

MAINTENANCE MANUAL

806—825 MHz CUSTOM MVP EXCITER BOARD 19D424793GI AND OSCILLATOR BOARD 19C327782GI

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DESCRIPTION

The exciter is a crystal controlled, frequency modulated exciter designed for one through four frequency operation in the 806-825 MHz frequency band. Both integrated circuits and discreet components are used to provide a nominal 65 milliwatts of RF Power to the PA assembly or 15 milliwatts to the receiver. In the receive mode the exciter provides the injection frequency for the local oscillator input to the 1st IF mixer stage.

The exciter includes the audio processor, oscillator board(s) with up to four ICOMs and 3 frequency multipliers. The FM ICOMs plug into the oscillator board which, in turn, plugs into the exciter.

The operating frequency is selected by the position of the channel selector switch on the control unit and is determined by the FM ICOM associated with the selected channel. The crystal frequencies range from approximately 16.7 to 17.2 MHz and are multiplied 48 times to generate the RF carrier frequency. Oscillator stability is maintained within ±0.0002% by individual temperature compensating circuits in each ICOM.

Audio, power supply voltage, and control functions are connected from the SAS board to the exciter through P902/J902.

Centralized metering jack J103 is provided for use with GE Test Set Model 4EX3A11 or Test Kit 4EX8K12. The Test Set meters all multiplier stages and the relative receiver L.O. RF output power.

CIRCUIT ANALYSIS

References to symbol numbers mentioned in the text are found on the schematic diagram, outline diagram and parts list.

OSCILLATOR BOARD

Depending on the number of operating frequencies, either one or two Oscillator boards may be present. Each Oscillator board contains space for two FM ICOMs and plugs into J104 on the exciter. When two Oscillator Boards are required, they are mounted piggy back fashion - one atop the other - and are plugged into J104 on the exciter. ICOMs for Channels 1 and 2 plug into the lower Oscillator Board. ICOMs for Channels 3 and 4 plug into the upper Oscillator Board.

In single frequency applications one Oscillator Board, equipped with one FM ICOM, is supplied. A DA jumper connected between H1 and H2 connects A- to the frequency select lead at XY2601-8. Since the exciter output is used as the 1st IF injection frequency for the receiver, the oscillator associated with the selected operating frequency is always operating.

In multi-frequency radios the DA jumper is removed. Frequency selection is then controlled by the FREQUENCY selector switch with A- being applied from the switch to the appropriate frequency select lead through J2601.

A voltage divider consisting of R2601 and R2602 applies approximately 6.2 Volts to pin 6 of the FM ICOM to operate the crystal. L2601 and C2605 provide additional filtering of the +10 Volt line.

The output of the Oscillator Board is applied to a tuned circuit consisting of T101, C113 and C114 on the exciter board. The 4th harmonic is selected and applied to FET Amplifier Q102.

FM ICOMs (Frequency Modulated)

Each ICOM is enclosed in an RF shielded can with the type ICOM 92C-FM ICOM) printed

on the top of the can. These FM ICOMs are not interchangeable with other type ICOMs. Each 2C-FM ICOM contains a crystal controlled Colpitts oscillator and a 2 PPM (±0.0002%) compensator IC.

Frequency selection is accomplished by switching the ICOM keying lead (terminal 8) to A- by means of the channel selector switch on the control unit. In single-frequency radios, a jumper from H1 to H2 on the Oscillator Board permanently connects terminal 8 of the F1 FM ICOM to A-. The selected oscillator is on all the time.

The audio output from the audio processor is applied to the FM ICOMs through J104-5 and modulates the crystal frequency. A tuned circuit, consisting of T101, C113 and C114, on the exciter board selects the 4th harmonic of the crystal frequency (approximately 67.16 MHz to 68.75 MHz) and applies the harmonic frequency to FET amplifier Q102 on the exciter board through J104-2.

-CAUTION-

All ICOMs are individually compensated at the factory and cannot be repaired in the field. Any attempt to repair or change the ICOM frequency will void the warranty.

The 2C-FM ICOMs are individually temperature compensated and will maintain 2 PPM frequency stability from -30°C to +60°C (-22°F to 140°F).

Oscillator Circuit

Quartz crystals used in ICOMs exhibit the traditional "S" curve characteristic of output frequency versus operating temperature.

At both the coldest and hottest temperatures, the frequency increases with increasing temperature. In the middle temperature range (approximately 0°C to 55°C), frequency decreases with increasing temperature.

Since the rate of change is nearly linear over the mid-temperature range, the output frequency change can be compensated for by choosing a parallel compensation capacitor with a temperature coefficient approximately equal to and opposite that of the crystal.

Figure 1 shows the typical performance of an uncompensated crystal as well as the typical performance of a crystal that has been matched with a properly chosen compensation capacitor.

At temperatures above and below the mid-range, additional compensation must be introduced. An externally generated compensation voltage is applied to a varactor

(voltage-variable capacitor) connected in parallel with the crystal. Refer to Figure 2 for a simplified diagram of the FM ICOM.

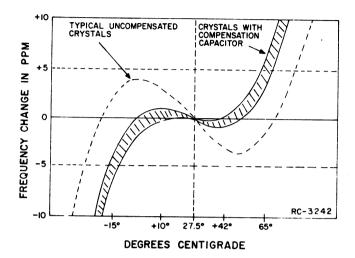


Figure 1 - Typical Crystal Characteristics

Modulation is accomplished with a hyperabrupt varicap connected in series with the crystal feedback capacitors. The varicap impedance is the dominant impedance in the loop. This allows large swings of load capacity with modulation, therefore, large frequency shifts are achieved for the modulated input. Biasing for the modulation varicap is provided by a voltage divider, R2601 and R2602 connected across the 10 volt regulator input on the Oscillator Board. A bias voltage of 6.2 volts is applied to pin 6 of all ICOMs.

Compensator Circuits

The 2C-FM ICOMs are temperature compensated at both ends of the temperature range to provide instant frequency compensation.

The cold end compensation circuit does not operate at temperatures above $0^{\circ}C$. When the temperature drops below $0^{\circ}C$, the circuit is activated. As the temperature decreases, the equivalent resistance decreases and the compensation voltage increases.

An increase in compensation voltage decreases the capacitance of the varactor in the oscillator, thereby compensating for the cold crystal characteristics and maintains a constant output frequency from the ICOM.

The hot end compensation circuit does not operate at temperatures below +55°C. When the temperature rises above +55°C, the circuit is activated. As the temperature increases, the equivalent resistance decreases and the compensation voltage decreses. The decrease in compensation voltage increases the capacity of the varactor, compensating

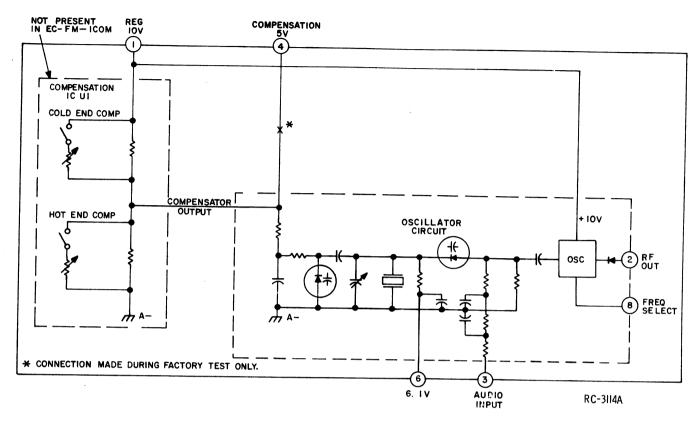


Figure 2 - Equivalent FM-ICOM Circuit

for the hot crystal characteristics and maintains a constant output frequency from the ICOM.

-SERVICE NOTE-

Proper ICOM operation is dependent on the closely-controlled input voltages for the 10-Volt regulator. Should all of the ICOMs shift off frequency, check the 10-Volt regulator module.

AUDIO PROCESSOR A101

The transmitter audio processor contains audio circuitry consisting of two operational amplifiers, AR101-A and -B, a pre-emphasis circuit with amplitude limiting and a post limiter filter. A total gain of approximately 24 dB is realized through the audio processor. Twenty dB is provided by AR101-B and 4 dB by AR101-A.

The 10-Volt regulator supplies power to the audio processor and applies regulated +10 V through XA101-6 to a voltage divider consisting of R108 and R110 in the audio processor. The +5 V output from the voltage divider establishes the operating reference point for both operational amplifiers. C107 provides decoupling to remove any noise transients from the 10-Volt regulator output.

Resistors R105, R106, and R107 and diodes CR101 and CR102 provide limiting for AR101-B. Diodes CR101 and CR102 are reverse biased by +5 VDC on AR101B-6 and voltage divider network R105, R106 and R107. The voltage divider network provides +7 VDC at the cathode of CR101 and +3 VDC at the anode of CR102. C102 and C103 permit a DC level change between AR101B-7 and the voltage divider network for diode biasing.

When the input signal to AR101B-1 is of a magnitude such that the amplifier output at AR101B-7 does not exceed 4 volts PP, the amplifier provides a nominal 20 dB gain. When the audio signal level at AR101B-7 exceeds 4 volts PP, diodes CR101 and CR102 conduct on the positive and negative half cycles providing 100% negative feedback to reduce the amplifier gain to 1. This limits the audio amplitude at AR101B-7 to 5 volts PP.

Resistors R102, R103 and R104 and C104 comprise the audio pre-emphasis network that enhances the signal to noise ratio. R104 and C104 control the pre-emphasis curve below limiting. R103 and C104 control the cut-off point for high frequency pre-emphasis. As high frequencies are attenuated, the gain of AR101 is increased.

Audio from the microphone is applied

to the audio processor at XA101-1 and coupled to the input of operational amplifier AR101-B through R101 and C101.

The amplified output of ARlO1-B is coupled through XAlO1-4 audio MOD ADJ control RlO3, XAlO1-3, ClO6, Rl12 and Rl13 to a second operational amplifier ARlO1-A. Audio MOD ADJ control is set for a deviation of 4.5 kHz.

The Channel Guard tone input is applied to the audio processor through J902-9 and a filter consisting of R101 and C104 and then through CG MOD ADJ R104 to A101-5. The CG tone is then coupled through C105 and R111 to AR101A-2 where it is combined with the microphone audio. AR101-A provides a signal gain of approximately 4 dB.

A post limiter filter consisting of AR101A, R112-R114, C108 and C109 provides 12 dB per octave roll off. R109 and C111 provide an additional 6 dB per octave roll off for a total of 18 dB.

---SERVICE NOTE---

R112-R114 are 1% resistors. This tolerance must be maintained to assure proper operation of the post limiter filter. Use exact replacements.

The output of the post limiter filter is coupled through C110 and XA101-9 to temperature compensating network RT101 and R107 to the input of the oscillator board at J104-5 on the exciter board.

FREQUENCY MULTIPLIERS

The fourth harmonic of the crystal frequency is applied to gate 1 of input of FET amplifier Q102 from the oscillator module through J104-2 and a tuned circuit consisting of T101, C113 and C114. Voltage for Q102 is supplied by the 10-volt regulator through J902-8. Q102 is metered through R116 with test set on position B.

The output of Q102 is coupled through tuned circuits T102, T103 and C124 to the base of first doubler Q103. T102 and T103 are tuned to four times the crystal frequency. Collector voltage for Q103 is supplied through collector feed network L102, R123, C130 and R124. Q103 is metered through R122 with test set on position D.

The output of first doubler Q103 is coupled through tuned circuits T104, T105 and C134 to the base of second doubler Q104. T104 and T105 are tuned to eight times the crystal frequency. Collector voltage for Q104 is supplied through collector feed network L103 and R126. Q104 is metered through R126 with test set on position F.

The output of second doubler Q104 is

coupled to the base of tripler Q105 through impedance matching circuitry and a double tuned circuit tuned to the 16th harmonic of the crystal frequency (267.2-275.2 MHz). These circuits also contribute to the rejection of spurious and harmonic output and consist of L103-L105, C141 and C143-C146.

Cl41 and Ll04 form a high pass filter that matches the collector impedance of Q104 to the impedance of the first tuned circuit consisting of Ll04 and Cl43. Coupling capacitor C145 couples the signal to the second tuned circuit consisting of L105 and C146. The signal from the second tuned circuit is applied to the base of tripler Q105 through a second high pass filter consisting of L105 and C147. L105 and C147 match the impedance of the second tuned circuit to the input impedance of Q105. Bias for Q105 is supplied from the 10-Volt line through a biasing network consisting of R129, C160 and CR103. C160 provides decoupling. CR103 establishes the quiescent biasing level of Q105 at approximately 0.6 VDC through R131. The emitter current of Q105 is metered through R232 with the test set in position G.

-SERVICE NOTE-

The values of the coupling capacitors and certain decoupling capacitors are critical to proper equipment operation. When replacing these components, be sure to use exact value replacement parts. The following capacitors are especially critical: C124, C134, C130, C131, C136, C139, C141, C145, C147 and C152.

The output of tripler Q107 is coupled to the antenna through iris coupled, double tuned helical resonators, Z101 and Z102, relay K101, and output jack J101 when transmitting or to output jack J102 when receiving. Z101 and Z102 are tuned to the operating frequency. Collector voltage for Q107 is supplied through L107, R134 and Z101 pins 1 & 3.

Relative power output of the exciter is metered through a metering network consisting of CR102, R138, R139, C161 and C162 and is metered on position A of the test set. Relative power out (position A) is metered only in the receive mode.

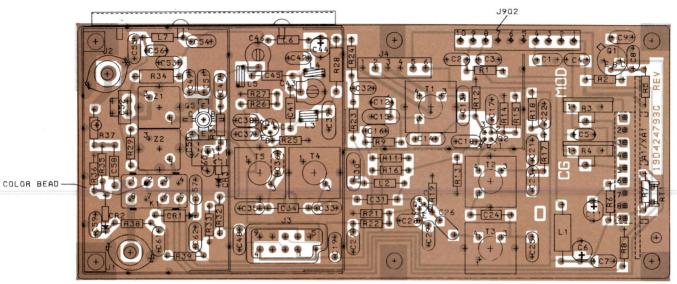
OUTPUT CONTROL RELAY

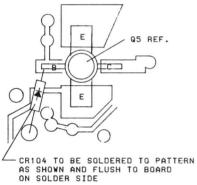
The output control relay steers the exciter output to the PA in the transmit mode and to the receiver first mixer when in the receive mode. This circuit consists of relay control transistor Q101 and output control relay K101.

When operating in the receive mode, Q101 is turned off and relay K101 is

de-energized. The exciter output is applied to the receiver first mixer as the local oscillator input through closed relay contacts 1 and 3, C158, R137 and J102. Closed relay contacts 5 and 7 short the audio input circuit of the oscillator board to ground (A-) in the receive mode. This prevents modulation of the FM ICOM and quietens the LO injection signal to the 1st mixer.

When operating in the transmit mode, +10 V is applied to the base of Q101 through J902-1 and R102, turning Q101 on. Q101 energizes K101 which removes the audio short from the audio input to the oscillator board, restoring modulation capability to the FM ICOM. Closed contacts 3 and 8 of K101 apply the exciter output directly to the PA assembly through J101.

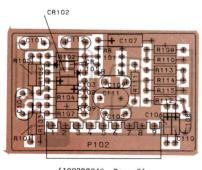




PARTIAL REFERENCE DESIGNATIONS ARE SHOWN.
FOR COMPLETE DESIGNATIONS, PREFIX WITH
100 SERIES.
EXAMPLE: C1-C101, R1-R101, ETC. EXCEPT P902.

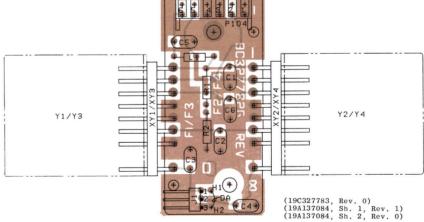
(19D424795, Rev. 1) (19B227982, Sh. 1, Rev. 0) (19B227982, Sh. 2, Rev. 0)

AUDIO PROCESSER



(19C327048, Rev. 2) (19A130538, Sh. 1, Rev. 1) (19A130538, Sh. 2, Rev. 1)

OSCILLATOR BOARD



PARTIAL REFERENCE DESIGNATION ARE SHOWN. FOR COMPLETE DESIGNATIONS PREFIX WITH 2600 SERIES EXAMPLE: C1-C2601, R1-R2601, ETC. EXCEPT P104.

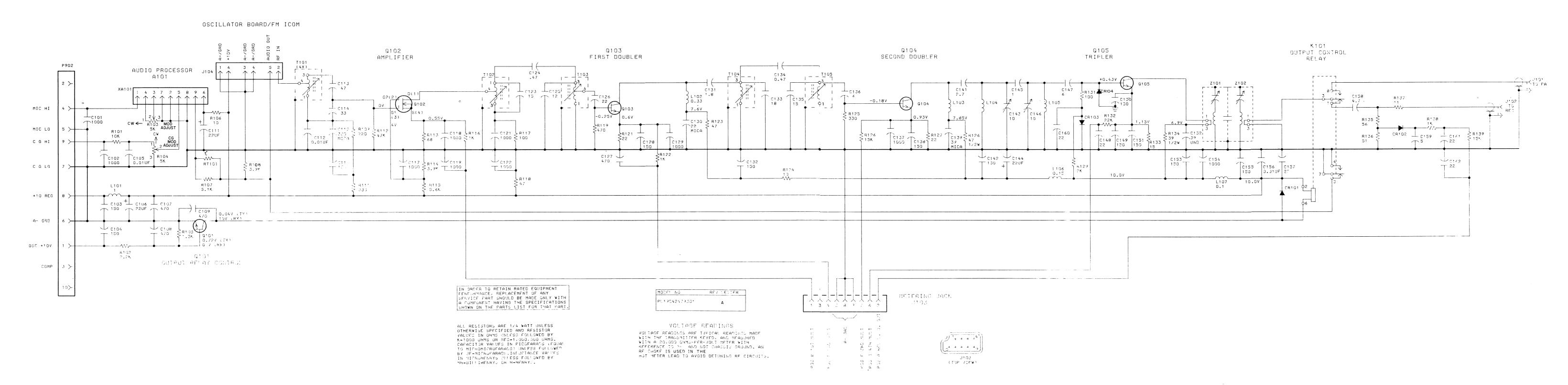
OUTLINE DIAGRAMS

806-825 MHz EXCITER

RUNS ON SOLDER SIDE

RUNS ON BOTH SIDES

RUNS ON COMPONENT SIDE



(19R622297, Rev. 4)

SCHEMATIC DIAGRAM

LBI30601

PARTS LIST

LBI30597A

806-825 MHz EXCITER BOARD 19D424793G1

SYMBOL

			0144
			C144 C145
SYMBOL	GE PART NO.	DESCRIPTION	C146
			C147
			C148
C101 and C102	19A116655P19	Ceramic disc: 1000 pf ±20½, 1000 VDCW; sim to RMC Type JF Discap.	C149 thru
C103 and C104	19A116655P7	Ceramic disc: 150 pf ±20%, 1000 VDCw; sim to RMC Type JF Discap.	C151 C152
C105	19A116080P1	Polyester: 0.01 µf ±20%, 50 VDCw.	C153
C106	19A134202P6	Tantalum: 22 μf ±20%, 15 VDCw.	C154
C107 thru C109	19A116655P13	Ceramic disc: 470 pf $\pm 20\%$, 1000 VDCw; sim to RMC Type JF Discap.	C155
C111	19A134202P6	Tantalum: 22 μf ±20%, 15 VDCW.	C156
C112	19A116080P1	Polyester: 0.01 μf ±20%, 50 VDCw.	C157
C113	19A116656P47J8	Ceramic disc: 47 pf ±5%, 500 VDCw, temp coef -80 PPM.	C158
C114	19A116656P33J8	Ceramic disc: 33 pf ±5%, 500 VDCw, temp coef -80 PPM.	C158
C115	7489162P39	Silver mica: 330 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.	C160 thru
C116	19A116655P7	Ceramic disc: 150 pf $\pm 20\%$, 1000 VDC+; sim to RMC Type JF Discap.	C162
C117 thru C119	19A116655P19	Ceramic disc: 1000 pf ±20%, 1000 VDCw; sim to RMC Type JF Discap.	CR101
C121 and	19A116655P19	Ceramic disc: 1000 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	CR102 CR103
C122 C123	19A116656P15J2	Ceramic disc: 15 pf ±5%, 500 VDCw, temp coef	CR104
G104	5401C01D12	-220 PPM. Phenolic: 0.47 pf ±10%, 500 VDCw.	
C124 C125	5491601P13 19A116656P12J2	Ceramic disc: 12 pf ±5%. 500 VDCw, temp coef	J101
C126	19Al16656P22J0	-220 PPM. Ceramic disc: 22 pf ±5%, 500 VDCW, temp coef 0 PPM.	and J102 J103
C127	19A116655P13	Ceramic disc: 470 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	J104
C128	19A116655P7	Ceramic disc: 150 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	J902
C129	19A116655P19	Ceramic disc: 1000 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	
C130	19A134666P3	Silver mica: 22 pf ±5%, 500 VDCw; sim to Electro Motive Type DM154CR.	K101
C131	5491601P124	Phenolic: 1.8 pf ±5%, 500 VDCW.	
C132	19A116655P7	Ceramic disc: 150 pf $\pm 20\%$, 1000 VDCW; sim to RMC Type JF Discap.	L101
C133	19A116656P18J8	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.	L102
C134	5491601P113	Phenolic: 0.47 pf ±5%, 500 VDCW.	L102
C135	19A116656P15J8	Ceramic disc: 15 pf ±5%, 500 VDCW, temp coef -80 PPM.	L103 L104
C136	19A116656P6J0	Ceramic disc: 6 pf ±0.5 pf, 500 VDCW, temp coef 0 PPM.	L105
C137	19A116655P19	Ceramic disc: 1000 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	L106
C138	19A116655P7	Ceramic disc: 150 pf $\pm 20\%$, 1000 VDCW; sim to RMC Type JF Discap.	L107
C139	7489162P17	Silver mica: 39 pf ±5%, 500 VDCw; sim to Electro Motive Type DM-15.	
C141	5491601P128	Phenolic: 2.7 pf ±5%, 500 VDCw.	Q101
			Q102
			Q103 and Q104
			Q105

)L	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION
	19A116655P7	Ceramic disc: 150 pf ±20%, 1000 VDCw; sim to RMC Type JF Discap.			RESISTORS			ASSOCIATED ASSEMBLIES			JACKS AND RECEPTACLES
	19B209544P2	Variable, air: 2.04 to 9.9 pf, 250 v; sim to E.F. Johnson Type T 187-0106-005.	R101	3R152P103J	Composition: 10K ohms ±5%, 1/4 w.	A101		AUDIO PROCESSOR 19C321542G1	J2602	19A134468P1	Contact, electrical: sim to AMP 87233-3.
	19A134202P6	Tantalum: 22 µf ±20%, 15 VDCW.	R102 R103	3R152P222J 19B209358P105	Composition: 2.2K ohms ±5%, 1/4 w. Variable, carbon film: approx 200 to 5K ohms						
	5491601P120	Phenolic: 1.0 pf ±5%, 500 VDCW.	and R104		$\pm 10\%$, 0.25 w; sim to CTS Type X-201.	AR101*	19A116754P2	Linear Amplifier. In REV A:	L2601	19B209420P117	Coil, RF: 2.20 µh ±10%, 0.38 ohms DC res max; sim to Jeffers 4436-4K.
	19B209544P2	Variable, air: 2.04 to 9.9 pf, 250 v; sim to E.F. Johnson Type T 187-0106-005.	R105	3R152P152J	Composition: 1.5K ohms ±5%, 1/4 w.	1	19A116754P1	Linear Amplifier.			P. 1950
	19A116656P6J0	Ceramic disc: 6 pf ±0.5 pf, 500 VDCw, temp coef 0 PPM.	R106 R107	3R152P100J 3R152P512J	Composition: 10 ohms ±5%, 1/4 w. Composition: 5.1K ohms ±5%, 1/4 w.	1			P104	19A116659P4	Connector, printed wiring: 6 contacts; sim to
	19A116656P22J0	Ceramic disc: 22 pf ±5%, 500 VDCw, temp coef	R108	3R152P392J	Composition: 3.9K ohms ±5%, 1/4 w.	C101	19A116080P204	Polyester: 0.033 µf ±5%, 50 VDCW.		İ	Molex 09-52-3062.
	19A116655P7	0 PPM. Ceramic disc: 150 pf ±20%, 1000 VDCw; sim to	R109	3R152P221J	Composition: 220 ohms ±5%, 1/4 w.	C102	5491674P36	Tantalum: 3.3 µf ±20%, 10 VDCw; sim to Sprague Type 162D.			RESISTORS
		RMC T pe JF Discap.	R111	3R152P331J	Composition: 330 ohms ±5%, 1/4 w.	C103			R2601	19C314256P23831	Metal film: 3.83K ohms ±1%, 1/4 w.
	19Al16679P39J	Metallized teflon: 39 pf $\pm 5\%$, 250 VDCW.	R112 R113	3R152P473J 3R152P680J	Composition: 47K ohms ±5%, 1/4 w. Composition: 68 ohms ±5%, 1/4 w.	C104 C105	19A116080P205 19A116080P204	Polyester: 0.047 µf ±5%, 50 VDCw. Polyester: 0.033 µf ±5%, 50 VDCw.	R2602	19C314256P26191	Metal film: 6.19K ohms ±1%, 1/4 w.
	19A116655P7	Ceramic disc: 150 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	R114	3R152P392J	Composition: 3.9K ohms ±5%, 1/4 w.	C106	5491674P28	Tantalum: 1.0 µf ±20%, 25 VDCw; sim to			
	19A116655P19	Ceramic disc: 1000 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	R115	3R152P562J	Composition: 5.6K ohms ±5%, 1/4 w.	C107	5496267P9	Sprague Type 162D. Tantalum: 3.3 µf ±20%, 15 VDCw; sim to Sprague	XY2601 XY2602	19B227986G1 19B227986G2	Connector: 8 contacts. Connector: 8 contacts.
	19Al16655P7	Ceramic disc: 150 pf ±20%, 1000 VDCW; sim to	R116	3R152P102J	Composition: lK ohms ±5%, 1/4 w.			Type 150D.			
	19A116080P1	RMC Type JF Discap. Polyester: 0.01 µf ±20%, 50 VDCW.	R117 R118	3R152P101J 3R152P470J	Composition: 100 ohms ±5%, 1/4 w.	C108 C109	19A116080P216 19A116655P20	Polyester: 0.0068 µf ±5%, 50 VDCW. Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim			NOTE: When reordering specify FM ICOM Frequency
	19A116,56P22J0	Ceramic disc: 22 pf ±5%, 500 VDCW, temp coef	R119	3R152P470J	Composition: 47 ohms ±5%, 1/4 w. Composition: 470 ohms ±5%, 1/4 w.	1		to RMC Type JF Discap.			FM ICOM = Operating Frequency
	5491601P132	0 PPM. Phenolic: 4.7 pf ±5%, 500 VDCW.	R121	3R152P220J	Composition: 22 ohms ±5%, 1/4 w.	C110	5491674P36	Tantalum: 3.3 μ f $\pm 20\%$, 10 VDCW; sim to Sprague Type 162D.			48
	19A116656P5J0	Ceramic disc: 5 pf ±0.5 pf, 500 VDCw, temp coef	R122	3R152P102J	Composition: lK ohms ±5%, 1/4 w.	C111	19A116080P206	Polyester: 0.068 μf ±5%, 50 VDCW.	Y2601 thru	19A130605G7	Internally Compensated: ±2 PPM, 806-825 MHz.
	19A116656P22J0	0 PPM. Ceramic disc: 22 pf ±5%, 500 VDCW, temp coef	R123	3R152P680J	Composition: 68 ohms ±5%, 1/4 w.	C112*	5496218P37	Ceramic disc: 6.0 pf ±0.25 pf, 500 VDCw, temp coef 0 PPM. Added by REV B.	Y2604		
	194110030F2230	O PPM.	R124 R125	3R152P100J 3R152P331J	Composition: 10 ohms ±5%, 1/4 w. Composition: 330 ohms ±5%, 1/4 w.	1		DIODES AND RECTIFIERS			
		DIODES AND RECTIFIERS	R126	3R152P752J	Composition: 7.5K ohms ±5%, 1/4 w.	CR101	19A115250Pl	Silicon, fast recovery, 225 mA, 50 PIV.		19C327503G2	Shield. (Located by J103).
	4037822Pl	Silicon, 1000 mA, 400 PIV.	R127	19A116310P39	Composition: 22 ohms ±5%, 0.25 w; sim to Allen- Bradley CB.	and CR102				19C327900P1	Exciter shield.
	19A116052P2	Silicon, hot carrier: Fwd drop .410 v. max. Silicon.	R128	3R77P470J	Composition: 47 ohms ±5%, 1/2 w.	P100	104116650076			4036555P1	Insulator, washer: nylon. (Used with Q101, Q2601).
	19A115775P1 19A116052P2	Silicon, hot carrier: Fwd drop .410 v. max.	R129	3R152P202J	Composition: 2K ohms ±5%, 1/4 w.	P102	19A116659P76	Connector, printed wiring: 9 contacts; sim to Molex 09-52-3091.		19A116707P3	Insulator. (Used with Q102-Q104).
	,	Added by REV A.	R131	3R152P101J	Composition: 100 ohms ±5%, 1/4 w.			RESISTORS		19A129424G2 19B227624G1	Can. (Used with T101-T105). Can. (Used with Z101, Z102).
			R132 R133	3R152P223J 19A116310P37	Composition: 22K ohms ±5%, 1/4 w. Composition: 15 ohms ±5%, 0.25 w; sim to Allen-	R101	19A134231P223J	Deposited carbon: 22K ohms ±5%, 1.8 w; sim to Mepco/Electra Type CR16.		19B201074P203	Tap screw, Phillips POZIDRIV®: No. 4-40 x 3/16
	19A130924G1	Connector, receptacle: coaxial, jack type; sim to Cinch 14H11613.			Bradley CB.	R102	3R152P223J	Composition: 22K ohms ±5%, 1/4 w.		19B232266G1	(Located on 198227831Pl shield- Quantity 3). Oscillator Cover.
	19B219374G1	Connector: 9 contacts.	R134 R135	3R77P390J 3R152P560J	Composition: 39 ohms ±5%, 1/2 w. Composition: 56 ohms ±5%, 1/4 w.	R103*	3R152P471J	Composition: 470 ohms ±5%, 1/4 w.		19A134814P1	Plate nut.
	19A116659P126	Connector, printed wiring: 6 contacts; sim to	R136	3R152P510J	Composition: 51 ohms ±5%, 1/4 w.			In REV A & earlier:			
	19A116659P27	Molex 09-64-1066. Connector, printed wiring: 10 contacts; sim to	R137	3R152P110J	Composition: 11 ohms ±5%, 1/4 w.	R104	3R152P681J 19C314256P25112	Composition: 680 ohms ±5%, 1/4 w. Metal film: 51.1K ohms ±1%, 1/4 w.			
		Molex 09-64-1101.	R138	3R152P102J	Composition: 1K ohms ±5%, 1/4 w.	R105	19C314256P21052	Metal film: 10.50K ohms ±1%, 1/4 w.			
		RELAYS	R139	3R152P153J	Composition: 15K ohms ±5%, 1/4 w.	R106	19C314256P21272	Metal film: 12.70K ohms ±1%, 1/4 w.	H	İ	
	19B209558P1	Hermetic sealed: 180 to 341 ohms coil res, 2 form C contacts, 8.0 to 16.3 VDC; sim to				R107	19C314256P21052	Metal film: 10.50K ohms ±1%, 1/4 w.			
		GE 3SAV1760A2.	RT101	5490828P55	2.2K ohms ±5%, color code yellow; sim to Carborundum Type 0325-F5-144.	R108 R109	19C314256P25111 3R152P132J	Metal film: 5.11K ohms ±1%, 1/4 w. Composition: 1.3K ohms ±5%, 1/4 w.			
						R110	19C314256P25111	Metal film: 5.11K ohms ±1%, 1/4 w.			
	7488079P6	Choke, RF: 1.00 μh $\pm 10\%$, 0.30 ohms DC res max; sim to Jeffers 4411-8.	т101	19C307170P311	Coil, RF: wire size No. 20 AWG; sim to Paul Smith 100375-DS-1.	R111	3R152P153J	Composition: 15K ohms ±5%, 1/4 w.			
	19B209420P7	Coil, RF: 0.33 µh ±5%, 0.22 ohms DC res max; sim to Jeffers 4416-7K.	T102	19C307170P309	Coil, RF: wire size No. 20 AWG; sim to Paul	R112	19C314256P22492				
	19A130255P4	Coil.	and T103		Smith 100375-DS-3.	R113	19C314256P21152 19C314256P23012	Metal film: 11.50K ohms $\pm 1\%$, 1/4 w. Metal film: 30.10K ohms $\pm 1\%$, 1/4 w.		-	
	19A136842P2	Coil.	T104 and	19C307169P204	Coil, RF: wire size No. 20 AWG; sim to Paul Smith 100374-DS-8.	R114 R115	3R152P272J	Composition: 2.7K ohms ±5%, 1/4 w.			
	19A136842P1 19B209420P103	Coil. Coil, RF: 0.15 µh ±10%, 0.10 ohms DC res max;	Т105					OSCILLATOR BOARD			
		sim to Jeffers 4416-3K.	XA101	19A116779P1	Contact, electrical: sim to Molex 08-50-0404.			19C327782G1			
	19B209420P101	Coil, RF: 0.10 µh ±10%, 0.08 ohms DC res max; sim to Jeffers 4416-1K.			(Quantity 9).			CAPACITORS			
		TRANSISTORS			NETWORKS	C2601 thru	19A116655P7	Ceramic disc: 150 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.			
	19A115300P2	Silicon, NPN; sim to Type 2N3053.	Z101 and	19D424303G2	Helical Resonator.	C2604	1011122222			Į	
	19A116818P1	N Channel, field effect; sim to 3N187.	Z102			C2605	19A116655P19	Ceramic disc: 1000 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.			
	19A116201P3	Silicon, NPN.				C2606	19A116655P7	Ceramic disc: 150 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.			
	19A134430P1	Silicon, NPN.					ĺ				

*COMPONENTS ADDED, DELETED OR CHANGED BY PRODUCTION CHANGES

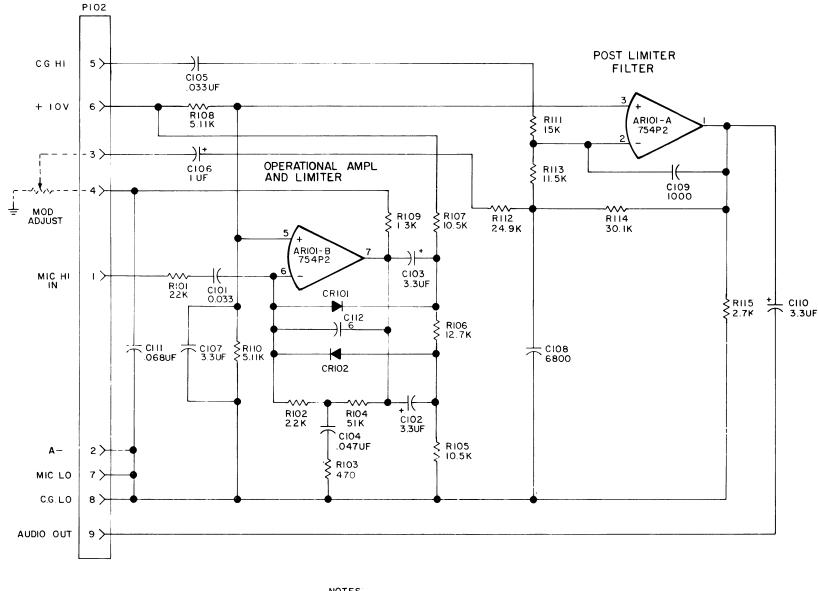
PRODUCTION CHANGES

Changes in the equipment to improve performance or to simplify circuits are identified by a "Revision Letter," which is stamped after the model number of the unit. The revision stamped on the unit includes all previous revisions. Refer to the Parts List for descriptions of parts affected by these revisions.

- REV. A Exciter Board 19D424793G1
 Incorporate reverse voltage clamping diode for Q105.
 Added CR104.
- REV. A <u>Audio Processor 19C321542G1</u>

 Incorporated in initial shipment.
- REV. B To improve audio response. Changed AR101 and R103. Added C112.
- REV. C To improve operation. Changed R103 and AR101.

AUDIO PROCESSOR



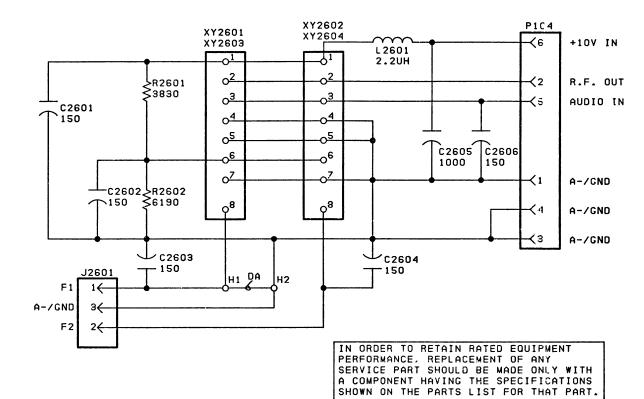
MODEL NO REV LETTER PL19C32I542GI

(19C321854, Rev. 5)

I.CONNECT GRD TO PIN 4 ON ARIOI. CONNECT VCC (+10 V) TO PIN 8 ON ARIOI

ALL RESISTORS ARE 1/4 WATT UNLESS
OTHERWISE SPECIFIED AND RESISTOR
VALUES IN OHMS UNLESS FOLLOWED BY
K=1000 OHMS OR MEG=1,000,000 OHMS
CAPACITOR VALUES IN PICOFARADS (EQUAL
TO MICROMICROFARADS) UNLESS FOLLOWED
BY UF = MICROFARADS, INDUCTANCE VALUES IN MICROHENRYS UNLESS FOLLOWED BY MH= MILLIHENRYS OR H= HENRYS.

OSCILLATOR BOARD



ALL RESISTORS ARE 1/2 WATT UNLESS OTHERWISE SPECIFIED AND RESISTOR VALUES IN OHMS UNLESS FOLLOWED BY K-1000 OHMS OR MEG-1,000,000 CHMS. CAPACITOR VALUES IN PICOFARADS (EQUAL TO MICROMICROFARADS) UNLESS FOLLOWED BY UF-MICROFARADS. INDUCTANCE VALUES IN MICRCHENRYS UNLESS FOLLOWED BY MH-MILLIHENRYS OR H-HENRYS.

THIS ELEM DIAG APPLIES TO MODEL NO REV LETTER PL19C327782G1

1. DA JUMPER WIRE CONNECTED BETWEEN H1 AND H2 IS REMOVED IN MULTI-FREQUENCY UNITS.

(19C327796, Rev. 1)

SCHEMATIC DIAGRAMS

AUDIO PROCESSOR AND OSCILLATOR BOARD