|  | description |
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| \%oxem |  |
|  | , mex |
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 | HLEAB9A (RANGE 2) |
| :--- |
| LEA3S5A (RANGE 3.5) |




## Section Contents

$\qquad$
Common Circuits Board Text
W10001S42

RF Power Control Troubleshooting Charts PW-2767

## Schematic, Circuit Board Diagram, and

Parts List for HLN4905B Common Circuits Board
PW-5767

## 1. Description

Common board circuitry performs two functions: voltage regulation and RF amplifier power control. The circuit description, theory of operation, and troubleshooting chart for the RF power control are in the transmitter section of your manual. This section covers the voltage regulators.

## 2. Regulator Theory of Operation

The voltage regulators consist of the 1000 series part designators. The regulator voltages are: switched 9.6 volts, switched 5 volts, and unswitched 5 volts. The power switch at the control unit controls the switched supplies (9.6 and 5 volts). The unswitched 5 volt supply remains powered up as long as the $\mathrm{A}+$ lead to the radio is live, and the B - lead provides a ground return path.

### 2.1 9.6 VOLT REGULATOR

The 9.6 volt regulator obtains its reference from the zener diode on HY1000. The reference voltage input of U1000B at pin 5 is approximately 7.0 volts DC. The output of U1000B at pin 4 is the 9.6 volt reference. U1000C, Q1001, and the output transistor Q1000 amplifies this reference voltage. If a short circuit occurs on the 9.6 volt supply line, the diode CR1001 forward biases, removes base drive to Q1001, and shuts down the regulator to prevent further damage.

### 2.2 UNSWITCHED 5 VOLT REGULATOR

The TO220 packaged device U1001 contains the unswitched 5.0 volt regulator. The device generates its own reference, and is internally current limited and thermally protected. The switched 5 volt supply uses this unswitched voltage as reference, so the two regulated voltages closely track each other.

### 2.3 SWITCHED 5 VOLT SUPPLY

The switched 5 volt supply obtains its reference voltage from the unswitched 5 volt supply. The switched 5 volt supply is protected against excessive output current drain. Excessive current drain is sensed by the output resistors R1021 and R 1022. If the drop across these resistors is .6 volts or more,
the transistor Q1005 begins to conduct. This begins starving base drive to the output Darlington transistor Q1006.

### 2.4 SHUTBACK CIRCUIT

Both the switched supplies ( 5 and 9.6 volt) switch on and off by the shutback circuit. The shutback circuit senses the SW B+ line voltage, and turns the regulators off if line voltage is irregular. The shutback circuit senses over and under voltage conditions on the SW B+ line. The 9.6 volt regulator shuts back through Q1002. The base of Q1002 normally pulls low through R 1006 and allows a path for Q 1001 emitter current. When shut back, the base of Q1002 is pulled high by Q1004 and turns the 9.6 volt regulator off. The switched 5.0 volt regulator is shut back in a similar manner. The 5.0 volt supply is shut back through the diode CR1003. The diode is normally reverse biased and has no effect on the circuit. When shut back, the diode conducts and forces the op-amp output (U1000D) low. This causes the regulator to shut off completely. The shutback circuit senses the low-line shutback condition through the op-amp U1000A. The op-amp compares the unswitched 5.0 voltage on its positive input with the resistively divided SW B+ input on its negative input.

The circuit shuts back the regulators when SW B+ falls to approximately 8.5 volts, and turns on when SW B+ is over 9.4 volts. The high line shutback is sensed by 18 -volt zener diode VR 1000 . This diode is presented with the SW B+ line voltage by Q1003. VR 1000 has no effect to the circuit until SW B+ reaches about 20.5 volts. The 18 -volt zener then conducts and clamps the base voltage of Q1004 to 19 volts. As SW B+ rises, the transistor Q1004 conducts and shuts back the switched regulators at high SW B+ voltages.

## 3. Regulator Troubleshooting

The following situations are explained to help troubleshoot the regulators in the SYNTOR X 9000 radio.

[^2]
### 3.1 BOTH 5 AND 9.6 VOLT REGULATOR FAILURE

(1) Inspect P300 and Jl and verify that they are properly installed.
(2) Measure $\mathrm{SW} \mathrm{B}+$ on the common circuits board. This voltage range is 10.7 to 16.2 volts. If SW B+ is outside of this range, the regulator shutback circuitry disables the regulators.
(3) Measure the voltage at the collector of Q1004. It should be .6 volts or less. If the collector is above 6 volts, repair the shutback circuit.

### 3.2 UNSWITCHED 5 VOLT REGULATOR FAILURE

(1) Measure the input to U 1001 pin 1 . This range is 10.7 to 16.2 volts. If not, repair the open path $\mathrm{A}+$ or $\mathrm{B}-$ to the common circuits board.
(2) Measure the resistance from U1001 pin 2 to $\mathrm{J} 1-\mathrm{B}$ on the personality board. This should be below . 1 ohms. If not, locate the resistive path or connector and repair.
(3) Measure the output of U1001 pin 3. If not between 4.75 to 5.25 volts, unsolder pin 3 to determine if the supply is shorted. If the unconnected output is not five volts, replace U1001.

### 3.3 9.6 VOLT REGULATOR FAILURE

(1) Measure the voltage at the emitter of Q1000. It should be between 10.7 to 16.2 volts. If not, find the open path supplying the collector.
(2) Check the op-amp output at U1000B pin 4. It should be 6.65 to 7.35 volts. Next, check U1000B pins 5 and 6 . Reading should be 6.2 volts. If not, repair the reference circuit.
(3) Measure the base voltage on Q1001. This point is normally at 3.1 volts. If this point is below 2 volts or above 6 volts, repair the driving op-amp circuit involving U1000A.
(4) Measure the voltage on the base of Q1000 (output pass transistor). The base voltage should be .5 to .8 volts below the SW B+ voltage on the emitter of Q1000. If this voltage is out of range, repair the output driver involving Q1000 and Q1001.

### 3.4 SWITCHED 5 VOLT REGULATOR FAILURE

(1) Measure the input reference voltage at U1000D pin 13, This should be 4.75 to 5.25 volts. If not, recheck the unswitched 5.0 volt regulator output. If the unswitched 5.0 supply is present, unsolder U1000 pin 13 to check if U1000 is faulty.
(2) Check the collector voltage of Q1005. Acceptable range is 10.7 to 16.2 volts. If not, find the open path to the common circuits board.
(3) Measure the driving op-amp U1000 pin 12 to determine if sufficient base drive is present for Q1006. U1000 pin 12 should be 6.4 to 7 volts. If this voltage is more than 7 volts, check the voltage drop across R1016. The drop is approximately .2 volts. If there is little or no drop across R1016, replace Q1006. If the voltage drop is excessive, remove Q1005 to disable the current shutback circuit, and recheck. Should the drop still be excessive, measure the drop across R 1021. If R1021 drop is more than .7 volts, locate the fault on the switched 5.0 -volt line. This fault is probably on another circuit board in the radio. If the R 1021 voltage drop is less than .7 volts, replace Q1006. If the voltage on U1000 pin 12 is below 6.4 and pin 14 is less than pin 13 of U1000, replace U1000. If U1000 pin 14 is more than pin 13 , check for an open R1017 or shorted CR1003. -



GPW-2538-A
Figure 1. Typical Systems 9000 Control Unit

1. Description
1.1 GENERAL

### 1.2 CONTROLS AND INDICATORS

### 1.2.1 Power Switch

The power switch is a slide switch on the right-hand bottom surface of the control unit. It turns the radio and its accessories on and off.

## 1.2 .2 Display

The eleven-character vacuum fluorescent display's primary function is to display mode numbers, mode names, volume level, and the status of options. It also functions as an on-off indicator for the entire system, and plays an integral role in the operator's reconfiguration of options.


Figure 2. Systems 9000 Control Unit for SYNTOR X 9000E Radios

GPW-4141-A

## 1.2 .3 Option Buttons

Located above the display window is a row of six buttons for turning options on and off. Below each is a small indicator light to show the status of the option.

## 1. 3 XMIT and BUSY Indicators

Above the six option buttons are XMIT and BUSY indicators. The XMIT indicator lights when the radio is transmitting. The BUSY indicator lights when the selected channel is busy.

### 1.3.1 Scan Indicators

In the right-hand side of the display window are the NON-PRI and PRI indicator lights. When scan operation detects activity on a non-priority (NON-PRI) channel, the NON-PRI light comes on. Activity on a second priority channel causes PRI to light. First priority channel activity causes PRI to flash.

## 1. 3.2 Mode Rocker Switch

Below the display window is the Mode rocker. Pressing the right side of this rocker switch increases the mode number. Press the left side to decrease the mode number. If you press and hold the switch, it scrolls the mode numbers up or down. The mode names appear in the display window.

## 1.3 .3 Volume Rocker Switch

Below the display window, beside the Mode switch is the Volume rocker. Press and release to check volume setting.

Your display shows "VOLUME _ _" and a number value ( $0-15$ ). Press and hold the right side of the rocker to increase the volume setting. Press and hold the left side to decrease volume. The number value scrolls up or down to your desired level.

The volume rocker also controls the volume level of the public address (PA) and external radio speaker (ExRd) options when they are enabled. The display window shows "PA $\mathrm{VOL}_{-}$_" when public address is on and the volume rocker is pressed.

## 1. 3.4 Home and Sel Buttons

Press the Home button to go to the radio's pre-programmed "Home" mode. You may use Home instead of Mode to change modes. Hold Home until a beep sounds to enter the configuration state. The display shows an entry prompt. Use the keypad to enter your new mode choice and press Home again. Your mode is now changed without scrolling.

Use the Sel button when configuring an option. See the descriptions of the options for more specific information.

### 1.3.5 DIM Button

Above the keypad, on the right side of the control unit, is the control for the brightness of the display and button backlighting. When you turn on the system, the display comes on at the highest level. Press DIM once to reduce the brightness of the display to medium level, and twice for low brightness level. Press DIM a third time to turn the display and button backlighting off. This is called the "surveillance" mode.

### 1.3.6 Keypad

The keypad is for changing the status of options and entering numbers to the display. See the Operator's Manual for a complete description of button operation.

## 2. Theory of Operation

### 2.1 GENERAL

The Systems 9000 control unit has solid state microprocessor circuitry that operates the standard and optional features built into the system. The control unit design allows installation in even the smallest of down-sized vehicles. Systems that have many options simply require more control unit buttons, not larger control units.

The control unit may be field programmed to alter the information stored in certain areas of its electronic memory. Some options are also added by field programming.

### 2.1.1 Display

The control unit has an cleven-character alphanumeric vacuum fluorescent display for indicating the following:

- Mode Names
- Squelch Level
- Volume Level
- Status Codes
- Message Codes
- Telephone Numbers
- Identification Numbers
- Alarm Displays
- Option Status


### 2.1.2 Controls and Indicators

A twelve button keypad contains traditional alphanumeric keys. These keys double as function keys for SYNTOR $X 9000$ options. All buttons are backlit to allow operation in low-light. Six ON/OFF option buttons and indicator lights above the display window tell whether these options are on or off.

Other indicators include BUSY, TRANSMIT, PRIORITY, and NON-PRIORITY. BUSY lights when activity is detected on the channel. The XMIT (transmit) indicator lights when you are transmitting.

When activity occurs during a Scan sequence, the $\mathrm{NON}-$ PRI (non-priority) or PRI (priority) light is on. If the detected activity be on a NON-PRI mode, the NON-PRI light is on. If the activity is on PRI mode the PRI indicator lights for second priority modes, and flashes for first priority modes.

## 2. 2 CONTROL BOARD

The control board's microprocessor (MPU) communicates on the serial bus, receives and interprets keypad data, and controls the volume. The MPU sends ASCII data to a decoder to control the display, and sends data to turn the LEDs on or off. The control board has a watchdog timer that senses the need for a system reset. The vehicle interface ports are also controlled on this board.

### 2.2.1 Microprocessor (MPU)

The MPU operates in mode 2 (expanded bus with internal ROM active). Table 1 gives jumper placements for different modes. The clock frequency is 4.9152 MHz that results in an internal operating frequency of 1288 kHz . The limited number of I/O ports is augmented by using a serial-to-parallel shift register (U3) to scan the keyboard, and to switch the VIP drivers (Q28, Q29, Q30, and Q33).

Table 1. Mode Jumper Placement

| Microprocessor Mode | JU3 | JU6 |
| :---: | :--- | :--- |
| No. 1-Expanded mode with <br> external ROM only. | IN | OUT |
| No. 2-Expanded mode with <br> internal ROM active. | OUT | IN |
| No. 3-Single Chip. | OUT | OUT |

### 2.2.2 Watchdog Timer

The watchdog timer consists of U5 (comparator) and Q4 (SCR). On system power-up, C06 pulls the inverting input of U5 high while R 10 and R11 hold the non-inverting input at $\mathrm{VCC} / 2$. The output goes low and the microprocessor resets.

As C06 charges through R14, the voltage on the inverting input drops below that of the non-inverting input, the output goes high, and the microprocessor can start operating. R14 is now pulling up on C06, and the inverting-input voltage begins to rise.

During this interval, the processor generates tickle pulses to periodically fire Q 4 , preventing the inverting-input voltage from rising above the non-inverting input voltage and repeating the reset cycle. If the tickle pulses stop for more than 150 mSec , the reset cycle is repeated.

## 2. 2. 3 EEPROM

The EEPROM stores customer data including mode names, button functions, and VIP settings. The customer data can be altered only by enabling the "STORE" function (grounding the MIC HI line); an automatic function of the control unit programmer. Power strobing minimizes EEPROM power consumptions. Jumpers configure the EEPROM for the uses shown in Table 2.

Table 2. EEPROM Jumper Table

| JUMPER | USE/PLACEMENT |
| :--- | :--- |
| JU1 | Used for future options |
| $J U 2$ | IN for 6301X Microprocessor |
| $J U 4$ | IN for 2K EEPROM; OUT for 8 K <br> EEPROM (option W930) |
| $J U 5$ | IN for 8K EEPROM (option W930) <br> OUT for 2K EEPROM |

### 2.2.4 Bus Transceiver

The serial bus transceiver consists of Q1, Q2, Q3, and U4 (CA3140). Q1, Q2, and Q3 transmit data on the bus while U4 acts as a comparator to receive data from the bus.

## 2. 2 .5 Vacuum Fluorescent Voltage Converter

Voltage for the vacuum fluorescent display is generated by a fixed frequency, variable-duty cycle driven, flyback voltage converter. Q31 and Q32 form an emitter-coupled astable multivibrator that runs at about 150 kHz . The square wave output from this circuit is integrated by R71 and C39 to form a triangle that is applied to the non-inverting input of half of U5.

During start up, the inverting input is biased at 3.7 volts by R66 and R67. Q23 is on while the non-inverting input voltage is below 3.7 volts. This allows current to flow the T1, building a magnetic field. When the triangle wave exceeds 3.7 volts, Q23 turns off and the magnetic field collapses, inducing negative current in T1.

This current flows through cither CR 13 or CR14, charging C27 and C28. As the voltage on C28 increases beyond -35 volts, CR 13 begins to conduct, pulling U5's inverting input below 3.7 volts. This decreases the cycle time that Q23 is on to the time needed to produce -35 volts on C28. The -41 volt sup ply is not regulated, but it tracks the -35 volt supply.

Similarly, the AC supply for the vacuum fluorescent filament is not regulated, but is controlled to within one volt by and inductor on the display board:

## 2. 2.6 Vehicle Interface Ports (VIP)

The VIP outputs are driven by a serial-to-parallel shift register. Output transistors (Q28, Q29, Q30) can sink 300 mA current. Primarily, these transistors control external relays. The relay is connected between the collector and switched B+.

Each VIP input transistor (Q25, Q26, Q27) is connected to a dedicated input port through transistors used for input protection. These VIP inputs are connected to ground with either normally-open or normally-closed switches.

### 2.2.7 Power Supplies

Both the +5 and the +9.4 volt supplies are linear regulators. The +9.4 supply is built with a discreet transistor (Q11). The regulation is provided by VR09. The +5 volt supply is a 7805 , three-terminal regulator IC.

## 2. 2.8 Ignition Sense Circuits

Q7 senses the vehicle ignition's state, disabling transmit when the ignition is off. For negative-ground systems, the orange lead is typically connected to the fuse box $(+12 \mathrm{~V})$. For more information, see the cable kit section.

### 2.2.9 EEPROM Write-Protect Circuit

Q12, Q13, and associated circuitry guard against inadvertently writing into the EEPROM. When MIC HI is grounded, Q21 (normally on) is turned off. A hot-carrier diode (CR24) ensures that Q21 turns off. CR24 is normally off so it does not interfere with the MIC HI line.

CR 19 forces the system to be write-protected during reset; this is especially crucial during system power-up.

## 2. 3 DISPLAY BOARD

This board contains the main operator interface points of the system, including the vacuum fluorescent display, the status indicator LEDs, and the user keypad.

## 2. 3.1 Vacuum Fluorescent Display

The vacuum fluorescent (VF) display is an eleven digit, 14 -segment display that needs three separate voltages to operate: the cathode needs -35 volts to accelerate electrons to the anode; the grid needs -40 volts to totally shut off current flow; the filament needs 3.8 volts AC at 80 mA . These voltages are obtained from the VF up-converter on the controller board.

### 2.3.2 Vacuum Fluorescent Display Driver

This IC (U101) receives ASCII data from the controller board, decodes it into 14-segment display data, and then scans the display with the data. Once properly loaded into the driver, the displayed data is refreshed without any further processor action. The display driver is periodically reset by the actions of transistors Q118, Q119, and Q110 that watch the clock line from the processor to the display driver. When the clock line is held low for more than 600 mSec , the display driver resets and new display data follows.

### 2.3.3 Voltage Supply

The AC voltage present on Q23 of the controller board is used to obtain the -10 volts needed to run the display driver IC. This voltage is fed through L101 to limit the current and then rectified by CR107 and shunt regulated by CR108.

## 2. 3.4 Status LEDs

These LEDs are driven by the display driver as though they were decimal points on the VF display. Level shifting transistors are required for this since the display driver uses 39 volts for control signals.


GPW-3017-A
Figure 3. Disassembly of the Control Unit

### 2.3.5 Backlight LEDs

The same microprocessor signal that turns the VF power supply on and off also operates the backlight LEDs. Q120 supplies base current to the individual LED driver transistors. The driver transistors act as constant current sources to the LEDs. Backlight LEDs CR115, CR116, CR117, and CR118 are connected to thermistor R163 by way of Q108. This circuit allows more current to flow through these LEDs at room temperature and reduces current as the temperature rises.

## 3. Control Unit Maintenance

### 3.1 DISASSEMBLY OF CONTROL UNIT (See Figure 3)

## Note

Before disassembling the control unit, note the location of the labeled buttons.

Remove the two 30 mm slotted screws that hold the front and back of the control unit together. The two halves separate
at the top; at the bottom, they are held together by the flex cable that interconnects the circuit boards. Place the unit so the PC boards are facing up.

Remove the five 8 mm screws in the display board and carefully remove the front of the control unit housing. Keep the front housing parts as a complete unit (including the front housing, buttons, and display board light pipe). Always keep the front of the display housing face down when handling.

Remove the two 16 mm self-tapping screws on the control board. Remove the back of the control unit housing. Remove the black gasket around the switch and set it aside. Remove the shields from the top and bottom of the control board. All components should be easily accessible.

## Note

When working with chips and SOT parts, use extreme caution when heating. Never reuse a chip or SOT part: always replace with correct Motorola parts.

## 3. 2 RE-ASSEMBLY OF THE CONTROL UNIT

Be sure the orange gasket is still around the out side of the control cable "mini D" connector. If it was removed, replace it, ensuring a snug fit to the PC board. Replace the gasket around the power switch. Replace the shiclds on the top and bottom of the control board. Place the control board in the back housing, being careful to put the toggle switch arm in the proper position in the ON/OFF button actuator.

Screw in the two 16 mm self-tapping screws to $6-8$ inch lbs. Also, be sure the ON/OFF actuator still slides back and forth easily. Carefully check to see that all buttons are still in place, then place the display board in the front housing. Screw in the five 8 mm self-tapping screws to $6-8$ inch lbs. Be sure the black gasket is around the outside groove of the front housing. When mating the front and back housings, make sure the flex cable slides behind the control board and is not pinched. Screw in the two 30 mm slotted screw to $9-10^{\prime \prime}$ Ibs.

## 4. Vehicle Interface Ports

The Vehicle Interface Ports (VIP) allow the control unit to operate outside circuits and to receive inputs from outside the control unit. There are three VIP outputs that are used for relay control. There are also three VIP inputs that accept inputs from switches. See the cable kit section for typical connections of VIP input switches and VIP out put relays.

## 4. 1 VIP OUTPUT CONNECTIONS

The VIP output pins are located on the back of the control unit below the area labeled "VIP." These connections are used to control relays. One end of the re lay should be connected to switched $B+$, while the other side is connected to a software controlled ON/OFF switch inside the control unit.

The relay can be normally-on or normally-off depending on how the VIP outputs are configured. The control unit provides for three of these VIP output connections. See Table 3.

The function of these VIP outputs can be defined by field programming the control unit. Typical applications for VIP outputs are external horn/lights alarm and horn ring transfer relay control. For further information on VIP outputs, see the control unit programming manual.

### 4.2 VIP INPUT CONNECTIONS

The VIP input pins are located on the back of the control unit below the area labeled "VIP." These connections are used to accept inputs from switches. One side of the switch is connected to ground while the other side is connected to a buffered input to the control unit. The switch can be nor-mally-closed or normally-open depending on how the VIP inputs are configured. The control unit permits three of these VIP input connections. See Table 4.

The function of these VIP inputs is defined by field programming the control unit. Typical applications for the VIP inputs are for a foot switch or a horn ring switch. For further information on VIP inputs, sce the control unit programming manual.

## 5. Power Connections

## CAUTION

Use only SYNTOR X 9000 cable kits. Connection to other cable kits or control panels may cause electrical damage.

Replace the fuse in the in-line fuscholder of the red power cable coming from the radio in the trunk. Also connect the green (and/or orange) fused wire(s) coming from the control unit to the ungrounded terminal (or source) of the battery.

Pull all excess cabling into the trunk. Clamp the cables to the vehicle body or chassis with the cable clamps supplied. Drill $1 / 8$ " mounting holes, then attach the clamps with four \#8 by $3 / 8$ " tapping screws and four $1 / 4$ " lockwashers. Finally, be sure all in-line fuses are installed.

Table 3 . VIP Output Connections

| VIP OUTPUT NO. | SWITCHED B+ PIN NO. | ON/OFF SWITCH <br> PIN NO. | DEFAULT FUNCTION IS CHANGED <br> WITH FIELD PROGRAMMER |
| :---: | :---: | :---: | :--- |
| 1 | 18 | 2 | HORN RELAY (ALARM) |
| 2 | 19 | 1 | LIGHT RELAY (ALARM) |
| 3 | 35 | 34 | SIREN-HORN TRANSFER |

Table 4. VIP Input Connections

| VIP INPUT NO. | GROUND PIN NO. | ON/OFF SWITCH <br> PIN NO. | DEFAULT FUNCTION IS CHANGED <br> WITH FIELD PROGRAMMER |
| :---: | :---: | :--- | :--- |
| 1 | 20 | 4 | SIREN; HORN RING |
| 2 | 21 | 3 | EMERGENCY (IF OPTION PRESENT) |
| 3 | 36 | 37 | NONE |




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& \text { PW-4385-B }
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| (Sheet 2 of |
| :--- |
| $8: 30188$ |



COMPONENT SIDE VIEW


SHown from soloer side

parts list $\qquad$



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function
he palm microphone contains an amplificict to provic the radio with a high--level, noise-free audio input. The
microphone also provides push--to-talk transmit control or the radio as weil as off-hook channel monitoring (PL/DPL squelch disable) capability.



[^0]:    1. The orange and green power cables connect to either the vehicle battery or the ignition switch. Connect the green cable directly to the battery. The receiver operates when the control head is on. Connect the orange cable to the ignition switch. The transmitter operates only when the ignition switch is on. Alternate connectionsConnecting both green and orange cables to the battery allows the control head to turn the receiver and transmitter on or off. Connecting both green and orange cables to the ignition switch allows the ignition switch to turn the receiver and transmitter on or off. (Alternator whine and other noise problems may occur. Isolate the green cable with a Motorola relay, part \#59-00813674.)
    2. The radio primary power cable (red) comes in two parts. One is part of the radio control cable kit that goes from the radio to the engine compartment. The other comes with an in-line fuse on one end and a ring lug on the other end.
[^1]:    

[^2]:    - Failure of the switched 5.0 and 9.6 volt regulators
    - Failure of the unswitched 5.0 volt regulator ONLY
    - Failure of the 9.6 volt regulator ONLY
    - Failure of the switched 5.0 volt regulator ONLY

