

MAINTENANCE MANUAL

138-174 MHz PHASE LOCK LOOP EXCITER 19D423249G1 & G2

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DESCRIPTION

The Phase Locked Loop (PLL) Exciter is a crystal controlled, frequency modulated, wideband exciter designed for multi-frequency operation (1 through 8) with wide channel spacing in 138-174 MHz frequency band. The wideband exciter utilizes a phase locked loop to provide a maximum transmitter frequency spacing of up to 17 MHz in the 138-155 MHz range or up to 24 MHz in the 148-174 MHz range. The frequency range is determined by the response of the plug-in bandpass filter and the core in L101. The solid state exciter uses integrated circuits (IC's) and discrete components to provide 250 milliwatts of RF power to the PA assembly. The exciter is used in standard and Voice Guard applications.

The operating frequency is selected by the channel selector switch on the control unit and is determined by the FM ICOM associated with the selected channel. The crystal frequencies range from approximately 11.5 to 14.5 MHz and are one-twelfth the RF carrier frequency. Oscillator stability is maintained within $\pm 0.0005\%$ or $\pm 0.0002\%$.

Except for individual frequency trimmer adjustments on the FM ICOMS and the modulation controls, only one tuning control, L101, in the voltage controlled oscillator (VCO) cirucit, is used to center tune the exciter for all operating frequencies. For this reason, a centralized metering jack to monitor exciter operation is not applicable. The exciter RF output power is metered by the PA metering jack.

The PLL exciter utilizes the divided VCO frequency (Countdown train), phase detector, and a feedback path to lock the

output frequency of the VCO to the 12th multiple of the FM ICOM frequency.

CRICUIT ANALYSIS

The phase detector compares the 3rd harmonic of the FM-ICOM with the output frequency of the VCO (divided by 4) to derive an error voltage proportional to the frequency and phase difference of the two inputs. The error voltage is amplified, passed through a lead/lag filter and applied to a varactor which instantaneously corrects the output frequency and phase of the VCO to the 12th multiple of the FM ICOM frequency.

After the VCO frequency is locked, (a maximum of 20 milliseconds), the RF amplifiers are turned on and the RF carrier output is presented to the PA.

Temperature compensation is provided in the audio and voltage regulator circuits to assure frequency stability and distortion free communications over the specified operating termperature range.

References to symbol numbers mentioned in the text are found on the block diagram, schematic diagram, outline diagram and parts list. Figure 1 is a block diagram of the PLL exciter.

Audio, supply voltages and control functions are connected from the system board to the exciter board through P902.

The PLL exciter contains up to eight FM ICOMs, an Audio processor and amplifier, bandpass filter, harmonic amplifier, phase lock loop, RF amplifiers, frequency lock detector, voltage regulators and temperature compensation circuits.

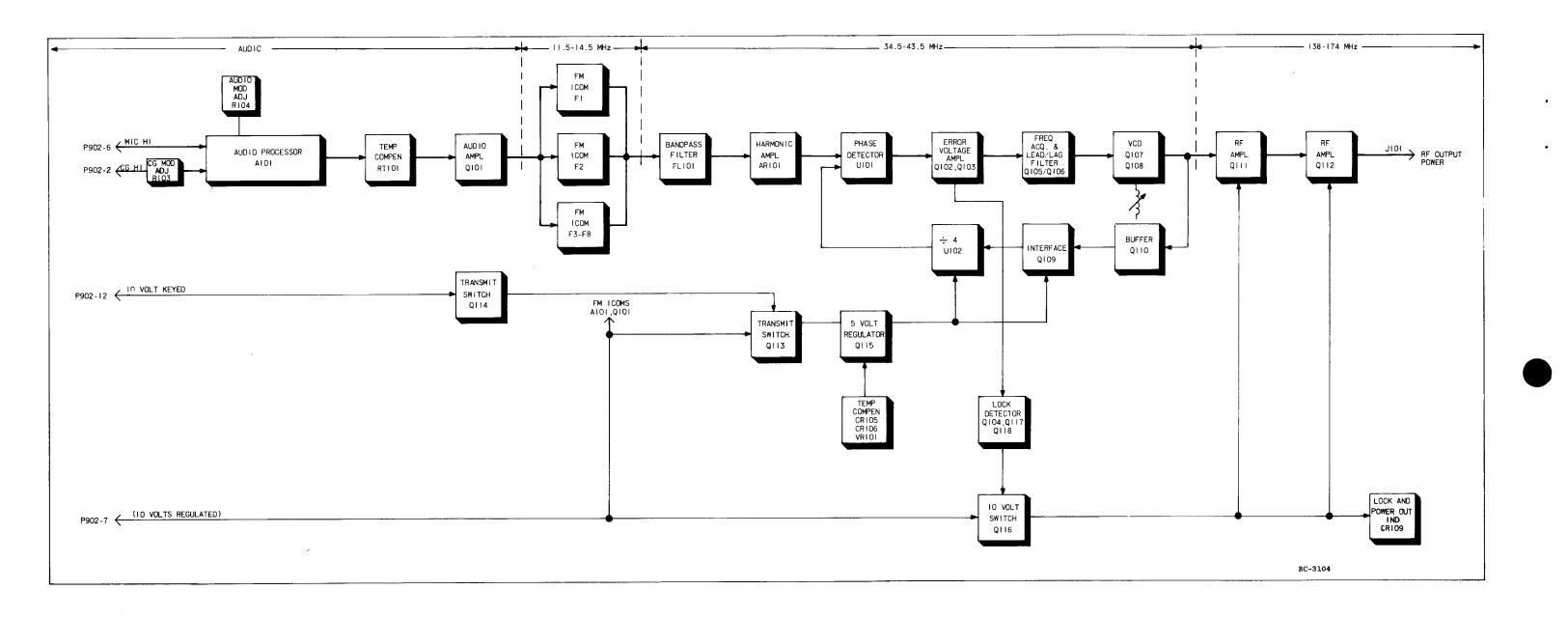


Figure 1 - Block Diagram

FM ICOMS (Frequency Modulated)

Three different types of FM ICOMs are available for use in the exciter. Each ICOM contains a crystal-controlled Colpitts oscillator, and two of the ICOMs contain compensator ICs. The different FM ICOMs are:

5C-FM ICOM - contains an oscillator and a 5 part-permillion (±0.0005%) compensator IC. Provides compensation for EC-ICOMs.

EC-FM ICOM - contains an oscillator only. Requires external compensation from a 5C-ICOM.

2C-FM ICOM - contains an oscillator and a 2 PPM (±0.002%) compensator IC. Will not provide compensation for an EC-FM ICOM.

The ICOMs are enclosed in an RF shielded can with the type ICOM (5C-FM ICOM, EC-FM ICOM or 2C-FM ICOM) printed on the top of the can. Access to the oscillator trimmer is obtained through a hole in the top of the can.

Frequency selection is accomplished by switching the ICOM keying lead (terminal 9) to A- by means of the frequency selector switch on the control unit. In single-frequency radios, a jumper from H9 to H10 in the control unit connects terminal 9 of the FM ICOM to A-. The oscillator is turned on by applying a keyed +10 Volts to the external oscillator collector load resistor, R153, which forward biases an internal diode switch.

The FM ICOMs have an audio input which receives audio from the audio processor circuit. Therefore, with Modulation present, the output frequency of the "FM" ICOM varies at an audio rate.

- CAUTION -

All ICOMs are individually compensated at the factory and cannot be repaired in the field. Any attempt to repair or change the ICOM frequency will void the warranty.

In standard 5 PPM radios using EC-FM ICOMs, at least one 5C-FM ICOM or 5C ICOM must be used. The 5C ICOM is normally used in the receiver F1 position, but can be used in any receive position. A 5C-FM ICOM can be used in any transmit position.

The EC and 5C type ICOMs are not interchangeable with EC-FM or 5C FM type ICOMs. The EC and 5C type ICOMs are used only in the receivers. While the EC-FM and 5C-FM type ICOMs are always used in the transmitter.

One 5C ICOM or 5C-FM ICOM can provide compensation for up to 15 EC ICOMs or EC-FM ICOMs in the transmitter and receiver. Should the 5C ICOM or the 5C-FM ICOM compensator fail in the open mode, the EC-FM ICOMs will still maintain 2 PPM frequency stability from 0°C to 55°C (+32°F to 131°F) due to the regulated compensation voltage (5 Volts) from the 10 Volt regulator IC. If desired, up to 8 5C-FM ICOMs may be used in the radio.

The 2C-FM ICOMs are self-compensated at 2 PPM and will not provide compensation for EC-FM ICOMs.

Oscillator Circuit

Quartz crystals used in ICOMs exhibit the traditional "S" curve characteristics of output frequency versus operating temperature.

At both the coldest and hottest temperatures, the frequency increases with increasing temperature. In the middle temperature range (approximately 0°C to 55°C), frequency decreases with increasing temperature.

Since the rate of change is nearly linear over the mid-temperature range, the output frequency change can be compensated by choosing a parallel compensation capacitor with a temperature coefficient approximately equal to and opposite that of the crystal.

Figure 2 shows the typical performance of an uncompensated crystal as well as the typical performance of a crystal which has been matched with a properly chosen compensation capacitor.

At temperatures above and below the mid-range, additional compensation must be introduced. An externally generated compensation voltage is applied to a varactor (voltage-variable capacitor) connected in parallel with the crystal. Refer to Figure 3 for a simplified diagram of the FM ICOM.

A constant bias of 5 Volts (provided from Regulator IC U901 connected in parallel with the compensator) maintains varactor capacity at a constant value over the entire mid-temperature range. This compensation voltage achieves the ±2 PPM stability.

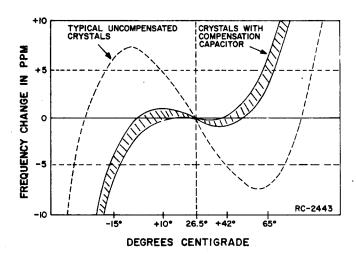


Figure 2 - Typical Crystal Characteristics

Modulation is accomplished with a hyperabrupt varicap connected in series with the crystal feedback capacitors. The varicap impedance is the dominant impedance in the loop. This allows large swings of load capacity with modulation, therefore, large frequency shifts are achieved for the modulated input. Biasing for the modulation varicap is provided by a voltage divider, R152 and R163, connected across the 10 volt regulator input at P902-7. A bias voltage of 6.2 volts is applied to pin 6 of all ICOMs.

Compensator Circuits

Both the 5C-ICOMs and 2C-FM ICOMs are temperature compensated at both ends of the temperature range to provide instant frequency compensation.

The cold end compensation circuit does not operate at temperatures above 0°C. When the temperature drops below 0°C, the circuit is activated. As the temperature decreases, the equivalent resistance decreases and the compensation voltage increases.

An increase in compensation voltage decreases the capacitance of the varactor in the oscillator, thereby increasing the output frequency of the ICOM.

The hot end compensation circuit does not operate at temperatures below +55°C. When the temperature rises above +55°C, the circuit is activated. As the temperature increases, the equivalent resistance decreases and the compensation voltage decreases. The decrease in compensationn voltage increases the capacity of the varactor, decreasing the output frequency of the ICOM.

Proper ICOM operation is dependent on the closely-controlled input voltages for the 10-Volt regulator. Should all of the ICOMs shift off frequency, check the 10-Volt regulator module.

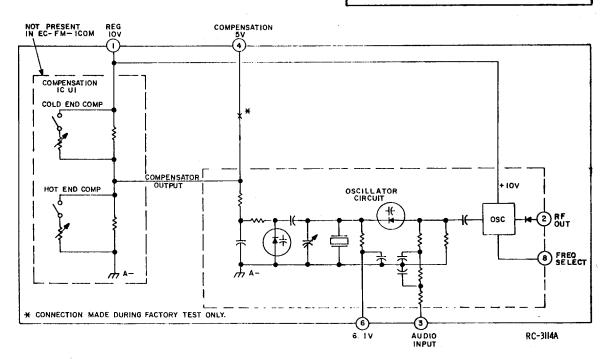


Figure 3 - Equivalent FM-ICOM Circuit

AUDIO PROCESSOR A101

The transmitter audio processor contains audio circuitry consisting of two operational amplifiers, AR101-A and -B, a pre-emphasis circuit with amplitude limiting and a post limiter filter. A total gain of approximately 24 dB is realized through the audio processor. Twenty dB is provided by AR101-B and 4 dB by AR101-A.

The 10 Volt regulator powers the audio processor and applies regulated +10 V thru P902-6 to a voltage divider consisting of R108 and R110. The +5 V output from the voltage divider establishes the operating reference point for both operational amplifiers. C107 filters out any noise that may be on the 10 Volt line to assure a stable voltage supply to the operational amplifiers.

Resistors R105, R106, and R107 and diodes CR101 and CR102 provide limiting for AR101-B. Diodes CR101 and CR102 are reverse biased by +5 VDC on AR101B-6 and voltage divider network R105, R106 and R107. The voltage divider network provides +7 VDC at the cathode of CR101 and +3 VDC at the anode of CR102. C102 and C103 permit a DC level change between AR101B-7 and the voltage divider network for diode biasing.

When the input signal at AR101B-6 is of a magnitude such that the amplifier output at AR101B-7 does not exceed 4 volts P-P, the amplifier provides a nominal 20 dB gain. When the audio signal level at AR101B-7 exceeds 4 volts PP, diodes CR101 and CR102 conduct on the positive and negative half cycles providing 100% negative feedback to reduce the amplifier gain to 1. This limits the audio amplitude at AR101B-7 to 5 volts PP.

Resistors R102, R103, and R104 and C104 comprise the audio pre-emphasis network that enhances the signal to noise ratio. R104 and C104 control the pre-emphasis curve below limiting. R103 and C104 control the cut-off point for high frequency pre-emphasis. As high frequencies are attenuated, the gain of AR101 is increased.

Audio from the microphone is applied to the audio processor at P102-1 and coupled to the input of operational amplifier AR101-B through R101 and C101.

The amplified output of AR101-B is coupled through P102-4 audio MOD ADJ control R104, R102-3, C106, R112 and R113 to a second operational amplifier AR101-A. Audio MOD ADJ control is set for a deviation of 4.5 kHz.

The Channel Guard tone input is applied to the audio processor through

P902-2, CG MOD ADJ R103 to P102-5. The CG tone is then coupled through C105 and R111 to AR101A-2 where it is combined with the microphone audio. AR101-A provides a signal gain of approximately 4 dB.

A post limiter filter consisting of AR101A, R112-R114, C108, and C109 provide 12 dB per octave roll off. R109 and C111 provide an additional 6 dB per octave roll off for a total of 18 dB.

R112-R114 are 1% resistors. This tolerance must be maintained to assure proper operation of the post limiter filter. Use exact replacements.

The output of the post limiter filter is coupled through C110 and P102-9 to the temperature compensated audio amplifier Q101.

AUDIO AMPLIFIER, BANDPASS FILTER, AND HARMONIC AMPLIFIER

The output of the audio processor is presented to audio amplifier Q101 through temperature compensator and biasing network consisting of RT101, R108 and R109. RT101, with a nominal resistance of 50 ohms from 25°C to 70°C, maintains a constant modulation index over the normal operating temperature range. The resistance of RT101 increases with a decrease in temperature below 25°C, thereby decreasing the signal drive to audio amplifier Q101. Audio amplifier Q101 has a nominal gain of 2. The temperature compensated audio is applied to pin 3 of the FM ICOM. A varactor within the FM ICOM is used to modulate the carrier frequency at the audio rate. The output of the FM ICOM is taken from pin 2 and applied to the bandpass filter.

The bandpass filter is a passive device with sharp frequency cutoff characteristics that pass only the 3rd harmonic. The fundamental frequency and all other harmonics are suppressed by at least 30 dB. The 3rd harmonic is amplified by high frequency harmonic amplifier AR101. The harmonic amplifier circuit has a high input impedance and provides a nominal power gain of 10. The output of AR101 is presented to pin 4 of phase detector U101 in the phase lock loop. Bandpass filter 19B226748G1 is used for frequencies between 138-155 MHz while bandpass filter 19B226748G2 is used for frequencies between 148-174 MHz.

PHASE LOCK LOOP

Phase detector U101, error voltage amplifier Q102 and Q103, frequency

acquisition and lead/lag filter circuit Q105 and Q106, voltage controlled oscillator circuit (VCO) Q107 and Q108, buffers Q109 and Q110, and frequency divider U102 form a phase locked loop. The PLL locks the VCO frequency to the 12th multiple of the FM ICOM frequency to provide the RF carrier output frequency. The phase locked loop locks the output of the VCO in frequency and in phase.

Phase detector U101 is a doubly-balanced modulator used to detect the difference (frequency and phase) between the divided frequency from the VCO and the 3rd harmonic of the FM ICOM and to provide a resultant error voltage output. The error voltage is directly proportional to the frequency/phase error.

When the frequency input from VCO (+4) is exactly the same as the frequency received from the harmonic amplifier, the output of the phase detector will be 8.0 VDC. If the two input signals are not at the same frequency, the output of the phase detector will be a DC voltage with an AC component equal to the difference frequency. This error voltage is amplified and applied to the VCO to correct and lock the VCO to the operating frequency. Biasing of the phase detector is arranged so that both inputs must be present for normal operation. Lack of either input will cause the voltage at U101-6 to rise to its maximum value (approximately 8.2 VDC).

DIFFERENTIAL ERROR VOLTAGE AMPLIFIER

Q103 comprise and differential amplifier pair. Q103 is the reference amplifier that establishes the operating point against which error voltage amplifier Q102 operates. The operating point is established by a biasing network consisting of R127, R128, and C128. The differential amplifier pair translates the error signal and amplifies it to a level large enough to control the VCO. The error voltage detected by the phase detector is amplified by Q102 and applied to the emitter of reference amplifier Q103. The collector voltage of Q103 varies in proportion to the error voltage. When there is no frequency or phase error, there will be no varying error voltage. The collector voltage of Q103 is determined by its biasing network and the frequency assignments and spacing of the assigned transmitting frequencies. This voltage may be stable over a range of 3.4 to 6.4 Volts. A second output from the error voltage amplifier (taken from Q102-C) is applied to the lock detector (Q104, Q117, and Q118) to control the RF Amplifiers.

Lock detector/DC threshold control R171 controls the threshold level differential amplifier Q102, providing compensation for different output characteristics of U101. It is set for 1.8 ± 0.1 VDC as measured at Q102-C (top of R129) with the transmitter keyed and an unused channel selected.

R171 is preset at the factory and normally does not require field adjustment. However, if Q102, Q103, or U101 is replaced, readjustment may be necessary.

ACQUISITION CIRCUIT AND LEAD/LAG FILTER

The acquisition circuit consists of Q105 and Q106. The lead/lag filter circuit consists of R133, R135, R168, C129, and C130.

The lead/lag network controls the loop phase to provide frequency and phase stability and sets the bandwidth to about 20 kHz. The output of the differential error voltage amplifier is applied to the lead/lag filter. The lead/lag filter corrects the phase of the error signal applied to varactor CR102 to maintain loop stability. The varactor alters the frequency and phase of the VCO to stabilize the VCO at the RF output frequency.

During initial acquisition (when the transmitter is first keyed), the error signal from the differential error voltage amplifier will contain useful information far outside the normal bandwidth of the phase locked loop. For this reason, the acquisiton circuit consisting of Q105 and Q106 is used to greatly increase the bandwidth. When an error signal with high frequency components is present and that has sufficient amplitude, eithr Q105 or Q106 will turn on. Q105 has the capability of increasing the voltage applied to varicap CR102 to a nominal 8.5 V while Q106 has the capability of lowering the varicap voltage to less than 1 Volt. This wide range of voltage being applied to varicap CR102 permits large and instantaneous frequency range. As the free running frequency of the VCO approaches the operating frequency, Q105 or Q106 turns off to permit final acquisition and phase lock. Frequency acquisition, and RF power output occurs in less than 20 milliseconds after the Tx lead is keyed.

Test point TP101 monitors the voltage applied to the varicap and is used to optimize the VCO frequency over the operating range.

_____ NOTE -

When adjusting the VCO voltage, always be sure to use a high impedance meter (10 megohm input impedance minimum).

The voltage at TP101 varies directly with frequency, (as the voltage increases, the frequency increases) and may range from $+3.4~\rm V$ to $6.4~\rm V$; however, the normal operating voltage is optimized around $+5.0~\rm V$.

VCO (VOLTAGE CONTROLLED OSCILLATOR)

The VCO consists of two FET's, Q107 and Q108, connected in a cascade configuration with total feedback through C137 to provide instantaneous starts. The VCO operates over the output frequency range of 138-174 MHz. The free running frequency of the VCO is adjusted by L101 and is optimized by center tuning the free running frequency (TP101 at +5 V) between the highest and lowest operating frequencies. One of two cores are used in L101 to adjust the frequency (voltage) measured at TP101. One core is used for the 138-155 MHz range (ferrite) and a second core (aluminum) is used for the 148-174 MHz range.

BUFFER, INTERFACE AND FREQUENCY DIVIDER

RF output power from the VCO is taken from Q107 through a 4:1 step down transformer T101 and applied to the RF Amplifier and the feedback leg of the phase lock loop. The feedback leg of the phase lock loop consists of buffer Q110, interface Q109, and frequency divider U102.

The input to buffer Q110 is coupled through isolating resistor R139 and capacitor C148. Biasing for Q110 is provided by R149 and R150. The output of Q110 is taken from the collector and coupled through C149 to the base of emitter follower interface transistor Q109. Biasing for Q109 is provided by a voltage divider network consisting of CR104, R145, and R146. The output of interface transistor Q109 is taken from the emitter and applied directly to the input of frequency divider U102. The frequency divider divides the VCO frequency (assigned operating) by 4 and supplies it as the second input to the phase detector. The output of the frequency divider is compared frequency and phase with the 3rd harmonic of the selected FM-ICOM frequency to maintain the VCO output frequency at the 12th multiple of the FM ICOM frequency. Operating voltage for interface transistor Q109 and frequency divider Q102 is provided by a temperature compensated +5 Volt regulator, Q115.

RF AMPLIFIERS

The wideband RF Amplifiers, Q111 and Q112, supply a minimum of 250 milliwatts of RF power at the carrier frequency to the power amplifiers. Q111 receives its input from the 4:1 step down transformer through coupling capacitor C138. It is biased for Class A operation by a biasing network consisting of R140 and R141.

The output of Q111 is taken from the collector and coupled to class C amplifier Q112 through L104 and C130. The RF Amplifier provide 250 milliwatts of RF power to J101 through L105 and C142.

DC power for the RF Amplifiers is controlled by 10 Volt switch Q116 and is not applied until the VCO output frequency is stable and locked on frequency.

LOCK DETECTOR AND 10 VOLT SWITCH

The lock detector monitors the operation of the differential error voltage amplifier and turns the RF Amplifiers on when the VCO is locked on frequency or turns them off if the VCO begins to vary or if one of the inputs to the phase detector is missing.

The lock detector consists of voltage doubler CR107, CR108, and C127, DC switch Q104, and Schmitt trigger Q117 and Q118.

When the VCO frequency is not locked with the FM ICOM frequency, the phase detector output at U101-6, instead of being a stable DC level (≈ 8.0 Volts), will be a DC level with an AC component varying at the beat (difference) frequency of the two inputs. The AC component is rectified by the voltage doubler, filtered by C169 and R162. resultant DC voltage turns on DC switch Q104, lowering the base voltage of Schmitt trigger Q117. Q117 then turns off, allowing the base voltage of 10 volt switch Q116 to increase and turn it off. With Q116 turned off, +10 V is removed from the RF amplifiers, thereby removing the RF input to the PA. The collector of Q117 is also tied back to the base of Q118, the second stage of the Schmitt trigger. The increase in base voltage at Q118 causes it to turn on and raise the emitter voltage of Q117. With an increase in emitter voltage, Q117 is held off. The lock detect and control circuits and the RF amplifiers will remain in this state until the VCO achieves stability and is locked on frequency. The two inputs to the phase dectector must be synchronous for normal operation.

When either of the two inputs to the phase detector is absent, the phase detector output will increase to approximately +8.2 Volts dues to pull up

resistor R121. The increase in base voltage turns differential error voltage amplifier Q102 off causing the collector of Q102 to decrease to A- through R125. A- from the collector of Q102 is applied through R129 to the base of Schmitt trigger Q117, causing Q117 to turn off. With Q117 turned off, the base voltage of Q116 increases to near +10 V causing Q116 to turn off and remove voltage from RF Amplifiers Q111 and Q112.

Normally, Q117 is in the on condition, which allows 10 Volt switch Q116 to conduct and apply voltage to the RF amplifiers. RT102 in the base circuit of Q117 provides a temperature compensated reference for Q117 over the normal operating temperature range. The value of RT102 is approximately 2200 ohms.

LOCK DETECT INDICATOR

Lock detect indicator LED CR109 monitors the state of 10 Volt switch Q116. When Q116 is on and power is applied to the RF Amplifiers indicator CR109 is on. When the VCO voltage at TP101 is varying, or when one of the two inputs to the phase detector is lost, Q116 is switched off and indicator CR109 is out.

TRANSMIT SWITCH

The transmit switch applies +10 Volts to the exciter when the PTT switch

is operated. It consists of control transistor Q114 and 10 Volt switch Q113.

When the PTT switch is operated, +10 V (keyed) is applied to the base of Q114, turning it on. The collector of Q114 goes low turning 10 Volt switch Q113 on. Q113 controls the 10 Volt regulated input to the +5 Volt temperature compensated regulator Q115, pin 2 of the FM ICOMs, AR101, U101, Q102 and Q103, Q105 and Q106, and Q107 and Q108. 10 Volt regulated input power is applied directly to 10 Volt switch Q116, controlling the RF Amplifiers, pin 10 of all FM ICOMs, A101 and Q101.

+5 VOLT REGULATOR

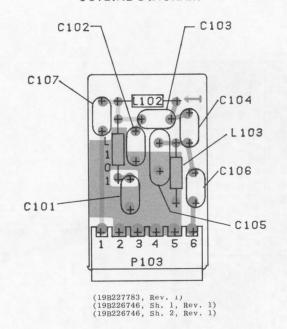
The +5 Volt regulator receives a regulated 10 Volt input from Q113 and supplies a temperature compensated +5 Volt output to buffer interface transistor Q109 and frequency divider U102. A 4.4 Volt zener diode VR101 and two series connected diodes (CR105 and CR106) having a positive temperature coefficient comprise the temperature compensating network.

- NOTE -

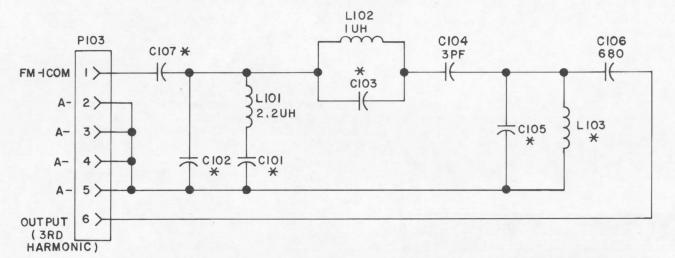
Due to the temperature compensation characteristics of CR105 and CR106, only exact replacement diodes should be used. See parts list.



GE Mobile Communications



SCHEMATIC DIAGRAM

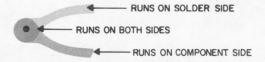


* C	MPONENT VALUE	CHART						
	138-155 MHZ(L)▲	148-174MHZ(H)▲						
CIOI	I5 PF	I2 PF						
C102	18 PF	15 PF						
C103	15 PF	12 PF						
C105	56 PF	51 PF						
C107	IO PF	9 PF						
L103	0.33UH	.27 UH						

BANDPASS FILTER	REV LETTER	FREQUENCY RANGE
19B226748GI		138 -155MHZ▲
19B226748G2		148-174MHZ ▲

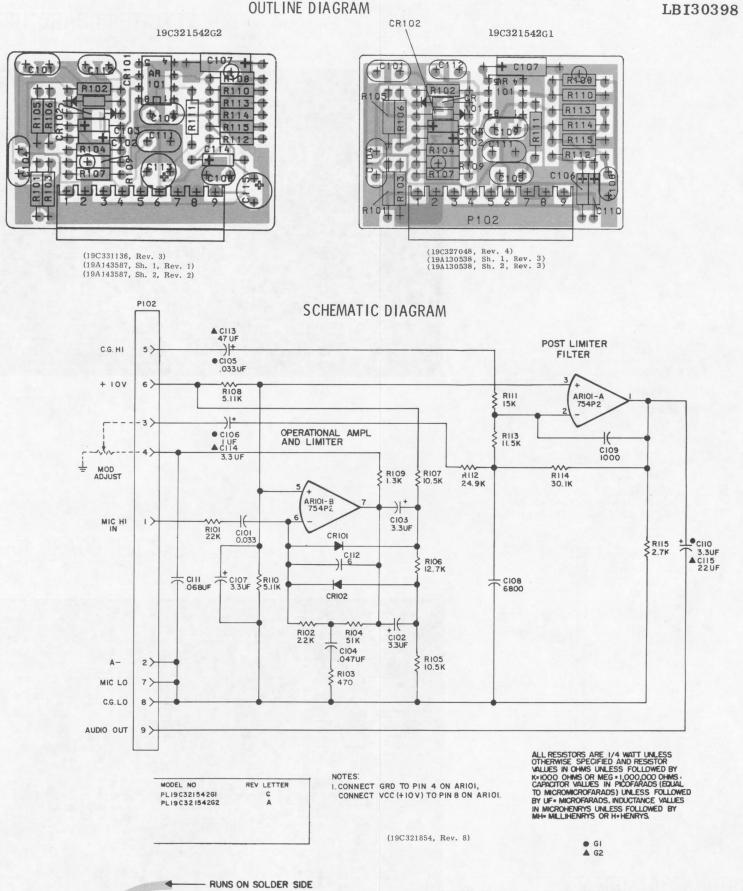
▲ TRANSMITTER OUTPUT FREQUENCIES

(19B227106, Rev. 3)



OUTLINE & SCHEMATIC DIAGRAM

138-174 MHz BAND PASS FILTER



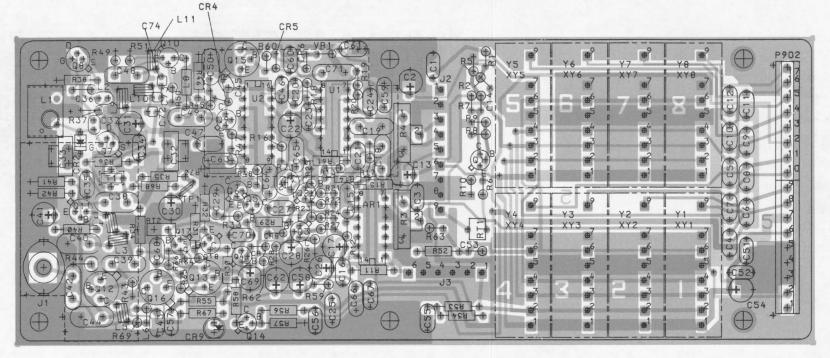
RUNS ON BOTH SIDES

- RUNS ON COMPONENT SIDE

OUTLINE & SCHEMATIC DIAGRAM

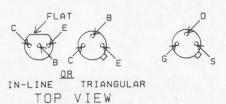
AUDIO PROCESSOR

EXCITER BOARD 19D423249G1



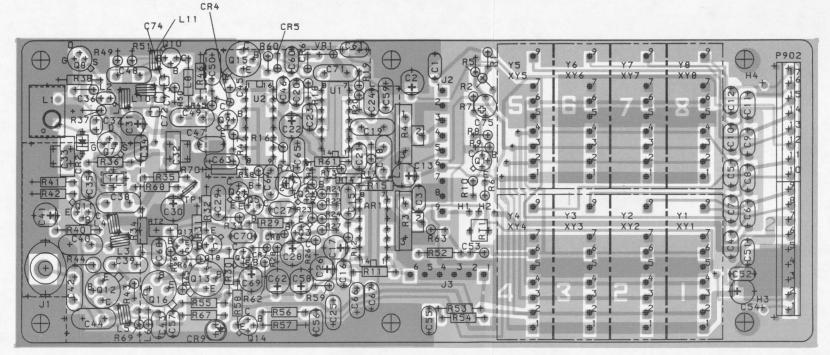
RUNS ON SOLDER SIDE RUNS ON BOTH SIDES - RUNS ON COMPONENT SIDE

LEAD IDENTIFICATION FOR Q1 THRU Q6, Q9 THRU Q18 Q7 AND Q8

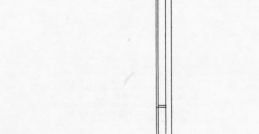


NOTE: LEAD ARRANGEMENT, AND NOT CASE SHAPE, IS DETERMINING FACTOR FOR LEAD IDENTIFICATION.





(19D432754, Rev. 1) (19A143781, Sh. 1, Rev. 2) (19A143781, Sh. 2, Rev. 1)



OUTLINE DIAGRAM

138—174 MHz PHASE LOCK LOOP EXCITER

10 Issue 6



CR4 THRU CR8 AND VR1

PARTIAL REFERENCE DESIGNATIONS ARE SHOWN. FOR COMPLETE DESIGNATIONS, PREFIX WITH 100 SERIES. EXAMPLE: C1-C101, R1-R101 ETC.

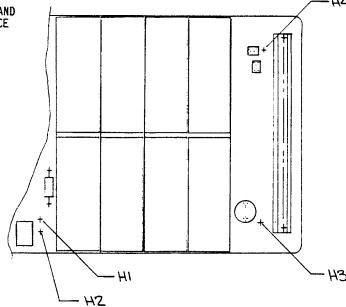
EXCEPT P902.



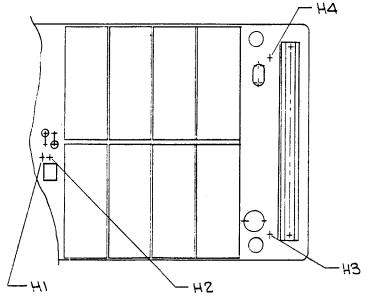
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THIS INSTRUCTION MODIFIES A HIGH BAND OR UHF MASTR II FM EXCITER FOR VOICE GUARD OPERATION.

- 1. REMOVE JUMPER BETWEN H1 & H2.
- 2. SOLDER SF24-R FROM H1 TO H3. (PL19B234774G1).
- SOLDEK SF24-R FROM H2 TO H4. (PL19B234774G1)



EXCITER BOARD (UHF)
PLISD432679



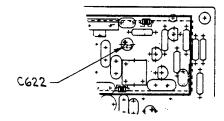
EXCITER BOARD HB PLIPD 423249



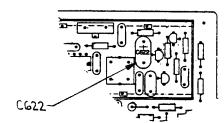
THIS INSTRUCTION MODIFIES A HIGH BAND OR UHF MASTR II RECEIVER IFAS BOARD FOR VOICE GUARD OPERATION.

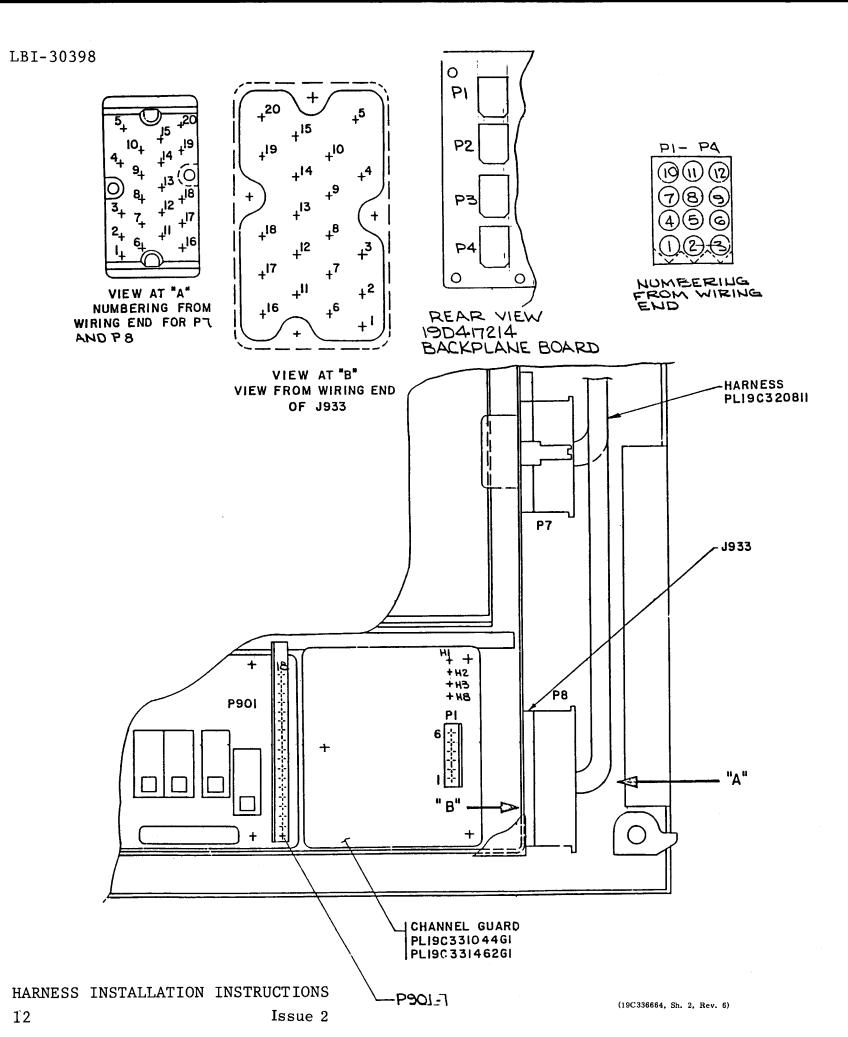
- 1. REMOVE COVER FROM FM DETECTOR AREA.
- REPLACE C622(0.47 UFD) WITH A 10 UFD CAPACITOR PART NUMBER 315A6047P106N (OBSERVE CORRECT POLARITY).
- 3. REPLACE COVER.

IF/AUDIO/SQUELCH BOARD 19D432667GI



IF/AUDIO/SQUELCH BOARD
19D417707G1





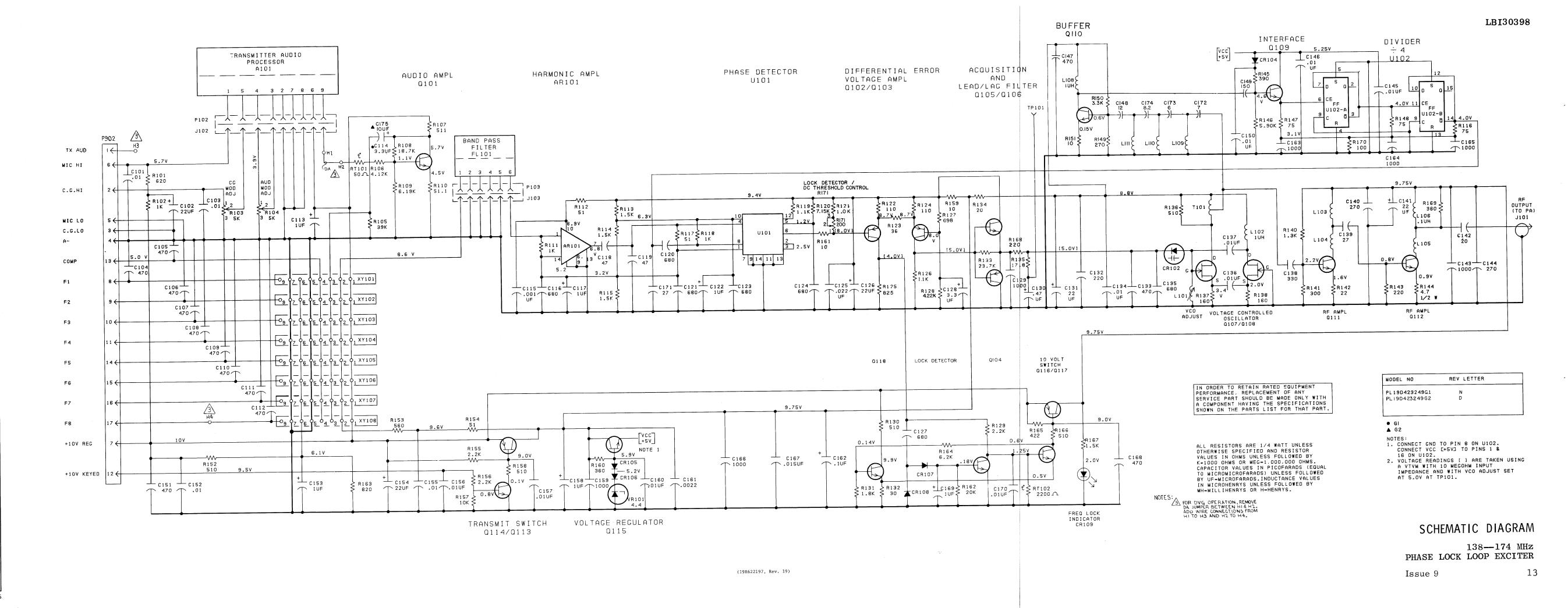
- THESE INSTRUCTIONS COVER THE INSTALLATION OF CABLE HARNESS PL19C851484 62 & 63
 - INSTALL DA JUMPER BETWEEN H3 & H8 ON CG ENCODER. IF H8 NOT PRESENT CUT TERRINAL FROM WRBL WIRE (PL19234774G3) AND SOLDER TO H3. CONNECT OTHER END TO J933-18 AND SPOT TIE TO EXISTING CHANNEL GUARD HARNESS. SKIP TO STEP 3 IF H8 IS NOT PRESENT.
 - 2. IF H8 IS PRESENT, INSTALL WRBL WIRE (PL198234774G3) IN P1-2 & SOLDER OTHER END TO J933-18 & SPOT TIE TO EXISTING CHANNEL GUARD HARNESS.
 - 3. INSTALL YELLOW WIRE (PL19823477464) IN P901-2 & SOLDER OTHER END TO J933-19 & SPOT TIE TO EXISTING EXCITER HARNESS.
 - 4. INSTALL ORANGE WIRE (PL198234774G2) IN P901-18 & SOLDER OTHER END TO J933-20 & SPOT TIE TO EXISTING EXCITER HARNESS.
 - 5. INSTALL ORANGE WIRE PART OF PL19C851484G2 HARNESS IN P3-9 SOLDER OTHER END TO P8-20. INSTALL YELLOW WIRE PART OF PL19C851484G2 HARNESS IN P4-2 & SOLDER OTHER END TO P8-19. INSTALL WRBL WIRE PART OF PL19C851484G2 HARNESS IN P4-9 & SOLDER THE OTHER END TO P8-18. SPOT TIE THE PL19C851484G2 HARNESS TO EXISTING PL19C320811 HARNESS.
- THESE INSTRUCTIONS COVER THE INSTALLATION OF CABLE HARNESS PL19C85148463 AND PL19B23484161.
 - 1. DO STEPS 1 THRU 4 OF PART 2 ABOVE.
 - 2. INSTALL YELLOW WIRE PART OF PL19B234841G1 HARNESS IN P1-1 SOLDER OTHER END TO P7-5. INSTALL WHITE-RED WIRE PART OF PL19B234841G1 HARNESS IN P4-9 SOLDER OTHER END TO P8-18. INSTALL WHITE-BLUE-BLACK WIRE PART OF PL19B234841G1 HARNESS IN P4-2 SOLDER OTHER END TO P8-19. INSTALL WHITE-ORANGE WIRE PART OF PL19B234841G1 HARNESS IN P3-9 SOLDER OTHER END TO P8-20.
 - 3. SPOT TIE PL19B23484161 TO EXISTING PL19C320811 HARNESS WITH CABLE CLAMPS SUPPLIED WITH PL19B23484161 HARNESS.
- 5) 800 MHz PST 19B234774GB
 - 1. INSTALL YELLOW WIRE IN P901-2 & SOLDER OTHER END TO J933-19.
 - INSTALL W-O WIRE IN P901-15 AND SOLDER OTHER END TO J933-20. SPOT TIE YELLOW AND GRANGE WIRES TO EXISTING EXCITER HARNESS.
 - 3. REMOVE DA WIRE BETWEEN 1933-4 AND 1933-8.

PARTS LIST

LBI30401K

138-174 MHz 19D423249G1 HB, PHASE LOCK LOOP 19D423249G2 HB, DIGITAL CHANNEL GUAI

	SYMBOL	GE PART NO.	DESCRIPTION							
	AR101	19A134441P1	Harmonic Amplifier.							
-			CAPACITORS							
ļ	C101	19A700005P7	Polyester: 0.01 uF ±10%, 50 VDCW.							
-	C102	19A134202P6	Tantalum: 22 uF ±20%, 15 VDCW.							
	C103	19A700005P7	Polyester: 0.01 uF ±10%, 50 VDCW.							
	C104 thru C112	19A116655P14	Ceramic disc: 470 pF \pm 10%, 1000 VDCW; sim. to RMC Type JF Discap.							
ı	C113	19A134202P14	Tantalum: 1 uF ±20%, 35 VDCW.							
	C114	5491674P36	Tantalum: 3.3 uF $\pm 20\%$, 10 VDCW; sim to Sprague Type 162D.							
	C115	19A116655P19	Ceramic disc: 1000 pF $\pm 20\%$, 1000 VDCW; sim to RMC Type JF Discap.							
	C116	19A116655P18	Ceramic disc: 680 pF $\pm 10\%$, 1000 VDCW; sim to RMC Type JF Discap.							
	C117	19A134202P14	Tantalum: 1 uF ±20%, 35 VDCW.							
	C118 and C119	19A700105P26	Mica: 47 pF <u>+</u> 5%, 500 VDCW.							
	C120 and C121	19A116655P18	Ceramic disc: 680 pF ±10%, 1000 VDCW; sim to RMC Type JF Discap.							
	C122	19A134202P14	Tantalum: 1 uF ±20%, 35 VDCW.							
	C123 and C124	19A116655P18	Ceramic disc: 680 pF ±10%, 1000 VDCW; sim to RMC Type JF Discap.							
	C125	19A700005P9	Polyester: 0.022 uF ±10%, 50 VDCW.							
	C126	19A134202P6	Tantalum: 22 uF ±20%, 15 VDCW.							
	C127	19A116655P18	Ceramic disc: 680 pF ±10%, 1000 VDCW; sim to RMC Type JF Discap.							
l	C128	19A134202P5	Tantalum: 3.3 uF +20%, 15 VDCW.							
	C129	19A116655P20	Ceramic disc: 1000 pF ±10%, 1000 VDCW; sim to RMC Type JF Discap.							
	C130*	19B209723P1	Tantalum: 0.47 uF ±10%, 35 VDCW. In REV B & earlier:							
		19A134202P112	Tantalum: 0.47 uF ±10%, 35 VDCW.							
	C131	19A134202P112	Tantalum: 22 uF ±20%, 15 VDCW.							
	C132	19A700015P37	Teflon/Mica: 220 pF ±5%, 250 VDCW.							
	C133	19A700015P45	Silver mica: 470 pF ±5%, 250 VDCW.							
	C134	19A700005P7	Polyester: 0.01 uF ±10%, 50 VDCW.							
2	C135	19A116655P18	Ceramic disc: 680 pF ±10%, 1000 VDCW; sim to RMC Type JF Discap.							
	C136 and C137	19A116192P1	Ceramic: 0.01 uF ±20%, 50 VDCW; sim to Erie 8121 Special.							
	C138	7489162P39	Silver mica: 330 pF ±5%, 500 VDCW; sim to Sprague Type 118.							
	C139	7489162P113	Silver mica: 27 pF ±10%, 500 VDCW; sim to Sprague Type 118.							
	C140	19A700105P46	Mica: 270 pF ±5%, 500 VDCW.							
	C141	19A134202P6	Tantalum: 22 uF ±20%, 15 VDCW.							
	C142	19A700105P16	Mica: 20 pF ±5%, 500 VDCW.							
	C143	19A116655P19	Ceramic disc: 1000 pF ±20%, 1000 VDCW; sim to RMC Type JF Discap.							
	C144	19A700105P46	Mica: 270 pF ±5%, 500 VDCW.							



*COMPONENTS ADDED, DELETED OR CHANGED BY PRODUCTION CHANGES.

SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION
				19A700024P13	Coil, RF: 1.0 uH +10%.	R119	3R152P112J	Composition: 1.1K ohms +5%, 1/4 w.	R162	3R152P203J	Composition: 20K ohms ±5%, 1/4 w.	C104	T644ACP347J	Polyester: 0.047 uF <u>+</u> 5%, 50 VDCW.	C103L	19A116656P15J1	Ceramic disc: 15 pF ±5%, 500 VDCW, temp coef -150 PPM.
C145*	19A116192P1	Ceramic: 0.01 uF ±20%, 50 VDCW; sim to Erie 8121 Special.	L102	l .	<u>-</u>	R120	19A701250P283	Metal film: 7.15K ohms +1%, 250 VDCW, 1/4 w.	R163	19A700106P61	Composition: 820 ohms ±5%, 1/4 w.	C105	T644ACP333J	Polyester: 0.033 uF ±5%, 50 VDCW.	C104	19A116656P3J1	Ceramic disc: 3 pF +5%, 500 VDCW, temp coef
		In REV G & earlier:	L103	19A130997P1 19A130996P1	Coil.	R121*	19A701250P201	Metal film: 1K ohms +1%, 1/4 w.	R164	3R152P622J	Composition: 6200 ohms ±5%, 1/4 w.	C106	5491674P28	Tantalum: 1 uF <u>+</u> 20%, 25 VDCW; sim to Sprague Type 162D.	C104	1341100301001	-150 PPM.
	19A116080P1	Polyester: 0.01 uF <u>+</u> 20%, 50 VDCW.	L104	19A130997P1	Coil.	11121	1011/012001201	In REV E & earlier:	R165*	19A701250P161	Metal film: 422 ohms ±1%, 1/4 w.	C107	5496267P9	Tantalum: 3.3 uF ±20%, 15 VDCW; sim to Sprague	C105H	19A700105P27	Mica: 51 pF ±5%, 500 VDCW.
C146	19A700005P7	Polyester: 0.01 uF <u>+</u> 10%, 50 VDCW.	L105	19B209420P1	Coil, RF: .10 uH +5%, .08 ohms DC res max; sim		19C314256P21151	Metal film: 1150 ohms +1%, 1/4 w.			In REV D & earlier:	C107	348020113	Type 150D.	C105L	19A700105P28	Mica: 56 pF ±5%, 500 VDCW.
C147	19A116655P14	Ceramic disc: 470 pF ±10%, 1000 VDCW; sim to RMC	LIOO	13820342011	to Jeffers 4416-6J.	R122	3R152P111J	Composition: 110 ohms ±5%, 1/4 w.		3R152P511J	Composition: 510 ohms ±5%, 1/4 w.	C108	T644ACP268J	Polyester: .0068 uF ±5%, 50 VDCW.	C106	19A116655P18	Ceramic disc: 680 pF ±10%, 1000 VDCW; sim to RMC Type JF Discap.
g1 10#	19A700105P8	Type JF Discap. Mica: 12 pF +5%, 500 VDCW.	L108	19A700024P13	Coil, RF: 1.0 uH ±10%.	R123	3R152P360J	Composition: 36 ohms ±5%, 1/4 w.	R166	3R152P511J	Composition: 510 ohms $\pm 5\%$, $1/4$ w.	C109	19A143481P20	Ceramic: 1000 pF ±10%, 1000 VDCW.	C107H	19A116656P9J1	Ceramic disc: 9 pF ±0.5 pF, 500 VDCW, temp coef
C148*	194700105P8	In REV G & earlier:	L109* thru	19A143019P1	Coil. Added by REV H.	R124	3R152P111J	Composition: 110 ohms ±5%, 1/4 w.	R167	19A700106P67	Composition: 1.5K ohms ±5%, 1/4 w.	C110	5491674P36	Tantalum: 3.3 uF ±20%, 10 VDCW; sim to Sprague Type 162D.			-150 PPM. Ceramic disc: 10 pF ±5%, 500 VDCW; temp coef
1	7489162P31	Silver mica: 150 pF +5%, 500 VDCW; sim to	L111*			R125	19A701250P189	Metal film: 825 ohms <u>+</u> 1%, 250 VDCW, 1/4 w.	R168	H212CRP122C	Composition: 220 ohms ±5%, 1/4 w.	C111	T644ACP368J	Polyester: 0.068 uF ±5%, 50 VDCW.	C107L	19A116656P10J1	-150 PPM.
	7403102731	Electro Motive Type DM-15.				R126*	3R152P112J	Composition: 1.1K ohms ±5%, 1/4 w.	R169	3R152P361J	Composition: 360 ohms ±5%, 1/4 w.	C112*	19A143491P6J0	Ceramic: 6 pF ±5%, temp coef 0 PPM. Added by			INDUCTORS
C149	19A700105P38	Mica: 150 pF ±5%, 500 VDCW.	P902		Connector. Includes:	. 1		In REV C & earlier:	R170	19A700106P39	Composition: 100 ohms ±5%, 1/4 w.			REV B.	L101	19A700024P17	Coil, RF: 2.2 uH +10%.
C150	19A700005P7	Polyester: 0.01 uF ±10%, 50 VDCW.		19B219594P2	Contact, electrical: 8 pins.		3R152P102J	Composition: 1K ohms ±5%, 1/4 w.	R171*	19A116412P1	Variable, cermet: 200 ohms ±10%, 1/2 w; sim to Helipot Model 62 PR. Added by REV J.	C113	19A701534P9	Tantalum: 47 uF ±20%, 6.3 VDCW. Tantalum: 3.3 uF ±20%, 10 VDCW; sim to Sprague	L101	19A700024P17	Coil, RF: 1.0 uH +10%.
C151	19A116655P14	Ceramic disc: 470 pF ±10%, 1000 VDCW; sim to RMC Type JF Discap.		19B219594P3	Contact, electrical: 9 pins.	R127*	19A701250P182	Metal film: 698 ohms ±1%, 250 VDCW, 1/4 w.				C114	5491674P36	Type 162D.	L102H	19B209420P106	Coil, RF: .27 uH +10%, .16 ohms DC res max; sim
C152	19A700005P7	Polyester: 0.01 uF ±10%, 50 VDCW.						IN REV F & earlier:			THERMISTORS	C115	19A701534P8	Tantalum: 22 uF ±20%, 16 VDCW.	110011	155200120120	to Jeffers 4416-6K.
C153	5491674P28	Tantalum: 1 uF ±20%, 25 VDCW; sim to Sprague	Q101	19A700023P1	Silicon, NPN; sim to Type 2N3904.		19C314256P22001	Metal film: 2000 ohms ±1%, 1/4 w.	RT101	5490828P54	Thermistor: 50 ohms ±10%, color code blue; sim to Carborundum Type B0807J-16.	•		DIODES AND RECTIFIERS	L103L	19B209420P107	Coil, RF: .33 uH $\pm 10\%$, .22 ohms DC res max; sim to Jeffers $4416-7K$.
	10110100000	Type 162D.	Q102	19A700022P1	Silicon, PNP; sim to Type 2N3906.	R128	19A701250P261	Metal film: 4.22K ohms <u>+</u> 1%, 1/4 w.	RT102	5490828P55	Thermistor: 2200 ohms ±5%, color code yellow; sim to Carborundum Type 0325-F5-144.	CR101	19A115250P1	Silicon, fast recovery, 225 mA, 50 PIV.			
C154	19A134202P6 19A700005P7	Tantalum: 22 uF ±20%, 15 VDCW. Polyester: 0.01 uF +10%, 50 VDCW.	Q103*	19A115779P1	Silicon, PNP; sim to Type 2N3251.	R129	19A700106P71	Composition: 2.2K ohms ±5%, 1/4 w			Sim to Carborandam Type 0020-10-144.	and CR102					
C155 thru C157	1941000014	Totaleger. Great drtow, go vacus.			In REV C & earlier:	R130	3R152P511J	Composition: 510 ohms ±5%, 1/4 w.						PLUGS	P103	19A116659P6	Connector, printed wiring: 6 contacts rated € 5 amps; sim to Molex 09-52-3061.
C157	19A134202P14	Tantalum: 1 uF +20%, 35 VDCW.		19A115852P1	Silicon, PNP; sim to Type 2N3906.	R131	19A700106P69	Composition: 1.8K ohms ±5%, 1/4 w.	T101	19A130998G1	Coil.	P102	19A116659P76	Connector, printed wiring: 9 contacts rated at			MISCELLANEOUS
C159	19A116655P19	Ceramic disc: 1000 pF +20%, 1000 VDCW; sim to	0104 and	19A700023P1	Silicon, NPN; sim to Type 2N3904.	R132	3R152P300J 19A701250P337	Composition: 30 ohms ±5%, 1/4 w. Metal film: 23.7K ohms +1%, 1/4 w.			TEST POINTS			5 amps; sim to Molex 09-52-3091.		19A701332P1	Insulator disk. (Used with Q103, Q107, Q108,
		RMC Type JF Discap.	Q105	1015000001	Silicon, PNP; sim to Type 2N3906.	R133 R134	3R152P200J	Composition: 20 ohms ±5%, 1/4 w.	TP101	19B211379P1	Spring (Test Point).			RESISTORS		19A701332P1	Q110, Q111).
C160	19A700005P7	Polyester: 0.01 uF ±10%, 50 VDCW.	Q106 Q107	19A700022P1 19A134402P1	N Type, field effect.	R134	19A701250P25	Metal film: 17.8 ohms +1%, 250 VDCW, 1/4 w.				R101	19A134231P223J	Deposited carbon: 22K ohms ±5%, 1/8 w.		19AA701332P4	Insulator, washer: nylon. (Used with Q112, Q113, Q115, Q116).
C161	19A700005P3	Polyester: .0022 uF ±10%, 50 VDCW.	and Q108	19413440221	N Type, field effect.	R136	3R152P511J	Composition: 510 ohms ±5%, 1/4 w.				R102	19A700106P95	Composition: 22K ohms ±5%, 1/4 w.		19B227717P1	Support. (Used with L101).
C162	19A134202P14	Tantalum: 1 uF ±20%, 35 VDCW.	Q109	19A700023P1	Silicon, NPN; sim to Type 2N3904.	R137	3R152P161J	Composition: 160 ohms ±5%, 1/4 w.	U101	19A116787P2	Linear Phase Detector.	R103*	19A700106P55	Composition: 470 ohms ±5%, 1/4 w.		19C327531G1	Shield. (Located in corner of Phase Lock Loop
C163 thru C166	19A116655P19	Ceramic disc: 1000 pF ±20%, 1000 VDCW; sim to RMC Type JF Discap.	Q110	19A702613P1	Silicon, NPN.	and R138			U102	19A134213P1	Digital Frequency Divider.			In REV A & earlier:			Exciter Board).
C166	19A700005P8	Polyester: 0.015 uF +10%, 50 VDCW.	Q111	19A116201P1	Silicon, NPN.	R139*	3R152P240J	Composition: 24 ohms ±5%, 1/4 w. Deleted by			VOLTAGE REGULATORS		3R152P681J	Composition: 680 ohms ±5%, 1/4 w.		19C327531G2	Shield. (Located in center of Phase Lock Loop Exciter Board).
C168	19A116655P14	Ceramic disc: 470 pF +10%, 1000 VDCW; sim to RMC	Q112	19A116868P1	Silicon, NPN; sim to Type 2N4427.			REV H.	VR101	4036887P4	Zener: 500 mW, 4.4 v. nominal.	R104	19A701250P369	Metal film: 51.1K ohms ±1%, 1/4 w.			!
0100	10,110000111	Type JF Discap.	Q113	19A115562P2	Silicon, PNP; sim to Type 2N2904A.	R140	3R152P132J	Composition: 1.3K ohms ±5%, 1/4 w. Composition: 300 ohms ±5%, 1/4 w.			SOCKETS	R105	19A701250P303	Metal film: 10.5K ohms ±1%, 1/4 w.		1	
C169	19A134202P14	Tantalum: 1 uF ±20%, 35 VDCW.	Q114	19A700023P1	Silicon, NPN; sim to Type 2N3904.	R141 R142	3R152P301J 19A700106P23	Composition: 22 ohms ±5%, 1/4 w.	XY101	19A701785P1	Contact, electrical; sim to Molex 08-50-0404.	R106	19A701250P311	Metal film: 12.7K ohms ±1%, 1/4 w. Metal film: 10.5K ohms ±1%, 1/4 w.			
C170	19A700005P7	Polyester: 0.01 uF ±10%, 50 VDCW.	Q115	19A115300P2	Silicon, NPN; sim to Type 2N3053.	R142	19A700106P47	Composition: 220 ohms ±5%, 1/4 w.	thru XY108		(Quantity 8 each).	R107	19A701250P303 19A701250P269	Metal film: 10.5K Ohms ±1%, 1/4 w. Metal film: 5.11K ohms +1%, 1/4 w.			
C171	7489162P13	Silver mica: 27 pF ±5%, 500 VDCW; sim to Sprague Type 118.	Q116	19A115562P2	Silicon, PNP; sim to Type 2N2904A.	R144*	19A700113P7	Composition: 4.7 ohms ±5%, 1/2 w.			ACCOCYAMED ACCEMBLIES	R108 R109	3R152P132J	Composition: 1.3K ohms ±5%, 1/4 w.			
C172*	19A116114P24	Ceramic: 7 pF ±5%, 100 VDCW, temp coef 0 PPM.	Q117* and	19A116774P1	Silicon, NPN; sim to Type 2N5210.			In REV A:			ASSOCIATED ASSEMBLIES	R110	19A701250P269	Metal film: 5.11K ohms ±1%, 1/4 w.			
21504	104110114700	Added by REV H. Ceramic: 6 pF ±5%, 100 VDCW; temp coef 0 PPM.	Q118*		In REV H & earlier:		7147161P39	Composition: 6.8 ohms ±5%, 1/2 w.				R111	19A700106P91	Composition: 15K ohms ±5%, 1/4 w.			
C173*	19A116114P20	Added by REV H.		19A115910P1	Silicon, NPN; sim to Type 2N3904.			Earlier than REV A:			NOTE: When reordering specify FM ICOM Frequency.	R112*	19A701250P339	Metal film: 24.9K ohms ±1%, 1/4 w.			
C174*	19A700219P24	Ceramic: 8.2 pF +5%, 100 VDCW, temp coef 0 PPM. Added by REV H.					7147161P42	Composition: 8.2 ohms ±5%, 1/2 w.			FM ICOM = Operating Frequency 12			Earlier than REV A:			
C175	19A700003P7	Tantalum: 10 uF ±20%, 16 VDCW.	R101	3R152P621J	Composition: 620 ohms ±5%, 1/4 w.	R145	19A700106P53	Composition: 390 ohms ±5%, 1/4 w.	Y101	19A130605G14	Externally Compensated: 5 PPM, 138-155 MHz.		19C314256P22472	Metal film: 24.7K ohms ±1%, 1/4 w.	<u> </u>		
			R102	19A700106P63	Composition: 1K ohms ±5%, 1/4 w.	R146	19A701250P275	Metal film: 5.9K ohms ±1%, 1/4 w.	thru Y108	19A130605G15	Externally Compensated: 5 PPM, 150.8-174 MHz.	R113	19A701250P307	Metal film: 11.5K ohms ±1%, 1/4 w.			
	1	DIODES AND RECTIFIERS	R103	19B209358P105	Variable, carbon film: approx 200 to 5K ohms ±10%, 1/4 w; sim to CTS Type X-201.	R147 and	19A700106P36	Composition: 75 ohms $\pm 5\%$, 1/4 w.	Y101	19A130605G1	Internally Compensated: 2 PPM, 138-155 MHz.	R114	19A701250P347	Metal film: 30.1K ohms $\pm 1\%$, 1/4 w.	<u> </u>		
CR102	19A700073P1	Silicon; sim to BB 409.	R104		210%, 1/1 W, Sim to Old Type if 2011	R148			thru Y108	19A130605G2	Internally Compensated: 2 PPM, 150.8-174 MHz.	R115	19A700106P73	Composition: 2.7K ohms $\pm 5\%$, $1/4$ w.			
CR104 thru CR108	19A115250P1	Silicon, fast recovery, 225 mA, 50 PIV.	R105	19A700106P101	Composition: 39K ohms ±5%, 1/4 w.	R149	19A700106P49	Composition: 270 ohms ±5%, 1/4 w	Y101	19A130605G8	STATION ONLY. Internally Compensated: 5 PPM, 138-155 MHz.			FILTERS			
CR109	162B3011P0002	Diode, optoelectronic: red; sim to Hew. Packard	R106	19A701250P260	Metal film: 4.22K ohms ±1%, 250 VDCW, 1/4 w.	R150	19A700106P75	Composition: 3.3K ohms ±5%, 1/4 w.	thru Y108	19A130605G9	STATION ONLY. Internally Compensated: 5 PPM, 150.8-174 MHz.	FL101		BANDPASS FILTER			
Chios	1028001110002	5082-4650.	R107	19A701250P169	Metal film: 511 ohms ±1%, 1/4 w.	R151	19A700106P15	Composition: 10 ohms ±5%, 1/4 w.	11					19B226748G1 138-155 MHz 19B226748G2 150.8-174 MHz		į	
		JACKS AND RECEPTACLES	R108	19A701250P327	Metal film: 18.7K ohms +1%, 250 VDCW, 1/4 w.	R152	3R152P511J 19A700106P57	Composition: 510 ohms ±5%, 1/4 w. Composition: 560 ohms +5%, 1/4 w.	A101		AUDIO PROCESSOR BOARD 19C321542G1						
J101	19A700049P2	Connector, receptacle: 500 VDCW maximum; sim to	R109 R110	19A701250P277 19A701250P69	Metal film: 6.19K ohms ±1%, 1/4 w. Metal film: 51.1 ohms ±1%, 1/4 w.	R153 R154	19A700106P37	Composition: 51 ohms ±5%, 1/4 w.			19C321542G2	g1017	19A116656P12J1	Ceramic disc: 12 pF ±5%, 500 VDCW; temp coef			!
100	10470170571	NTTF-1058.	R111	19A700106P63	Composition: 1K ohms ±5%, 1/4 w.	R155	19A700106P71	Composition: 2.2K ohms ±5%, 1/4 w.	AR101	19A116754P2	Linear, Dual 741C OP AMP; sim to MC1458SP1 High	C101H	19411003071231	-150 PPM.			
J102	19A701785P1	Contact, electrical; sim to Molex 08-50-0404. (Quantity 9).	R112	19A700106P32	Composition: 51 ohms ±5%, 1/4 w.	and R156		-			Slew Rate OP AMP. In REV A & earlier:	C101L	19A116656P15J1	Ceramic disc: 15 pF ±5%, 500 VDCW, temp coef -150 PPM.			
J103	19A701785P1	Contact, electrical; sim to Molex 08-50-0404. (Quantity 6).	R113	19A700106P67	Composition: 1.5K ohms ±5%, 1/4 w.	R157	19A700106P87	Composition: 10K ohms ±5%, 1/4 w.		19A116754P1	Linear: Dual In-Line 8-Pin Minidip package; sim	C102H	19A116656P15J1	Ceramic disc: 15 pF ±5%, 500 VDCW, temp coef	l i		
			thru R115			R158	3R152P511J	Composition: 510 ohms ±5%, 1/4 w.	1 1	19811075471	to T1, SN72558 NSC.			-150 PPM.			
			R116	19A700106P36	Composition: 75 ohms ±5%, 1/4 w.	R159	19A116310P35	Composition: 10 ohms ±5%, 1/4 w; sim to			CAPACITORS	C102L	19A116656P18J1	Ceramic disc: 18 pF ±5%, 500 VDCW, temp coef -150 PPM.			
L101	19B209595P502	Coil, RF: variable; sim to Paul Smith 02-19-75-AE-3. Includes:	R117	19A700106P32	Composition: 51 ohms ±5%, 1/4 w.	R160	3R152P361J	Allen-Bradley Type CB. Composition: 360 ohms ±5%, 1/4 w.	C101	T644ACP333J	Polyester: 0.033 uF ±5%, 50 VDCW.	С103Н	19A116656P12J1	Ceramic disc: 12 pF ±5%, 500 VDCW; temp coef -150 PPM.			+
	19B209631P6	Aluminum core: No. thd. size 6-32. (148-174 Mhz)	R118	19A700106P63	Composition: 1K ohms ±5%, 1/4 w.	R160	19A700106P15	Composition: 10 ohms ±5%, 1/4 w.	C102	5491674P36	Tantalum: 3.3 uF ±20%, 10 VDCW; sim to Sprague			LOU FEM.			
	19B209631P5	Ferrite core: No. thd. size 6-32. (138-155 MHz)							and C103		Type 162D.						
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PRODUCTION CHANGES

Changes in the equipment to improve performance or to simplify circuits are identified by a "Revision Letter," which is stamped after the model number of the unit. The revision stamped on the unit includes all previous revisions. Refer to the Parts List for descriptions of parts affected by these revisions.

REV. A - Audio Processor 19C321542G1

To standardize components. Changed R112.

REV. B - To improve audio response. Changed AR101 and R103. Added C112.

REV. C - To improve performance. Changed AR101 and R103.

REV. A - Exciter Board 19D423249G1

To increase exciter output power. Changed R144.

REV. B - To increase exciter output power. Changed R144.

REV. C - No units built. Superseded by Revision D.

REV. D - To improve operation. Changed R126 and Q103.

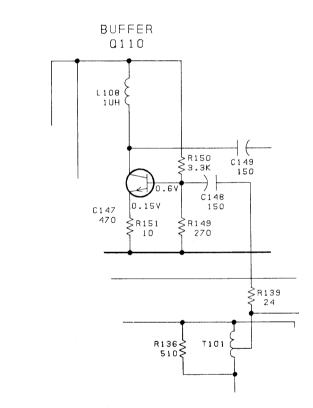
REV. E - To improve operation of lock detector indicator. Change R165.

REV. F - To improve operation of lock detector circuit. Changed R121.

REV. G - To shift voltage output range of differential error voltage amplifier to improve VCO lock on extremes of frequency split. Changed R127.

REV. H - To reduce level of conducted spurs. Added C172, C173, C174, L109, L110 and L111. Changed C148 and C145. Deleted R139.

OLD SCHEMATIC WAS:



REV. J - To improve detect sensitivity in cold environment. Changed Q117 and Q118. Added R171.

REV. K - To improve lock detector range and performance in a cold environment. Changed R125, R127 and R128.
R125 was: 19A700106P9 - Composition: 680 ohms ±5%, 1/4 W.
R127 was: 19C314256P21821 - Metal film: 1.8K ohms ±1%, 1/4 W.
in REV. F & earlier: 19C314256P22001 - Metal film: 2K ohms ±1%, 1/4W.
R128 was: 19C314256P21102 - Metal film: 11K ohms ±1%, 1/4 W.

REV. A - Exciter Board 19D423249G2

Incorporated into intial shipment.

REV.B- 138-174 MHZ PLL EXCITER BOARD 19D423249G2 REV.L- 138-174 MHZ PLL EXCITER BOARD 19D423249G1

To reduce conducted spurious and improve operation. Changed C174 to 8.2pF. Old part number for C174 was: 19A116114P20 - Ceramic: 6 pF $\pm 5\%$, 100 VDCW; temp coef 0 PPM. Added by REV H.

REV D - EXCITER BOARD 19D423249G1 REV N - EXCITER BOARD 19D423249G2 To allow Lock Detector LED to extinguish when exciter is unkeyed, changed R165.

REV A - <u>AUDIO PROCESSOR BOARD 19C321542G2</u>

To improve low frequency response on Channel Guard Input, changed C113.

Cll3 was: 19A701534P7 Tantalum: 10 uF + 20%, 16 VDCW.