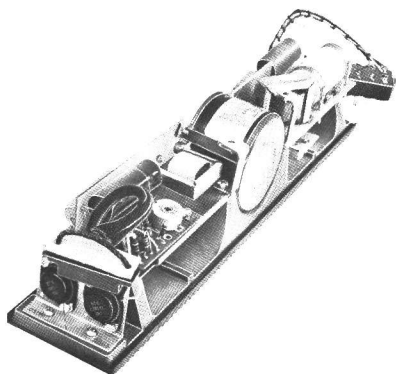


MASTR

Progress Line

12-VOLT, 30 WATT POWER SUPPLY MODEL 4EP37B10



SPECIFICATIONS *

Type Number

EP-37-B

Output

Voltage

Current

Regulated Receiver

10 volts

150 mA

Regulated Transmitter

25-88 MHz

-20 volts

45 mA

132-470 MHz

-20 volts

90 mA

Bias

-45 volts

Low B-Plus

25-88 MHz

300 volts

70 mA

132-174 MHz

300 volts

110 mA

406-470 MHz

300 volts

95 mA

High B-Plus

25-88 MHz

455 volts

150 mA

132-174 MHz

450 volts

160 mA

406-470 MHz

430 volts

200 mA

Battery Drain

Transmit

25-88 MHz

13.6 volts

12 amps

132-174 MHz

13.6 volts

12 amps

406-470 MHz

13.6 volts

14 amps

Receive

Standby-Squelched

13.8 volts

150 mA

Standby-Unsquelched

13.8 volts

1.1 amps

Squelched-Transmitter

Filaments on

13.8 volts

1.2 amps (25-174 MHz)

2.1 amps (406-470 MHz)

Transistors

Multivibrator Circuit

2

10-Volt Regulator Circuit

3

-20 Volt Regulator Circuit

2

Rectifiers

10

Zener Diodes

2

Battery Voltage

13.6 volts $\pm 20\%$ (positive or negative ground, 12-volt system)

Duty Cycle

Transmit: 20% (one minute transmit, four minutes off)

Ambient Temperature Range

-30°C (-22°F) to +60°C (+140°F)

*These specifications are intended primarily for the use of the serviceman. Refer to the appropriate Specification Sheet for the complete specifications.

TABLE OF CONTENTS

SPECIFICATIONS	Cover
DESCRIPTION	1
CIRCUIT ANALYSIS	1
Multivibrator Circuit	1
Rectifier and Filter Circuits	3
-20 Volt Regulator	4
10-Volt Regulator	5
Receiver Muting	5
MAINTENANCE	5
Heat Sink Servicing	5
Reinstallation	5
Disassembly	5
Troubleshooting Procedures	7
OUTLINE DIAGRAM	8
SCHEMATIC DIAGRAM	9
PARTS LIST	10
PRODUCTION CHANGES	10

ILLUSTRATIONS

Figure 1	12-Volt Power Distribution Diagram	2
Figure 2	Simplified Multivibrator Circuit	3
Figure 3	Bias and 20-Volt Regulator Supply Circuit	3
Figure 4	Transmitter Multiplier B-Plus Circuit	3
Figure 5	Power Amplifier B-Plus Circuit	4
Figure 6	-20 Volt Regulator Circuit	4
Figure 7	Disassembly of Power Supply	6

WARNING

No one should be permitted to handle any portion of the equipment that is supplied with high voltage; or to connect any external apparatus to the units while the units are supplied with power. KEEP AWAY FROM LIVE CIRCUITS.

DESCRIPTION

Transistorized Power Supply Model 4EP37B10 is used with 12-volt, 30/35-watt MASTR mobile combinations. The power supply provides:

- Plate, screen and bias voltages for the transmitter multiplier and power-amplifier stages,
- Regulated -20 volts for the transistorized transmitter exciter board,
- Regulated +10 volts for the receiver and for the transmitter Channel Guard.

Low voltage for the transmitter filaments and the receiver audio amplifiers is taken directly from the vehicle battery.

CIRCUIT ANALYSIS

The fully transistorized power supply uses highly efficient silicon rectifiers for reliable operation. The use of Mylar® capacitors provides additional reliability with good performance at low temperatures. Regulation of critical transmitter and receiver supply voltages provides improved operation over the wide range of input voltages encountered in mobile communications.

The power supply may be used in vehicles having either positive or negative ground systems. The power cables are connected for the proper polarity when the Two-Way Radio is installed.

NOTE

No damage will occur if the radio is installed with the polarity accidentally reversed, as long as the transmitter is not keyed. Always check to see if the receiver is operating properly before keying the transmitter.

All connections to the transmitter, receiver and power cables are made through two plug connectors. Two clip-on connectors are used for connecting the power supply to the push-to-talk relay on the system frame. Figure 1 is a simplified power distribution and switching diagram.

MULTIVIBRATOR CIRCUIT (Figure 2)

Power Supply Model 4EP37B10 uses transistors as switches in an inductively coupled multivibrator circuit. These switches connect the battery voltage across alternate halves of the transmitter primary, resulting in alternating square waves. The output of the multivibrator circuit (square wave generator) is stepped up by power transformer T502, then rectified and filtered to supply B-plus and bias voltage for the transmitter.

Keying the transmitter closes the relay contacts and applies power to transistors Q501 and Q502. The bases of the transistors are biased negatively (with respect to their emitters) through resistor R504, and all transistors start to conduct. Due to inherently different characteristics, one transistor will conduct slightly more than the others.

Assuming that Q501 will initially conduct more than Q502, Q501 will draw more current through winding 1-2/3 of T502 than Q502 will draw through winding 2-3/4, making terminal 1 more positive than terminal 4.

The increasing magnetic field in the core of T502 induces a voltage in the windings 5-6-7, causing winding 7 to become negative with respect to the emitter of Q501. This increased bias causes Q501 to conduct even harder. At the same time, winding 5 becomes positive with respect to the emitter of Q502, stopping current flow through Q502 and winding 2-3/4. Current through winding 1-2/3 rapidly saturates the core of the transformer, and the magnetic field ceases to increase.

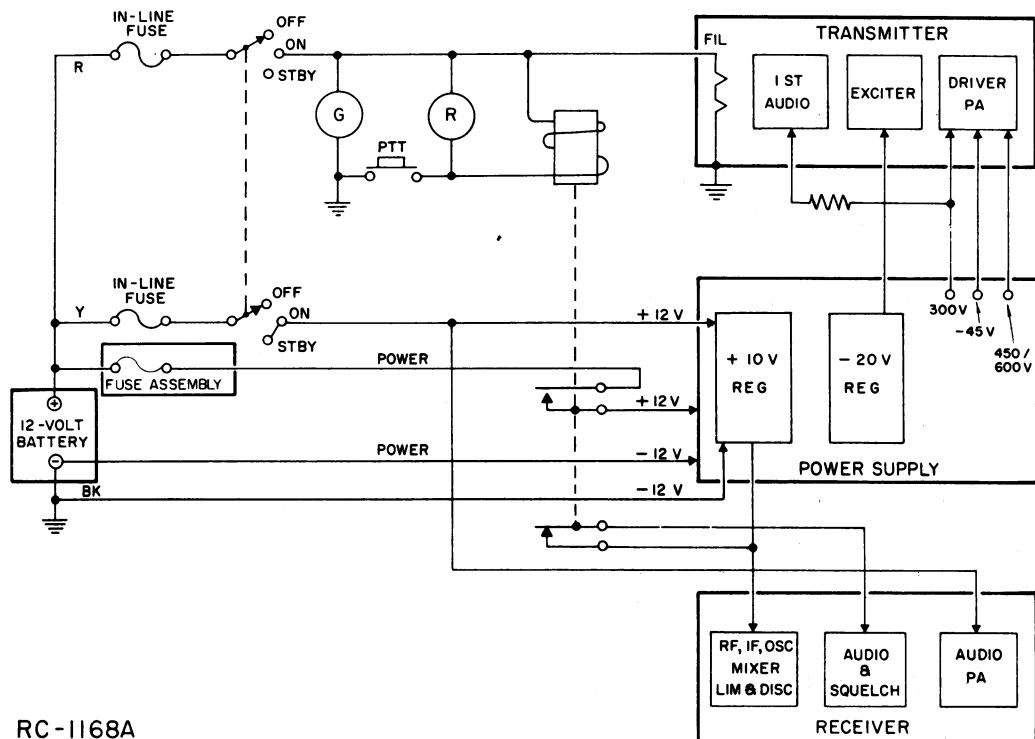
The voltage being induced in winding 5-7 therefore falls to zero, reducing the bias to Q501 to that obtained through R504. This reduced bias tends to cut off Q501 and reduce the current through winding 1-2/3.

The collapsing magnetic field in T502 induces a reverse voltage across winding 5-6-7, biasing Q501 off and biasing Q502 on. Q502 now conducts in a similar manner until T501 is again saturated.

Resistor R502 limits the base current which can flow through Q501 and Q502.

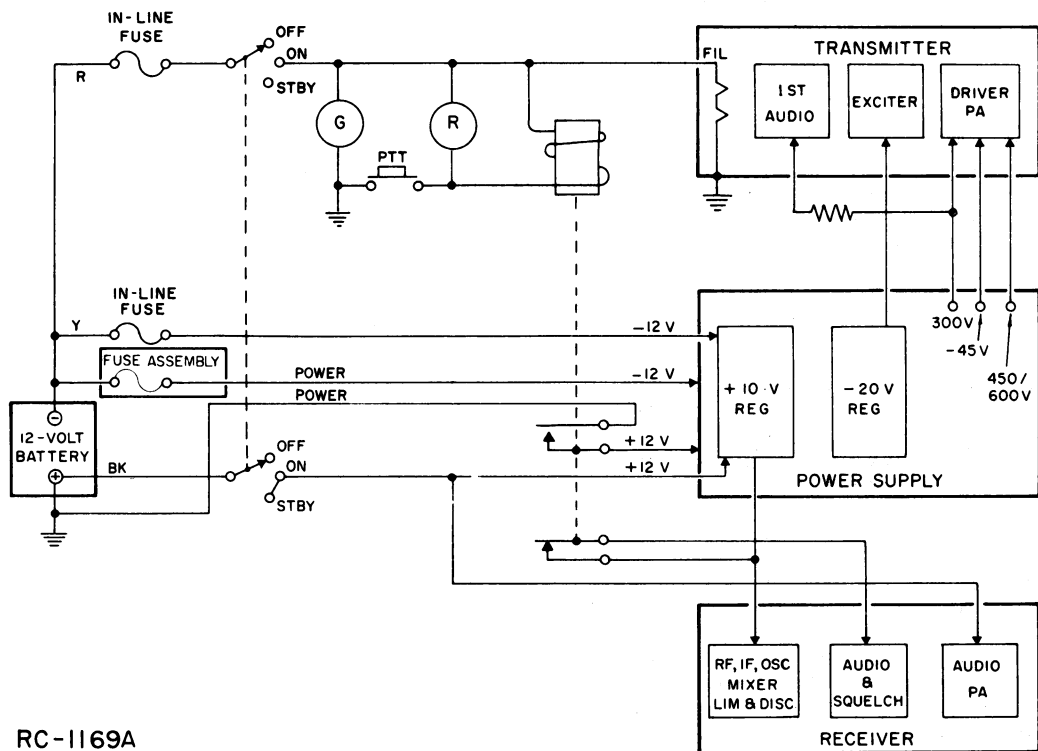
The two transistors continue to conduct alternately at a frequency of approximately 1330 hertz. The resulting waveform approaches that of a perfect square wave.

12 VOLT NEGATIVE GROUND



RC-II68A

12 VOLT POSITIVE GROUND



RC-II69A

Figure 1 - 12-Volt Power Distribution Diagrams

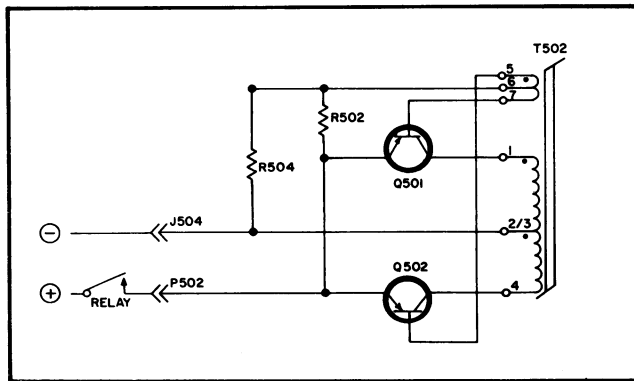


Figure 2 - Simplified Multivibrator Circuit

RECTIFIER AND FILTER CIRCUITS

Negative Bias and 20-Volt Regulator Supply (Figure 3) - The AC voltage developed across secondary windings 12-8-14 of transformer T502 is rectified by full-wave rectifiers CR501 and CR502. It is then filtered by C501, L502 and C502 to supply a negative 45 volts for the control grids of the transmitter driver and power amplifier, and also to supply 45 volts for the input of the 20-volt regulator. The bias voltage is present as a protective measure to limit cathode current in the PA tube while the PA is untuned, or in the case of loss of drive to the PA.

Transmitter Multiplier B-Plus (Figure 4) - The AC voltage developed across high voltage secondary windings of T502 is rectified by a full-wave, tapped bridge rectifier circuit.

During one-half of each AC cycle, the voltage across terminals 17 and 18 of the high voltage output winding is rectified by CR503 and CR507. During the second half of the cycle, the voltage across terminals 15 and 21 is rectified by CR504 and CR509.

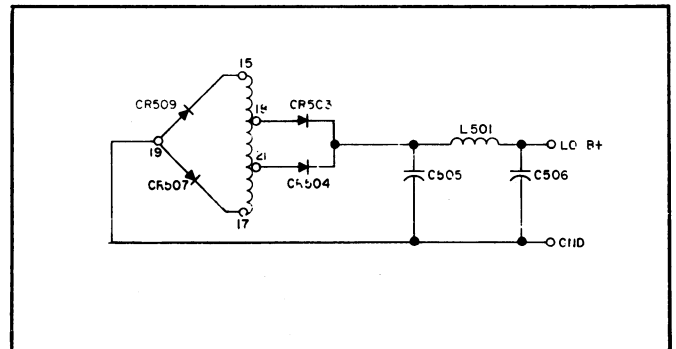


Figure 4 - Transmitter Multiplier B-Plus Circuit

Filtering is provided by L-C filter C505, L501 and C506. Relatively small values of L and C are required because of the high frequency and the square wave characteristics of the AC voltage. R505 prevents ringing in the oscillator circuit formed by C505, L501 and C506.

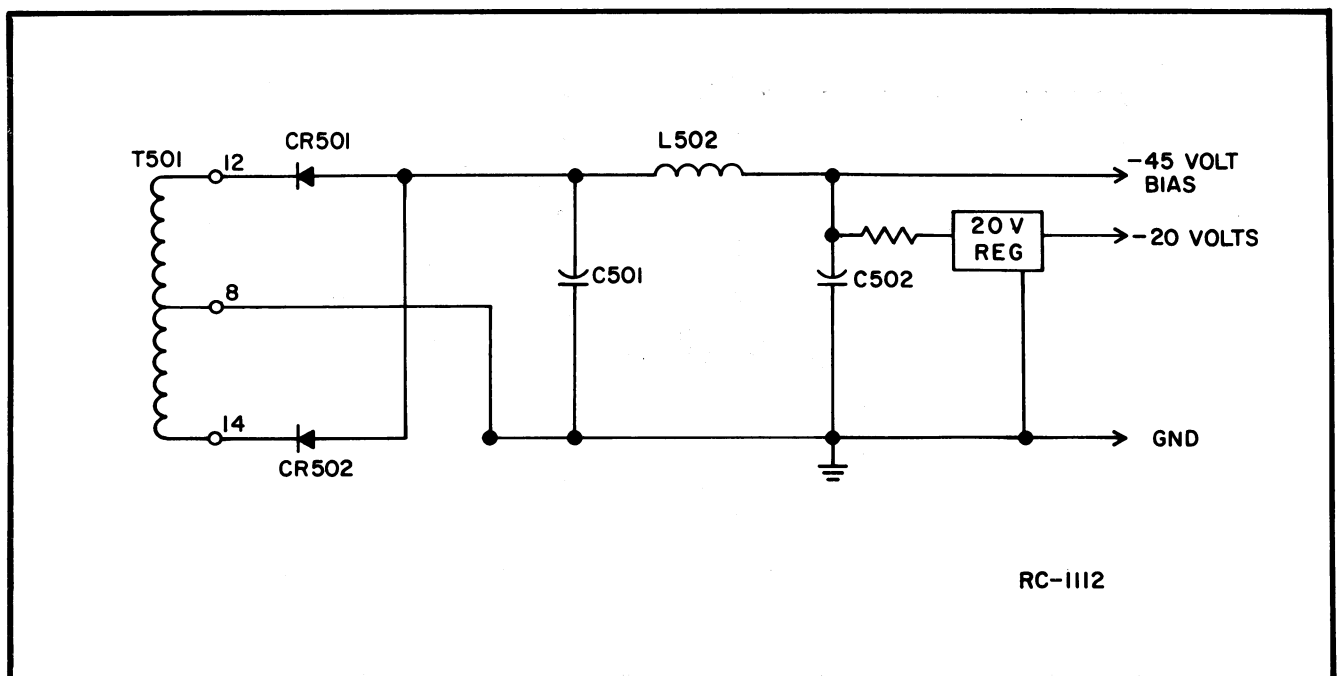


Figure 3 - Bias and 20-Volt Regulator Supply Circuit

Power Amplifier B-Plus (Figure 5) - The AC voltage developed across the high voltage secondary windings 15-17 of T502 is rectified by bridge rectifier circuit CR507, CR508, CR509 and CR510. The output of the bridge rectifier circuit provides the High B-Plus output. Filtering is provided by C508. Resistors R510 and R511 form a bleeder circuit which discharges C508 when the keying relay is opened.

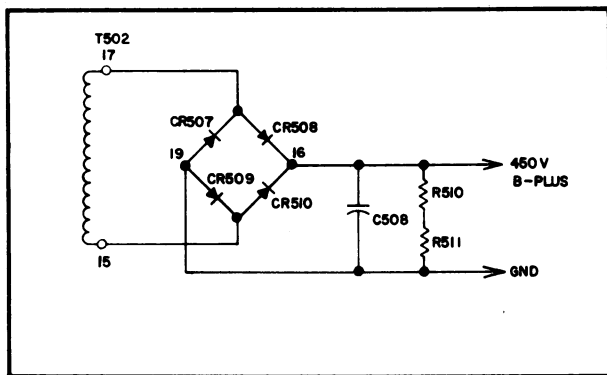


Figure 5 - Power Amplifier B-Plus Circuit

-20 VOLT REGULATOR (Figure 6)

The -20 Volt Regulator provides a closely controlled supply voltage for the transistorized exciter section of the transmitter. Input power is taken from the -45 volt bias output at TB1-3. Dropping resistor R507 provides the negative bias to turn on Q506. Zener diode VR501 provides a voltage reference for the regulator.

When the input voltage at TB1-3 rises, the output voltage at the emitter of Q506 also tends to rise. This causes a change in the base-emitter bias on Q507, making it conduct more heavily. When Q507 conducts, there is less base bias on Q506, and less base current. With less base current, the voltage drop across Q506 is larger, and the output voltage remains constant.

When the input voltage starts to drop, the output voltage also tends to drop, causing Q507 to conduct less. This increases the forward bias on Q506 and reduces the voltage drop across the transistor so that the output voltage remains constant. Capacitor C511 prevents high frequency oscillation.

R506, R508 and R512 form an adjustable voltage divider so that potentiometer R508 can be adjusted for a -20 volt output. R509 provides bias current for VR501. The output is metered at the transmitter centralized metering jack J102-12.

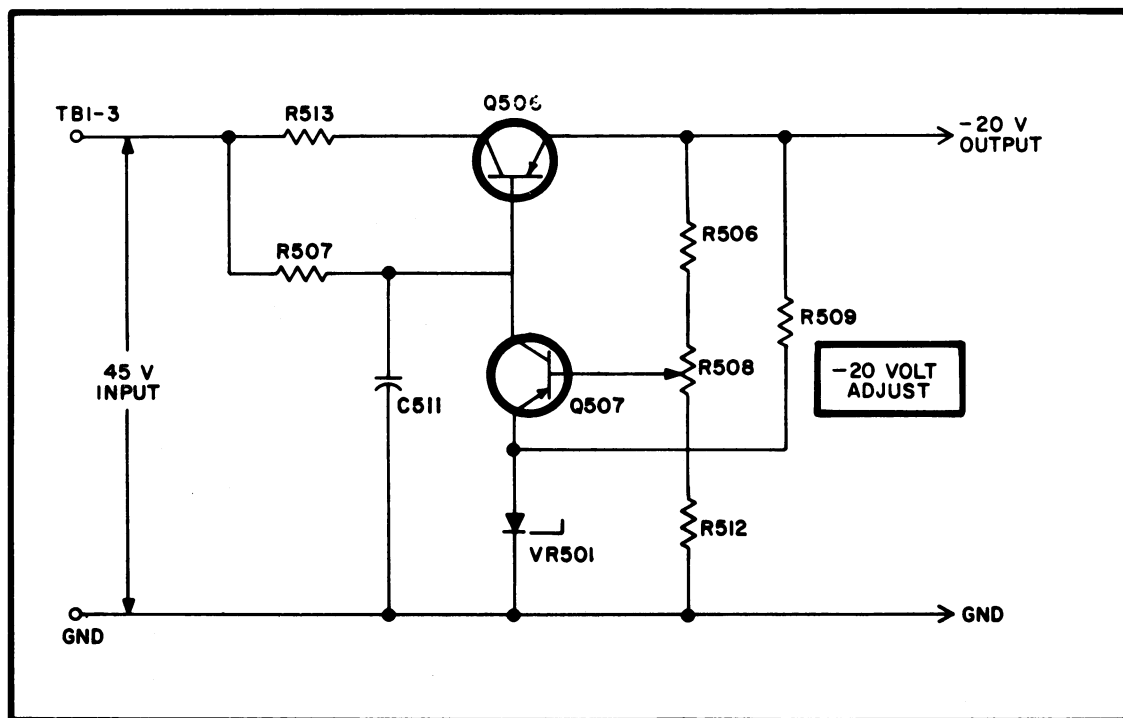


Figure 6 - -20 Volt Regulator Circuit

10-VOLT REGULATOR A501

The 10-Volt Regulator Circuit provides a closely controlled supply voltage for the receiver (except for the audio amplifier), and a supply voltage for the transmitter Channel Guard option, when present. Input voltage is supplied from the Control Unit on P505-5.

When the supply voltage (or output) starts to increase, the voltage at the base of Q1 also increases. As the emitter voltage of Q1 is kept constant by VR1, the emitter-base voltage increases. This causes Q1 to conduct more which means less base current for Q505. The voltage drop across Q505 becomes larger and the output remains constant.

When the input voltage starts to drop, the output voltage also tends to drop and Q1 will conduct less. This increases the forward bias on Q505 and reduces the voltage drop across Q505 to keep the output constant.

Diode CR1 gives reverse polarity protection to the supply. Potentiometer R4 is used to set the emitter-base voltage of Q1 for the desired 10-Volt $\pm 5\%$ output. R1 and R3 limit maximum current through Q1. R2 provides bias current for Zener diode VR1, and resistor R7 provides bias for Q505. C1 and C3 prevent high frequency oscillation. The output voltage is metered at P505-7.

RECEIVER MUTING

Transistor Q2 on the 10-volt regulator board operates as a switch for the receiver muting +10 volts. When the transmitter is not keyed, the base of Q2 is connected to ground, causing Q2 to conduct. When conducting, the +10 volts at the collector of Q2 is coupled from P505 to the base of receiver DC amplifier Q9, turning it on. With Q9 conducting Q10 is turned off, allowing the receiver to operate normally.

Keying the transmitter applies +12 volts to the base of the PNP muting switch (Q2), turning it off. This removes the +10 volts to receiver DC amplifier Q9, turning it off. Turning off Q9 causes DC amplifier Q10 to turn on, which turns off the receiver audio stages and mutes the receiver.

MAINTENANCE

HEAT SINK SERVICING

Since the metal envelopes of the transistors are at collector potential, they must be electrically isolated from ground. However, there must be a good path for heat

from the transistors to reach the cast aluminum radiator (heat sink) in which they are mounted, so that the heat will be dissipated by the heat sink. The anodized aluminum spacers used between the transistors and their mounting plate not only isolate the transistors electrically, but also provide a good conductor to conduct heat away from them.

Silicone grease is used between the metal parts in the heat sink to improve the thermal contact between them and allow the heat to be transferred more readily.

NOTE

Whenever the transistor mounting plate is removed from the heat sink, be sure that there is sufficient silicone grease on the plate to make good contact with the heat sink before it is replaced. There should also be a coating of grease beneath the transistors and beneath the anodized aluminum spacers.

REINSTALLATION

If the mobile combination in which the power supply is mounted is ever moved to a different vehicle, be sure to check the battery polarity of the new system and, if necessary, change the power cable connections to the fuse assembly along with ignition switch cables to maintain current polarity.

DISASSEMBLY

To service the power supply--

1. Pull the locking handle down and pull radio out of mounting frame.
2. Remove the two screws in bottom cover and take off cover.

To remove the power supply from the system frame--

1. Complete Steps 1 and 2 above.
2. Remove the two Phillips-head retaining screws in the front casting, and pull casting away from system frame.
3. Pry power connector out of connector supporting bracket. Next, unplug the clip-on connectors to the system relay, and unplug systems connector at the back of the power supply.
4. Lift the Two-Way Radio away from power supply.

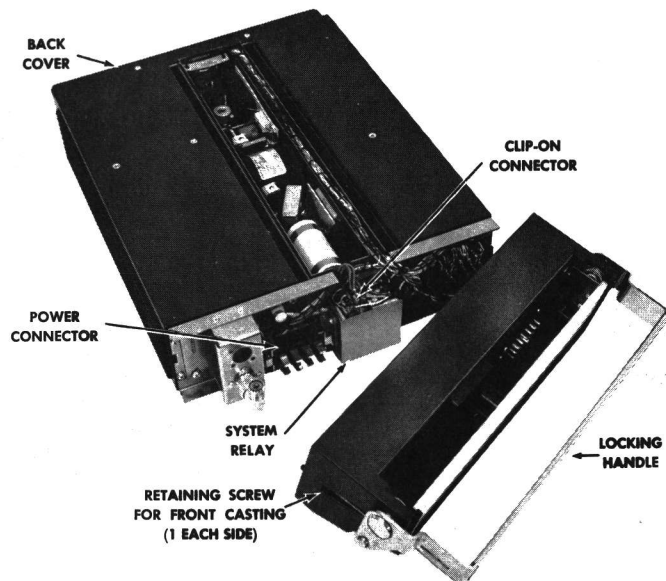
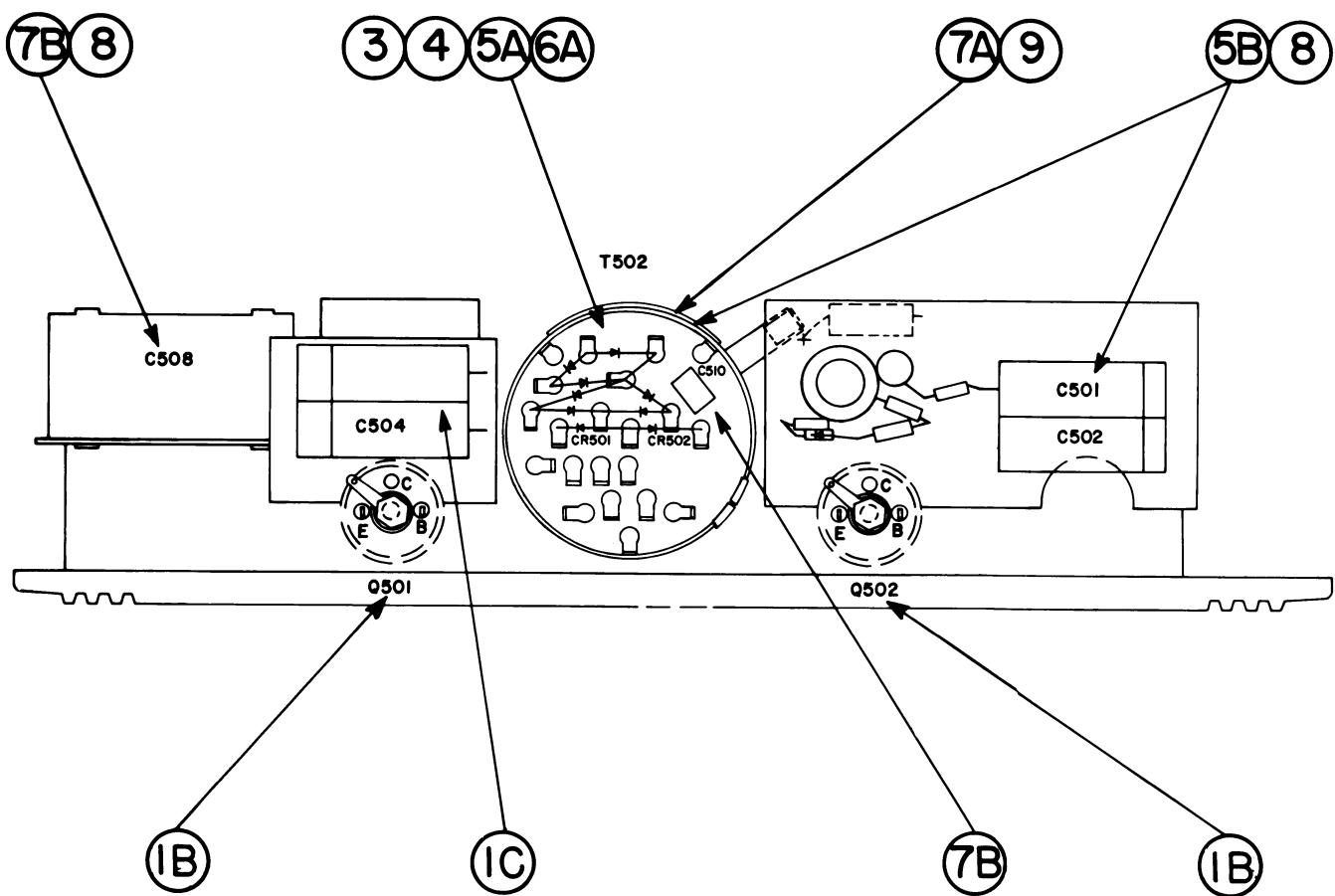
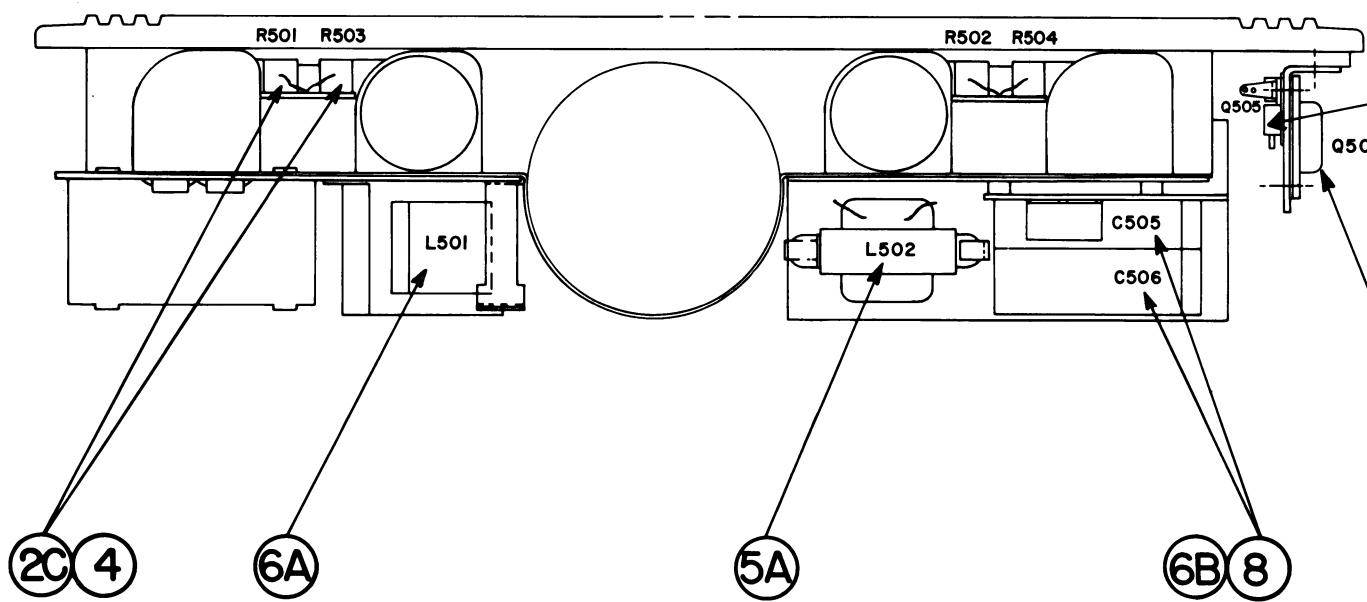


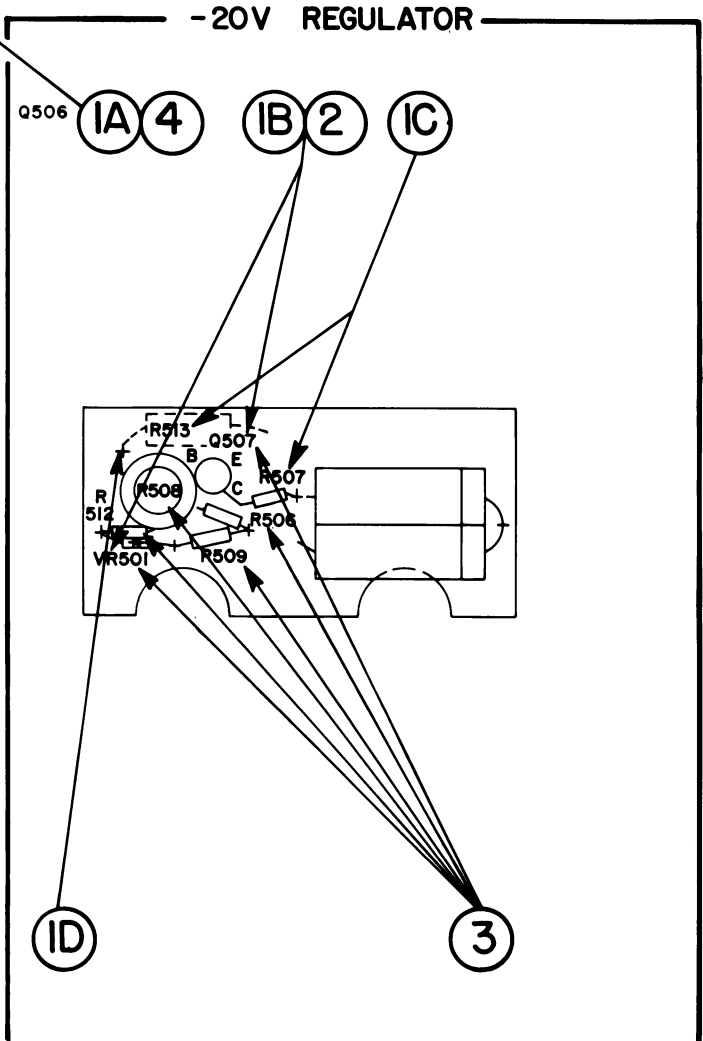
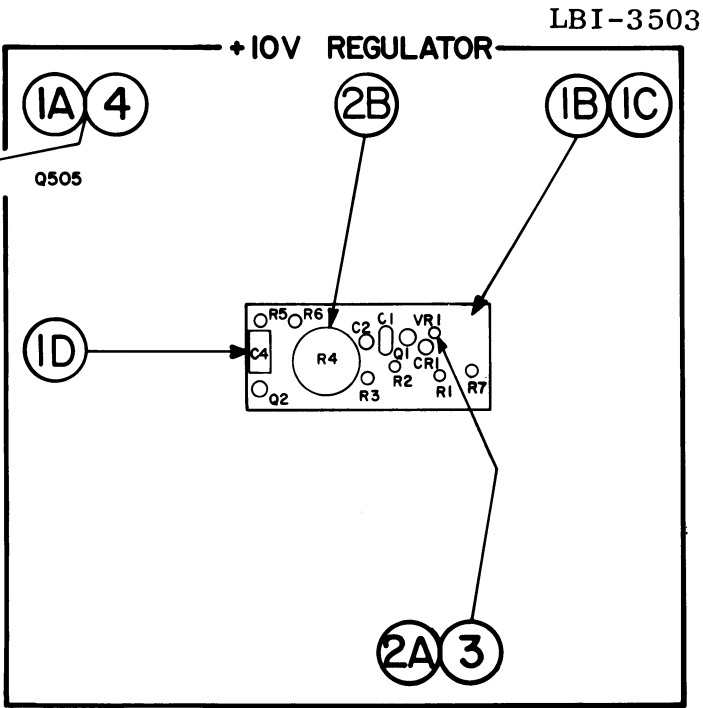
Figure 7 - Disassembly of Power Supply

STEP 1 - QUICK CHECKS

SYMPTOM	PROCEDURE	
No power supply output voltages at P505 when unit is keyed	<p>Check for 12 volts at J504-3-7. If O.K., go to Step 2; otherwise check:</p> <p>1. A. Check fuse assembly for open circuit. If fuse is open, check:</p> <p>B. Collector-to-emitter short in Q501, Q502, primary wiring short.</p> <p>C. If Q501 or Q502 is shorted, check for shorted C504.</p> <p>With 12 volts at J504, check the following steps:</p> <p>2. A. Open fuse in system cable.</p> <p>B. Keying relay in system should close when PTT switch is depressed.</p> <p>C. Open R501, R503.</p> <p>3. Check T502 for shorts and opens. Check for shorted winding turns by applying a 1/2-volt P-P from an audio signal generator to the primary winding of T502. Check output of each secondary winding with a scope. No output indicates shorted turns.</p>	
Output voltages low	4. Open R501, R503, diodes in affected circuit.	
No -45 volts at P505-2.	5. A. Open CR501, CR502, L502, T502.	B. Shorted C502, C501, T502.
No 300 volts at P505-1.	6. A. Open CR503, CR504, CR507, CR509, L501, T502.	B. Shorted C505, C506.
No 450 volts at P505-9	7. A. Oper CR507 through CR510 (two or more), T502.	B. Shorted C508, C510.
Excessive output ripple voltages	8. Open diodes, C501, C502, C505, C506, C508, C510.	
Reverse or high output voltage on bias output	9. Check for short between bias output winding and B+ output winding of T502.	
10-VOLT REGULATOR		
No 10 volts regulated at P505-7	1. Check for the following:	
	A. Open Q505.	
	B. 12 volts input.	
	C. Open DS1 (where applicable).	
	D. Shorted C4.	
	E. Open fuse in vehicle system.	
Output voltage too high, cannot be adjusted by R6	2. A. Check for open VR1.	B. Defective R4.
Very low output voltage	3. Check for a shorted VR1	
Output voltage equals input voltage	4. Shorted Q505.	
-20 VOLT REGULATOR		
No -20 volt regulated at P505-3	1. Check for the following:	
	A. Open Q506.	
	B. Shorted Q507 and/or VR501.	
	C. Open R507, R513.	
	D. -45 volts at TB1-18.	
Very low output voltage	2. Shorted Q507 or VR501.	
Output voltage too high, cannot be adjusted by R508	3. Open VR501, Q507, R506, R508, R509, R512.	
Output voltage equals input voltage	4. Shorted Q506.	

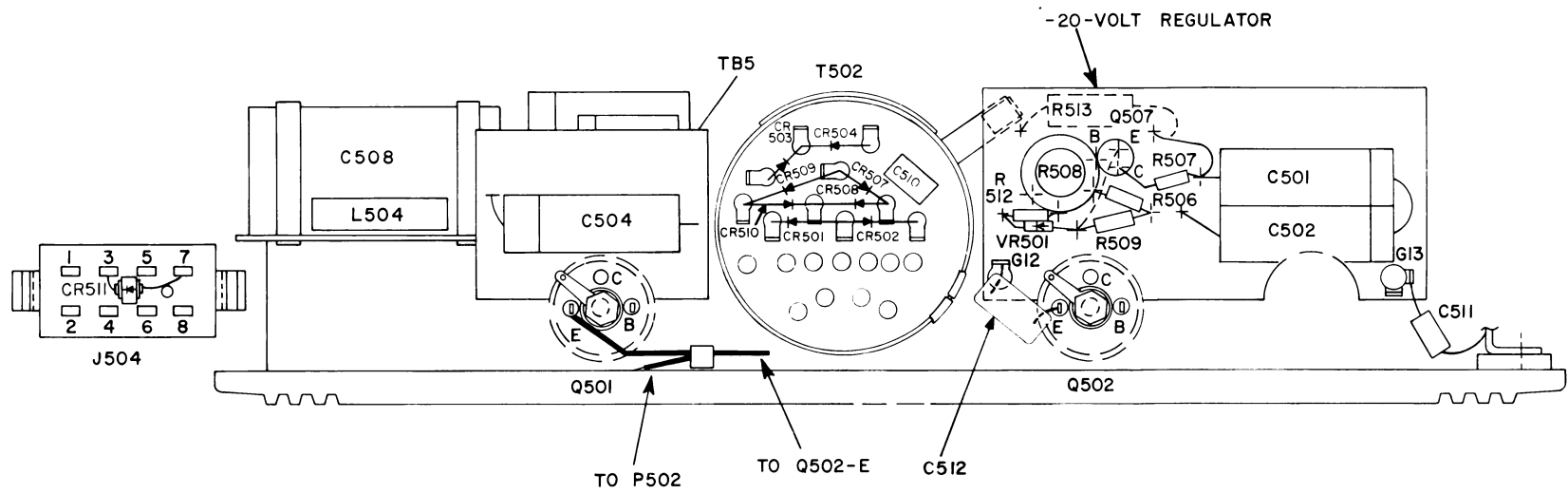
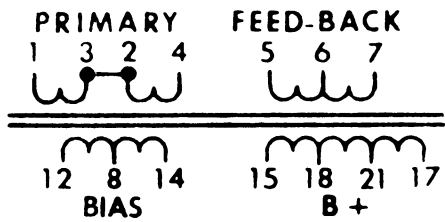
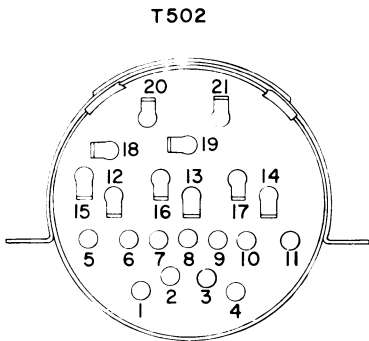
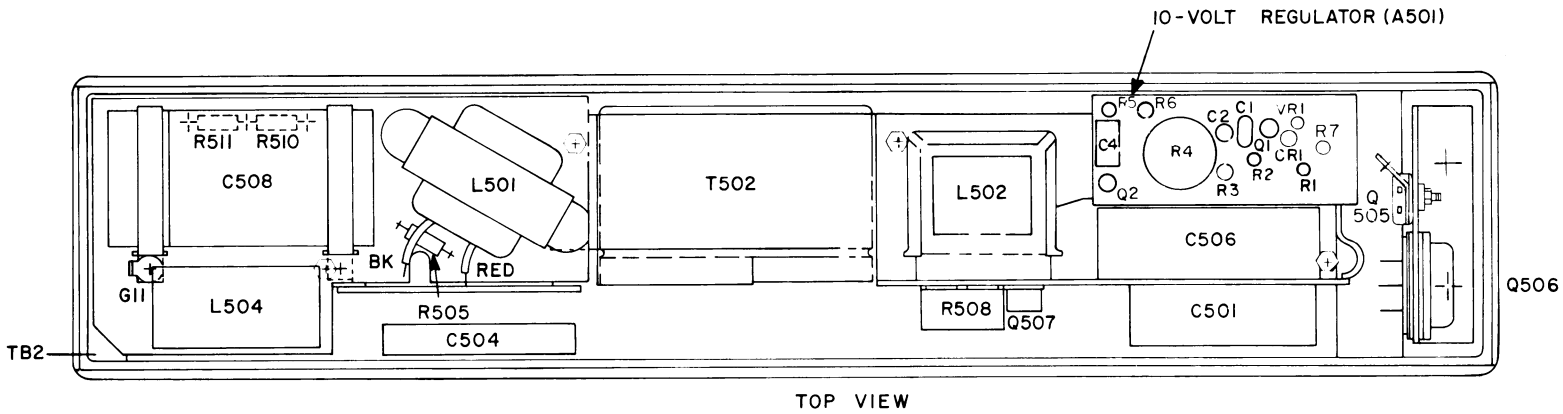
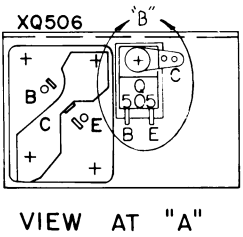
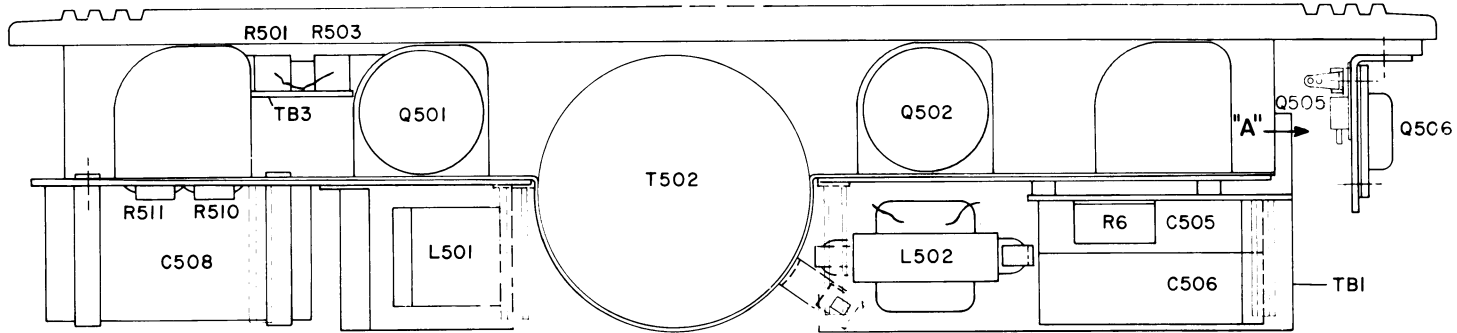


RC-1155C

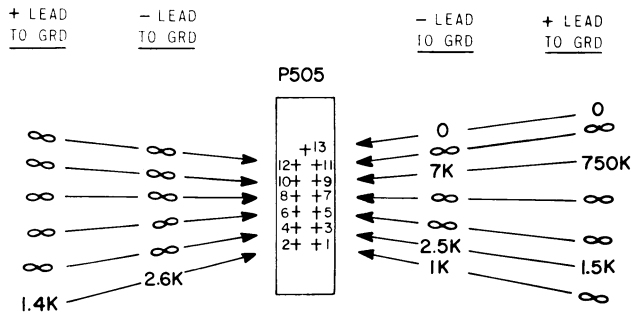


TROUBLESHOOTING PROCEDURE

30/35-WATT MASTR POWER SUPPLY
MODEL 4EP37B10

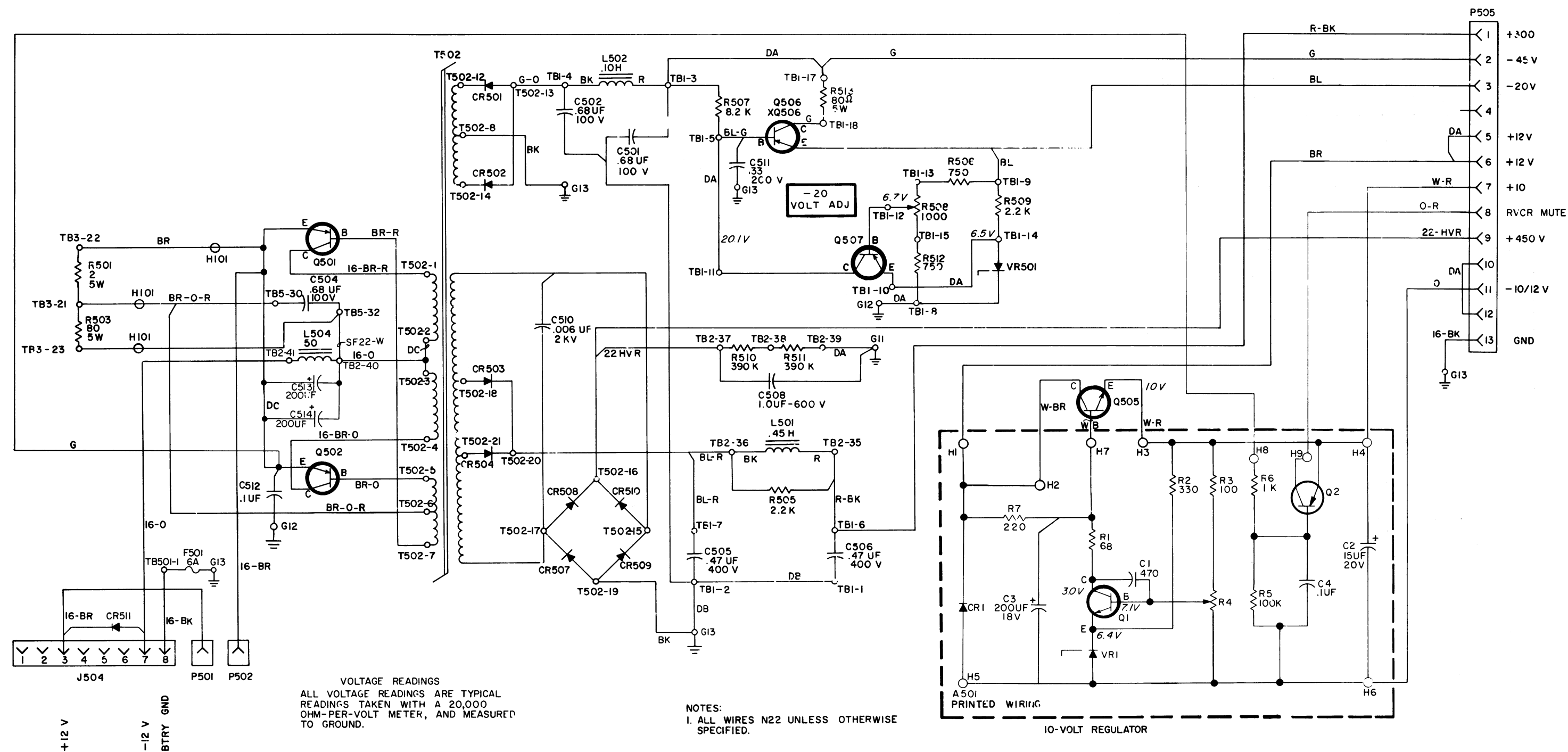


RESISTANCE READINGS
ALL RESISTANCE READINGS ARE TYPICAL READINGS
TAKEN WITH A 20,000 OHMS-PER-VOLT METER TO CHASSIS GROUND.



OUTLINE DIAGRAM

30/35-WATT MASTR POWER SUPPLY
MODEL 4EP37B10



VOLTAGE READINGS
ALL VOLTAGE READINGS ARE TYPICAL
READINGS TAKEN WITH A 20,000
OHM-PER-VOLT METER, AND MEASURED
TO GROUND.

NOTES:
1. ALL WIRES N22 UNLESS OTHERWISE SPECIFIED.

ALL RESISTORS ARE 1/2 WATT UNLESS OTHERWISE SPECIFIED AND RESISTOR VALUES IN OHMS UNLESS FOLLOWED BY K=1000 OHMS OR MEG=1,000,000 OHMS CAPACITOR VALUES IN PICOFARADS (EQUAL TO MICROMICROFARADS) UNLESS FOLLOWED BY UF= MICROFARADS. INDUCTANCE VALUES IN MILLIHENRYS UNLESS FOLLOWED BY MH= MICROHENRYS OR H=HENRYS

SCHEMATIC DIAGRAM

30/35-WATT MASTR POWER SUPPLY
MODEL 4EP37B10

Issue 9

9

- NOTE

For 60-watt input (Class A Citizens Band) move the two red wires from T502-16 to T502-20.

SYMBOL	GE PART NO.	DESCRIPTION
A501*		10 VOLT REGULATOR BOARD 19C317751G1
C1	7774750P1	Ceramic disc: .00047 μ f +100 -0%, 500 VDCW.
C2	5496267P14	Tantalum: 15 μ f \pm 20%, 20 VDCW; sim to Sprague Type 150D.
C3	19A115680P10	Electrolytic: 200 μ f +150% -10%, 18 VDCW; sim to Mallory Type TT.
C4	19A116080P107	Polyester: 0.1 μ f \pm 10%, 50 VDCW.
CR1	4037822P1	Silicon.
DS1*	4034664P1	Lamp, incandescent: 28 v; sim to GE 2148. Deleted by REV R.
Q1*	19A116755P1	Silicon, NPN; sim to Type 2N3947. In REV T and earlier:
	19A115123P1	Silicon, NPN; sim to Type 2N2712.
Q2*	19A115852P1	Silicon, PNP; sim to Type 2N3906. In REV T and earlier:
	19A115768P1	Silicon, PNP; sim to Type 2N3702.
R1	3R77P680K	Composition: 68 ohms \pm 10%, 1/2 w.
R2	3R77P331J	Composition: 330 ohms \pm 5%, 1/2 w.
R3	3R77P101J	Composition: 100 ohms \pm 5%, 1/2 w.
R4	19A115681P1	Variable: 1000 ohms \pm 20%, 3 w.
R5	3R77P104K	Composition: 0.10 megohm \pm 10%, 1/2 w.
R6*	3R77P102K	Composition: 1000 ohms \pm 10%, 1/2 w. In REV L and earlier:
	3R77P103K	Composition: 10,000 ohms \pm 10%, 1/2 w.
R7*	3R77P221J	Composition: 220 ohms \pm 5%, 1/2 w. Added by REV R.
VR1	4036887P6	Silicon, Zener.
A501*		In Models of REV G, H, J and K: 10 VOLT REGULATOR BOARD 19C303420G7
C4	7774750P1	Ceramic disc: .00047 μ f +100 -0%, 500 VDCW.
C5	5496267P14	Tantalum: 15 μ f \pm 20%, 20 VDCW; sim to Sprague Type 150D.
C6	19A115680P10	Electrolytic: 200 μ f +150% -10%, 18 VDCW; sim to Mallory Type TT.
CR3	4037822P1	Silicon.

SYMBOL	GE PART NO.	DESCRIPTION
DS1	4034664P1	----- INDICATING DEVICES ----- Lamp, incandescent: 28 v; sim to GE 2148.
Q5	19A115123P1	----- TRANSISTORS ----- Silicon, NPN; sim to Type 2N2712.
R8	3R77P680K	----- RESISTORS ----- Composition: 68 ohms \pm 10%, 1/2 w.
R9	3R77P331J	Composition: 330 ohms \pm 5%, 1/2 w.
R10	3R77P101J	Composition: 100 ohms \pm 5%, 1/2 w.
R11	19A115681P1	Variable: 1000 ohms \pm 20%, 3 w.
VR4	4036887P6	----- VOLTAGE REGULATORS ----- Silicon, Zener.
A501*		In Models of REV D, E and F: 10-VOLT REGULATOR BOARD 19C303420G5
C4	7774750P1	----- CAPACITORS ----- Ceramic disc: .00047 μ f +100 -0%, 500 VDCW.
C5	5496267P14	Tantalum: 15 μ f \pm 20%, 20 VDCW; sim to Sprague Type 150D.
CR2*	19A115250P1	----- DIODES AND RECTIFIERS ----- Silicon. Deleted by REV H.
CR3*	4037822P1	Silicon. Added by REV H.
DS1	4034664P1	----- INDICATING DEVICES ----- Lamp, incandescent: 28 v; sim to GE2148.
Q5	19A115123P1	----- TRANSISTORS ----- Silicon, NPN; sim to Type 2N2712.
R8*	3R77P680K	----- RESISTORS ----- Composition: 68 ohms \pm 10%, 1/2 w. In Models of REV D and earlier:
	3R77P161J	Composition: 160 ohms \pm 5%, 1/2 w.
R9	3R77P331J	Composition: 330 ohms \pm 5%, 1/2 w.
R10	3R77P101J	Composition: 100 ohms \pm 5%, 1/2 w.
R11	19A115681P1	Variable: 1000 ohms \pm 20%, 3 w.
VR4	4036887P6	----- VOLTAGE REGULATORS ----- Silicon, Zener.
A501*		In Models of REV C and earlier: 10-VOLT REGULATOR BOARD 19C303420G1
C1	5496267P10	----- CAPACITORS ----- Tantalum: 22 μ f \pm 20%, 15 VDCW; sim to Sprague Type 150D.
CR1	4037822P1	----- DIODES AND RECTIFIERS ----- Silicon.
Q1*	4037993P1	----- TRANSISTORS ----- Germanium, PNP; sim to Type 2N1303. Deleted by REV C.
Q2	19C300073P2	Germanium, PNP; sim to Type 2N1414.
Q3	19A115123P1	Silicon, NPN; sim to Type 2N2712.
R1	3R77P680J	----- RESISTORS ----- Composition: 68 ohms \pm 5%, 1/2 w.

SYMBOL	GE PART NO.	DESCRIPTION
R3	3R77P242J	Composition: 2400 ohms \pm 5%, 1/2 w.
R4	3R77P331J	Composition: 330 ohms \pm 5%, 1/2 w.
R5	3R77P681J	Composition: 680 ohms \pm 5%, 1/2 w.
R6	19B209113P1	Variable, wirewound: 250 ohms \pm 20%, 2.5 w.
R8	3R77P680K	Composition: 68 ohms \pm 10%, 1/2 w.
VR1	4036887P9	----- VOLTAGE REGULATORS ----- Silicon, Zener.
C501 and C502	19B209004P11	----- CAPACITORS ----- Polyester: 0.68 μ f \pm 10%, 100 VDCW; sim to Sprague 157P.
C504	19B209004P11	Polyester: 0.68 μ f \pm 10%, 100 VDCW; sim to Sprague 157P.
C505 and C506	5491656P42	Polyester: 0.47 μ f \pm 20%, 400 VDCW; sim to GE Type 61F.
C508	5491656P39	Polyester: 1 μ f +30% -10%, 600 VDCW; sim to GE Type 61F.
C510	5490825P4	Ceramic disc: 6000 pf \pm 10%, 2000 VDCW; sim to RMC Type JF Discap.
C511	19A115028P17	Polyester: 0.33 μ f \pm 20%, 100 VDCW.
C512*	19A115028P14	Polyester: 0.1 μ f \pm 20%, 100 VDCW. Added by REV B.
C513* and C514*	19A115680P10	Electrolytic: 200 μ f +150% -10%, 18 VDCW; sim to Mallory Type TT. Added by REV N.
CR501 thru CR504	4037822P1	----- DIODES AND RECTIFIERS ----- Silicon.
CR507 thru CR510	19A115845P4	Silicon.
CR511*	19A116783P1	Silicon. Added by REV T.
F501*	19A116658P14	----- FUSES ----- Enclosed link: 6 amp at 250 v; sim to Bussman GJV 6. Added by REV T.
J504	19A121524G1	----- JACKS AND RECEPTACLES ----- Connector, phen: 8 contacts rated at 15 amps at 1100 VRMS.
L501	19A121120P1	----- INDUCTORS ----- Reactor: 0.45 h +0.5 -.05 h ind min at 0.15 amp DC, 20 ohms \pm 10% DC res, 1000 v peak, 420 VDC operating.
L502	19B200777P1	Reactor: 0.1 h ind min at 0.15 amp DC, 12 ohms \pm 10% DC res, 720 v peak, 300 VDC operating.
L504	19A115392P1	Coil, RF: 50 μ h \pm 10% ind at 1000 Hz, .02 ohm DC res.
P501 and P502	19B209151P1	----- PLUGS ----- Terminal, solderless; sim to Amp 42284-5.
P505	19B204781P1	Phen: 13 female contacts.
Q501 and Q502	5490810P1	----- TRANSISTORS ----- Germanium, PNP.
Q505*	19A116742P1	Silicon, NPN.
	19A116203P3	Silicon, NPN. (REV K-T).
	19A116118P1	Silicon, NPN. (REV J).
	19A115948P1	Silicon, NPN. (REV F, G, and H).
	19A115527P1	Silicon, NPN. (REV D and E).
	19A115267P1	Germanium, PNP. (REV A, B, and C).

SYMBOL	GE PART NO.	DESCRIPTION
Q506	19A115341P1	Germanium, PNP.
Q507*	19A115852P1	Silicon, PNP; sim to Type 2N3906. In REV T and earlier:
	19A115768P1	Silicon, PNP; sim to Type 2N3702.
R501	5493035P3	----- RESISTORS ----- Wirewound, ceramic: 2 ohms \pm 5%, 5 w; sim to Hamilton Hall Type HR.
R503	5493035P4	Wirewound, ceramic: 80 ohms \pm 5%, 5 w; sim to Hamilton Hall Type HR.
R505	3R77P222K	Composition: 2200 ohms \pm 10%, 1/2 w.
R506	3R77P751J	Composition: 750 ohms \pm 5% 1/2 w.
R507	3R77P822K	Composition: 8200 ohms \pm 10%, 1/2 w.
R508	19B209113P3	Variable, wirewound: 1000 ohms \pm 20%, 2.5 w.
R509	3R77P222K	Composition: 2200 ohms \pm 10%, 1/2 w.
R510 and R511	3R77P394K	Composition: 0.39 megohm \pm 10%, 1/2 w.
R512	3R77P751J	Composition: 750 ohms \pm 5%, 1/2 w.
R513	5493035P4	Wirewound, ceramic: 80 ohms \pm 5%, 5 w; sim to Hamilton Hall Type HR.
T502	19C304106G2	----- TRANSFORMERS ----- Transformer.
TB1	19C303431G1	----- TERMINAL BOARDS ----- Eyelet board.
TB2	19B204509G1	Eyelet board.
TB3	19B204463G1	Eyelet board.
TB5	19C303422G1	Eyelet board.
VR501	4036887P6	----- VOLTAGE REGULATORS ----- Silicon, Zener.
XQ505*	5491888P1	----- SOCKETS ----- Transistor, phen: sim to Cinch 133-92-10-034. Deleted by REV D.
XQ506	5491888P1	Transistor, phen: sim to Cinch 133-92-10-034.
		MECHANICAL PARTS (SEE RC-1173)
1	7763541P4	Cable clamp. (Used with P505 cable).
2	4036555P1	(Not Used).
3	7140624P6	Spacer. (Used with A501).
4	19C303429P1	Support. (Used with A501).
5	7160861P2	Speed nut. (Used with T502).
6	19A121220P1	Support. (Used with power supply cover).
7	19B204454G2	(Not Used).
8	19D402261P1	Heat sink.
9	7160861P10	(Not Used).
10	7142162P89	(Not Used).
11	19B204431P1	Support. (Used with Q505 and Q506).
12	4029974P1	Transistor insulator. (Used with Q506).
13	4031291P1	Transistor insulator. (Used ith Q501 and Q502).
14	4034215P1	Bushing. (Used with Q501 and Q502).
15	4024225P1	Flat washer. (Used with Q501 and Q502).
16	N405P9C13	Lockwasher. No. 10. (Used with Q501 and Q502).
17	4032596P1	Nut. No. 10-32. (Used with Q501 and Q502).
18	4036835P1	Solder terminal. (Used with Q501 and Q502).
19	19A115221P3	Mica washer. (Used with Q501 and Q502).
20	7160861P4	Speed nut. (Used with power supply cover).
21	19A116023P2	Insulator. (Used with Q505).
22	19A115222P3	Insulator, bushing. (Used with Q505).

PRODUCTION CHANGES

Changes in the equipment to improve performance or to simplify circuits are identified by a "Revision Letter", which is stamped after the model number of the unit. The revision stamped on the unit includes all previous revisions. Refer to the Parts List for descriptions of parts affected by these revisions.

REV. A - To protect the 10-volt regulator against reverse polarity. Added CR1 to to the 10-volt regulator board A502.

REV. B - To reduce power supply switching spike from primary power supply leads. Added C512.

REV. C - To improve operation of the 10-volt regulator. Deleted Q1 and added R8.

REV. D - To improve reliability of 10-volt regulator. Changed Q505 and 10-volt regulator circuit.

REV. E - To improve operation of 10-volt regulator A501. Changed R8.

REV. F - To incorporate different transistor. Changed Q505.

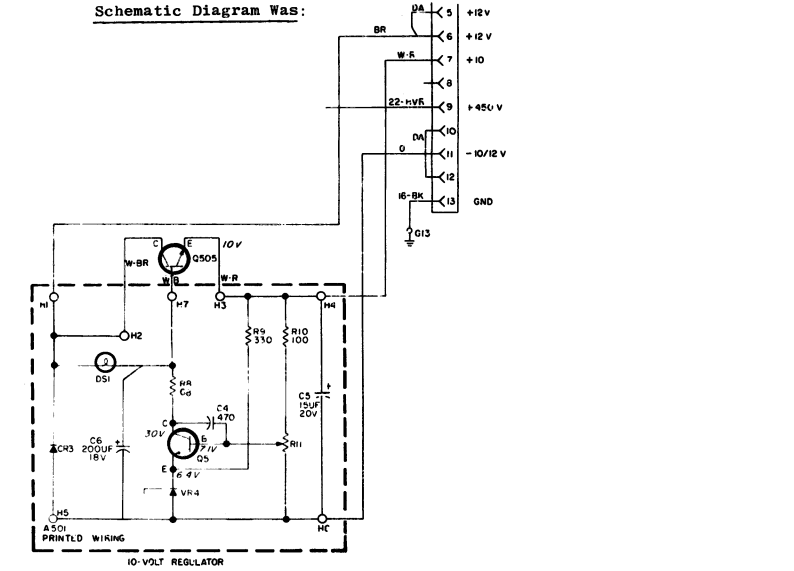
REV. G - To reduce alternator noise to the receiver. Changed 10-volt regulator board A501.

REV. H - To provide protection against reverse polarity. Deleted CR2 and added CR3 to 10-volt regulator A501.

REV. J - To incorporate different transistor. Changed Q505.

REV. K - To provide a more reliable connection to the 10-volt regulator transistor. Changed Q505.

REV. L - To incorporate a transistor switch on the 10-volt regulator board for receiver muting. Added C4, R5, R6, Q2 and new regulator board.



REV. M - To improve receiver muting when operating -20% battery voltage. Changed R6.

REV. N - To reduce residual spike deviation. Added C513 and C514.

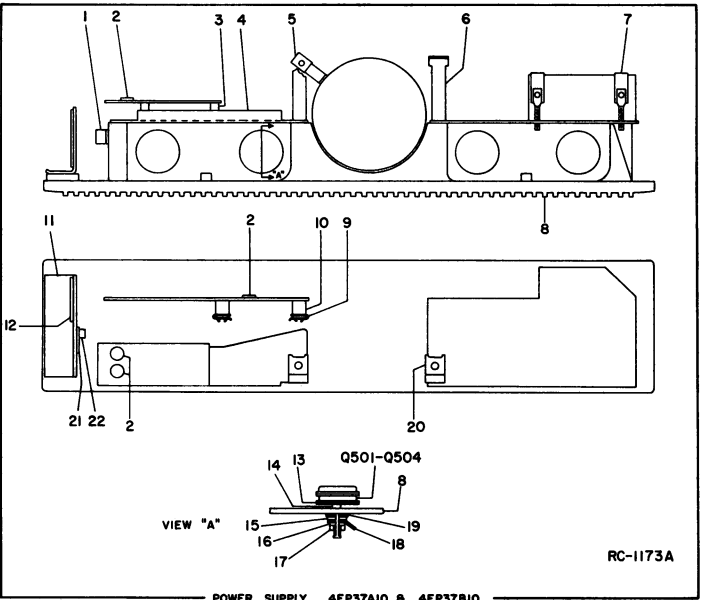
REV. P - To improve electrical performance and mechanical construction. Added standoffs. Changed DA wire from between TB5-32 and TB5-40 to SF22-W.

REV. R - To improve procurement. Deleted DS1. Added R12.

REV. S - To improve filtering. Changed connection of C513 and C514.

REV. T - Provide reverse polarity protection. Add CR511, F501 and TB501.

REV. U - To improve reliability of 20-volt regulator circuit. Changed Q507. Improve reliability of 10-volt regulator. Changed Q1 and Q2.



ORDERING SERVICE PARTS

Each component appearing on the schematic diagram is identified by a symbol number, to simplify locating it in the parts list. Each component is listed by symbol number, followed by its description and GE Part Number.

Service parts may be obtained from Authorized GE Communication Equipment Service Stations or through any GE Radio Communication Equipment Sales Office. When ordering a part, be sure to give:

1. GE Part Number for component
2. Description of part
3. Model number of equipment
4. Revision letter stamped on unit

These instructions do not purport to cover all details or variations in equipment nor to provide for every possible contingency to be met in connection with installation, operation or maintenance.

Should further information be desired, or should particular problems arise which are not covered sufficiently for the purchaser's purposes, contact the nearest Radio Communication Equipment Sales Office of the General Electric Company.

MAINTENANCE MANUAL

LBI-3503

MOBILE RADIO DEPARTMENT
GENERAL ELECTRIC COMPANY • LYNCHBURG, VIRGINIA 24502



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