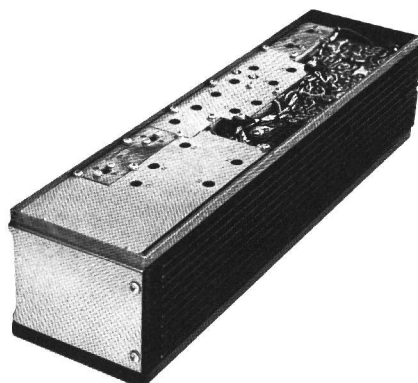


# MASTR

## Progress Line

25—50 MHz RECEIVER MODELS 4ER39C28—45



### SPECIFICATIONS \*

FCC Filing Designation

#### ER-39-C

Frequency Range

25— 50 MHz

Audio Output

5 watts at less than 5% distortion

Sensitivity

12-dB SINAD (EIA Method)  
20-dB Quieting Method

0.25  $\mu$ V  
0.35  $\mu$ V

Selectivity

EIA Two-Signal Method  
20-dB Quieting Method

-85 dB (adjacent channel, 20 kHz channels)  
-100 dB at  $\pm 15$  kHz

Spurious Response

-100 dB

First Oscillator Stability

$\pm 0.0005\%$  ( $-30^{\circ}\text{C}$  to  $+60^{\circ}\text{C}$ )

Modulation Acceptance

$\pm 7$  kHz (narrow-band)

Squelch Sensitivity

Critical Squelch  
Maximum Squelch

0.15  $\mu$ V  
Greater than 20 dB quieting (less than  
1.5  $\mu$ V)

Intermodulation (EIA)

-60 dB

Maximum Frequency Separation

0.4%

Frequency Response

+1 and -8 dB of a standard 6-dB per oc-  
tave de-emphasis curve from 300 to  
3000 Hz (1000-Hz reference)

\*These specifications are intended primarily for the use of the serviceman. Refer to the appropriate Specification Sheet for the complete specifications.

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#### WARNING

No one should be permitted to handle any portion of the equipment that is supplied with high voltage; or to connect any external apparatus to the units while the units are supplied with power.

KEEP AWAY FROM LIVE CIRCUITS

## DESCRIPTION

General Electric MASTR Progress Line Receiver Type ER-39-C is a double conversion, superheterodyne FM receiver designed for operation on the 25-50 megahertz band.

The receiver is of single-unit construction and is completely housed in a copper-plated aluminum casting for maximum shielding and rigidity. The top compartment of the casting contains the RF, oscillator, converter, and 1st low IF amplifier, and noise blanker. The bottom portion of the casting contains the audio-squelch board and the optional Channel Guard board.

## CIRCUIT ANALYSIS

The MASTR Progress Line Receiver is completely transistorized, using silicon transistors throughout for added reliability. Input leads to the receiver are individually filtered by the 20-pin feed-through by-pass connector J443. A regulated +10 volts is used for all receiver stages except the audio PA stage which operates from the 12-volt system supply.

Centralized metering jack J442 is provided for use with General Electric Test Set Model 4EX3A10 or 4EX8K10, 11 for ease of alignment and servicing. The Test Set meters the noise blanker, multiplier, and limiter stages as well as the discriminator, and regulated 10 volts.

### RF AMPLIFIERS (A341 & A344)

1st RF Amplifier (A341) consists of two high-Q helical resonators and an RF amplifier stage (Q1). The RF signal from the antenna is coupled by RF cable W441 to a tap on L341/L343/L345. The tap is positioned to insure the proper impedance match to the antenna. RF energy is coupled through the two coils by an opening in the shield wall to the base of 1st RF Amplifier Q1. The coils are tuned to the incoming frequency by air trimmer capacitors C341 and C342.

The output of Q1 is coupled through two or four tuned circuits to the base of the 2nd RF Amplifier (A344-Q1).

The output of the 2nd RF Amplifier (A344) is coupled through three tuned circuits to the base of 1st Mixer A369-Q2.

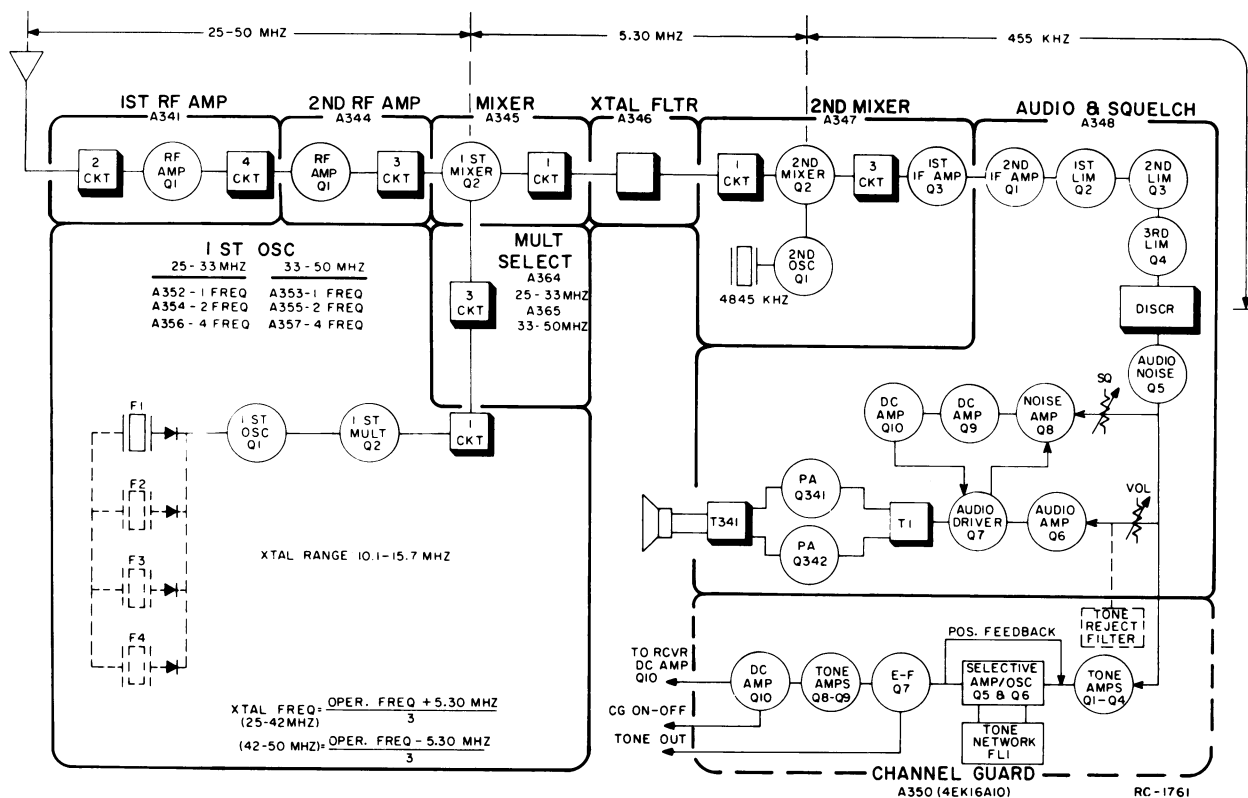


Figure 1 - Receiver Block Diagram

## 1ST OSCILLATOR AND MULTIPLIER (A352-A357)

The receiver 1st oscillator operates in a transistorized Colpitts oscillator circuit. The oscillator crystal operates in a fundamental mode at a frequency of approximately 10 to 15 megahertz. The crystal is cut to provide temperature compensation at the high end of the temperature range and is thermistor compensated at low temperatures. This provides  $\pm 0.0005\%$  frequency stability as soon as the receiver is energized — without the warm-up time required by crystal ovens or warmers.

In single frequency receivers, bias for the oscillator is obtained by a jumper from H1 to H2 on the oscillator board.

In multi-frequency receivers, a diode is connected in series with the crystal, and up to three additional crystal circuits can be added. The 10-volt jumper is removed and the proper frequency is selected by switching the desired crystal circuit to +10 volts by means of a frequency selector switch on the control unit.

Switching the +10 volts to the crystal circuit forward biases the diode and reduces its impedance. This applies the crystal frequency to the base of oscillator transistor Q1. Feedback for the oscillator is developed across C21/C22. The output is coupled to the base of 1st multiplier Q2.

The output of the 1st multiplier (tripler Q2) is transformer-coupled (T3/T4) to multiplier selectivity assembly A364/A365. The multiplier tank is tuned to three times the crystal frequency. The stage is metered at centralized metering jack J442-4 through metering network CR1, R1, C5 and C6.

## MULTIPLIER SELECTIVITY ASSEMBLY (A364/A365)

Following the 1st multiplier tank (T3/T4) are two additional L-C tuned circuits (A364/A365-L1, L2 and L3. Capacitor C12/C16 couples the multiplier selectivity output to the base of the first mixer.

## 1ST MIXER (A369) AND CRYSTAL FILTER (A346)

The RF signal from the RF amplifier and the injection voltage from the 1st multiplier are applied to the base of 1st mixer A345-Q2. The mixer collector tank (L2 and C3) is tuned to 5.3 megahertz and provides impedance matching to the high IF crystal filter.

A highly selective crystal filter (A346) following the 1st mixer provides the major selectivity for the receiver. The output of the filter is fed through impedance matching transformer A347-T1 to the base of the 2nd mixer.

## 2ND OSCILLATOR, 2ND MIXER AND 1ST LO IF AMPLIFIER (A347)

A347-Q2 operates in a Colpitts oscillator circuit, with feedback supplied through C4. The oscillator low-side injection voltage (4845 kHz) is applied to the base of the 2nd mixer.

The High IF signal from the filter and the injection voltage from the 2nd oscillator is applied to the base of 2nd mixer Q2. The 455 kHz mixer output is applied to three tuned low IF circuits, L1, L2 and L3. These tuned circuits are required for shaping the nose of the IF waveform, and for rejecting any undesired output frequencies from the 2nd mixer.

The low IF signal is applied to the base of 1st low IF amplifier A347-Q3. The output of A347-Q3 is R-C coupled to the base of the 2nd low IF amplifier.

## 2ND LO IF AMPLIFIER AND LIMITERS (A348)

Additional amplification of the low IF signal going to the limiter stages is provided by 2nd low IF amplifier A318-Q1. This stage is metered at J442-2 through a metering network consisting of C19, CR3 and R25.

Following the 2nd low IF amplifier are three R-C coupled limiter stages (A348-Q2, Q3 and Q4). The 1st limiter is metered at J442-3 through metering network C20, CR4 and R26.

## DISCRIMINATOR (A348)

The limiter output is applied to a Foster-Seely type discriminator, where diodes CR1 and CR2 rectify the 455-kHz signal to recover the audio. The discriminator is metered at J442-10 through metering network C16 and R23.

## AUDIO - NOISE AMPLIFIER (A348)

The discriminator output is coupled through a low-pass filter (C16, C18, R21 and R22) to the base of audio-noise amplifier Q5. The filter removes any 455-kHz signal remaining in the discriminator output. Q5 operates as an emitter-follower to match the discriminator impedance to the VOLUME control, SQUELCH control, and Channel Guard input. The stage also provides power gain.

## AUDIO AMPLIFIERS (A348)

Any audio present in the incoming signal is coupled from the emitter of Q5 through the VOLUME control and a de-emphasis network to the base of audio amplifier Q6. The de-emphasis network consists of C22, C23, R30 and R31.



Audio driver Q7 follows the audio amplifier. The audio output of Q7 is coupled through transformer T1 to provide phase inversion for the push-pull audio PA stage.

Q341 and Q342 operate as a push-pull, class AB audio PA stage. The PA output is coupled through audio transformer T341 to the loudspeaker. The yellow and white tertiary windings of T341 supply balanced feedback to the collector of Q7. The feedback winding minimizes distortion and prevents the pick-up of external electrical noise.

The PA stage provides a 5-watt output at less than 5% distortion into a 3.5-ohm load at the receiver output terminals (3.2-ohms at the Control Unit). Base bias for the PA stage and the elimination of crossover distortion is controlled by bias adjust potentiometer R43. The potentiometer is set at the factory as shown in STEP 1 of the receiver Test Procedure.

#### NOTE

Do not adjust bias adjust potentiometer R43 unless PA transistors Q341 and Q342 have been replaced.

Audio high and low are also present at centralized metering jack J442, and can be used as shown in STEP 1 of the Test Procedure.

#### SQUELCH (A348)

Noise from the audio-noise amplifier operates the squelch circuit. With no carrier present in the receiver, this noise is coupled to the base of noise amplifier Q8 through a high-pass filter which attenuates frequencies below 3 kHz. The filter consists of C30, C31 and R45, as well as C34 and L3 in the collector circuit of Q8. The gain of Q8 is determined by the Squelch control, which varies the bias on the base of Q8. Thermistor RT2 keeps the critical squelch constant over wide variations in temperature.

The output of noise amplifier Q8 is rectified by diodes CR5 and CR6, and filtered by C36 and C37 to produce a negative DC voltage. This DC voltage is applied to the base of DC amplifier Q9, turning it off. When turned off, the collector voltage of Q9 rises to approximately 8 volts, turning on DC amplifier Q10. When conducting, the collector voltage of Q10 drops to almost ground potential, which removes the base bias to audio amplifier Q6 and audio driver Q7, turning them off.

When the receiver is quieted by a sig-

nal (unsquelled), the noise in the receiver is reduced, turning DC amplifier Q9 on and DC amplifier Q10 off. This allows the audio stages to conduct so that sound is heard in the speaker. A network composed of C38, CR7 and R62 slows down the switching action of Q10, preventing an obnoxious "thump" from being heard in the speaker.

Resistor R53 connects from the emitter of audio driver Q7 to the emitter of noise amplifier Q8, providing a hysteresis loop in the squelch circuit. When a weak signal opens the squelch, the signal level may be reduced by 4 to 6 dB without the squelch closing. This limits squelch "flutter" or "picket-fence" operation.

With audio driver Q7 conducting, a positive voltage through R53 helps to reduce the gain of noise amplifier Q8. This positive feedback provides a quick, positive switching action in the squelch circuit. When the receiver squelches, audio driver Q7 turns off and its emitter potential drops to zero. This reduces the DC feedback through R53 to the emitter of noise amplifier Q8. Reducing the feedback causes Q8 to conduct harder, turning the audio stages off quickly.

Keying the transmitter removes the +10 volts from J19, turning off DC amplifier Q9 and turning on Q10 to mute the receiver.

#### NOISE BLANKER (A370/A372 - Figure 2)

An RF signal and noise pulse from the antenna is fed simultaneously to the Noise Blanker 1st RF Amplifier and the receiver 1st RF amplifier sections. The signal and noise is transformer coupled through T1/T2/T3 to the base of the first of two RF amplifier stages. The amplifier stages (Q1, Q2) raise the level of the noise pulse which is coupled through T10/T11/T12 and L10 to the base of the pulse detector Q3. A metering network consisting of R22, C21, C17 and R2 permits the blanker to be metered at centralized metering jack J442-11.

Base bias for the pulse detector is established by R9 and CR1. CR1 is normally conducting, which keeps Q3 in a barely conducting state. A noise pulse applied to the base of Q3 causes it to conduct heavily. This results in a negative pulse at the output (collector) of Q3. Following Q3 is a low-pass RF filter consisting of C18, C22 and L5.

The output of the filter is fed to the base of pulse amplifier Q4. This stage is biased by CR3, R12 and R13 so that it is just conducting. The negative-going pulse from the pulse detector cuts CR3 off, which biases Q4 on, and a positive pulse appears at the output of pulse amplifier Q4.

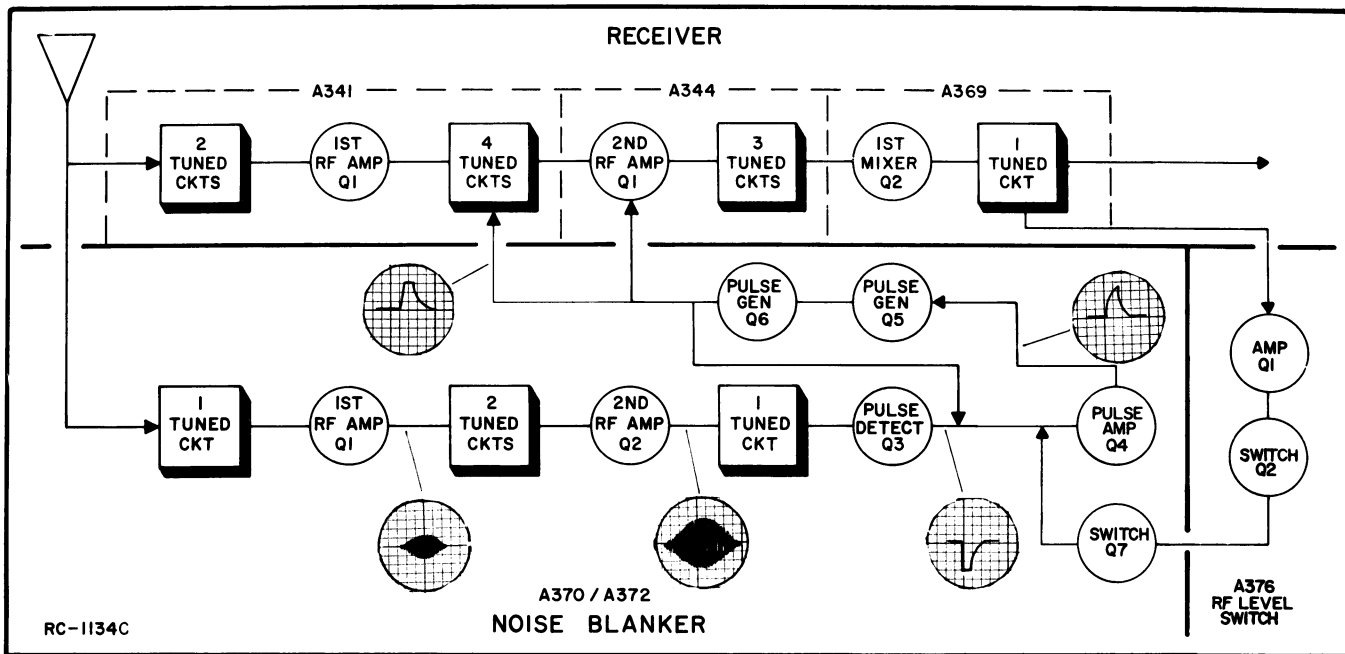


Figure 2 - Noise Blanker Block Diagram

Q5 and Q6 form part of the one-shot multivibrator circuit. Bias voltage through R17 keeps Q5 normally turned on. The positive voltage at the collector of Q5 keeps Q6 turned off. The positive-going pulse from the pulse amplifier (Q4) is fed to the base of Q5, cutting the stage off. As Q5 cuts off, Q6 is turned on; and the output is an 8-volt, 12 to 18 microsecond positive-going blanking pulse. The positive blanking pulse is fed to the emitter of 2nd RF Amplifier A344-Q1 and coil L2. The pulse cuts off Q1 and shunts L2 for the duration of the noise pulse.

The positive blanking pulse to the emitter of the 2nd RF amplifier A344-Q1 is controlled by the RF Level Shut-Off Switch A376. The output of the 1st Mixer is fed through a low-pass filter network in the RF level switch circuit to the base of the high IF level amplifier Q1. When the antenna signal input level is approximately 500-5000 microvolts, the high IF level output of Q1 is sufficient to turn ON level-sensitive switch Q2. The output of Q2 is filtered through C7, C8, L2 and then turns ON the Noise Blanker (A370/A372) switch Q7. The conduction of Q7 changes the bias to the 1st Pulse Amplifier Q4 and shorts the blanking pulse to ground.

The high IF output level (amplified by Q1) is not sufficient to turn Q2 ON when the antenna signal input is below the 500 to 5000 microvolt range. As a result, Q7 does not turn ON, and the positive blanking pulse is fed to the emitter of the 2nd RF Amplifier A344-Q1.

The blanking pulse width is determined

by R17 and C27. Diode CR6 keeps the output pulse a square wave. CR5 prevents oscillation at temperature extremes.

At the same time that the blanking pulse is applied to the receiver, samples of the pulse are fed to automatic repetition rate switch C30, C24, CR4, R13, R14 and R20. The pulse sample is coupled through C30 and is rectified by CR4. The rectified voltage charges C24 which then discharges through R13 and R14 to reverse bias CR3 and turn off pulse amplifier Q4. The components (C23, C24, R13, and R14) are selected so that the output pulses cannot blank the receiver continuously and prevent the desired signal from being heard.

The circuit time constant disables the blanking function whenever sinusoidal intermodulation signals produce beat frequencies of two kHz or higher. However, continuous impulse noise will not disable the blanker until a repetition rate of approximately 10 to 20 kHz is exceeded. The higher impulse noise repetition rate is provided by C23 which bypasses CR3 with the negative-going impulse noise. This turns on Q4 and allows the blanker to function.

As the noise signal from the antenna is applied to the Noise Blanker, the RF signal is applied to the receiver RF amplifier (A341). The six tuned circuits in the receiver front end provide a time delay for the RF signal, which enables the blanking pulse from the noise blanker to cut off the RF amplifier in the receiver before the noise pulse can get there.

The blanker may be disabled by shorting

across the yellow dot on the noise blanker printed wiring board. Refer to the Noise Blanker Troubleshooting Procedure, as listed in the Table of Contents, for a complete performance check.

#### CHANNEL GUARD

Channel Guard Board Model 4EK16A10 is a fully transistorized encoder-decoder for use with MASTR Professional Series mobile and station combinations. The tone frequencies are controlled by plug-in tone networks that are made with precision components for excellent stability and reliability. The tone frequencies range from 71.9 to 203.5 Hz.

##### Encoder (A350)

Keying the transmitter removes the receiver mute +10 volts, and forward biases feedback control diode CR5, causing it to conduct. When conducting, the diode shunts R39, R35 and C19). This provides the necessary gain to the base of Q5 to permit oscillation.

The encoder tone is provided by selective amp-oscillator transistors Q5 and Q6 which oscillate at a frequency determined by the tone network. Negative feedback applied through the tone network to the base of Q5 prevents any gain in the stage except at the desired encode frequency.

Starting network R45, C21, C22 and CR6 provide an extremely fast starting time for the encoder tone. Keying the transmitter removes the receiver mute +10 volts, causing a pulse to be applied to the base of Q6 to quickly start the oscillator. Thermistor-resistor combination R32 and RT1 provides temperature compensation for the oscillator output. Limiter diodes CR3 and CR4 keep the tone amplitude constant.

Emitter-follower Q7 follows the oscillator circuit. The encoder tone is taken from the emitter of Q7 and applied to the transmitter.

##### Decoder (A350)

The decoder function is designed to eliminate all calls that are not tone coded for the Channel Guard frequency. As long as the CHANNEL GUARD-OFF switch on the control unit is left in the CHANNEL GUARD position, all signals are locked out except those from transmitters that are continuously tone coded for positive identification by the receiver.

Placing the CHANNEL GUARD-OFF switch in the OFF position instantly disables the Channel Guard operation so that all calls on the channel can be heard. When the hook-switch option is used, lifting the microphone from its hanger disables the Channel Guard Circuit.

Audio, tone and noise are taken from the emitter of the receiver audio-noise amplifier A348-Q5 and is fed through A350-J1 to four tone amplifier and bandpass filter circuits. The filters remove the audio and high-frequency noise from the signal, and the tone amplifiers provide sufficient gain to insure clipping by limiter diodes CR1 and CR2. The clipping action eliminates variation in the squelch performance due to changes in tone deviation. The signal is then applied to selective amplifiers Q5 and Q6 which amplify only the tone determined by the tone network.

The output of the selective amplifier is applied through emitter-follower Q7 to the high gain, broad-band tone amplifiers Q8 and Q9. The output of Q9 is rectified by detector diodes CR7 and CR8, and the resulting negative DC voltage controls the squelch gate. Q8 is normally biased for low gain. When the tone is detected by CR7 and CR8, feedback is provided through R54 to quickly change the bias on Q8 for full gain. This ensures a more positive "un-squelching" action.

Squelch gate diode CR9 is normally forward biased by a positive DC voltage (approximately 1.5 volts) fed through R58. The forward bias causes CR9 to conduct, feeding a DC voltage to the base of DC amplifier A348-Q10 in the receiver. This removes the bias on the receiver audio stages and holds them off.

When the proper tone is applied to the decoder, the negative DC voltage from the detector diodes back-biases squelch gate diode CR9 and cuts off the positive bias to the receiver DC amplifier A348-Q10. However, the receiver noise squelch circuit continues to operate until a carrier quiets the receiver.

Placing the CHANNEL GUARD - OFF switch in the OFF position (or removing the microphone from its hookswitch) removes the ground to the base of the decoder DC switch (Q10), causing it to conduct. This back-biases squelch control diode CR9 and cuts off the positive bias to the receiver DC amplifier (A348-Q10). The receiver noise squelch circuit continues to operate until a carrier quiets the receiver.

A tone rejection filter connected in parallel with A348-J12 (in the receiver) bypasses any incoming tone to ground. This attenuates the tone level reaching the receiver audio circuits. The filter is composed of C26, C27, C28, C29, L1 and R59.

An optional tone reject filter (A402) that is identical to the filter described above is available for use in two-way radios with transmitter Channel Guard only.

## MAINTENANCE

### DISASSEMBLY

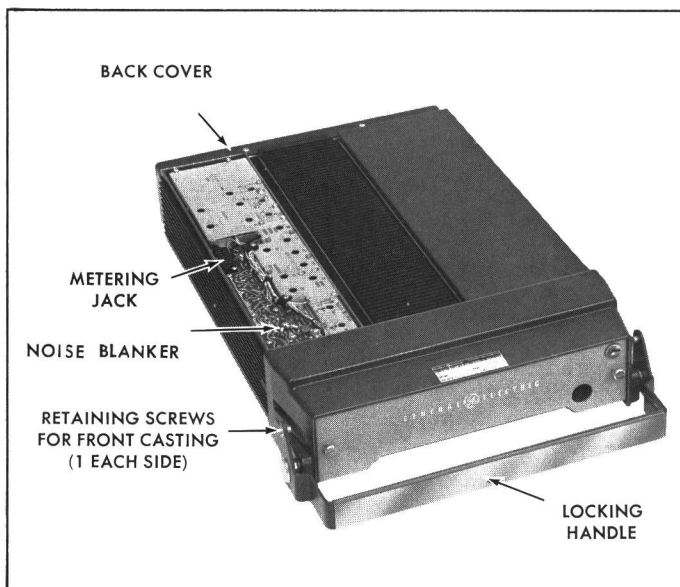


Figure 3 - Removing Top Cover

To service the receiver from the top--

1. Pull locking handle down and pull radio about one inch out of mounting frame.
2. Pry up cover at rear of receiver.
3. Slide cover back and lift off.

To remove the receiver from the system frame--

1. Loosen the two Phillips-head retaining screws in front casting (see Figure 3), and pull casting away from system frame.
2. Remove the four screws in the back cover.
3. Remove the two screws holding the receiver at each end of the system frame.
4. Disconnect the antenna jack and the 20-pin connector from the front of the receiver, and slide the unit out of the system frame.

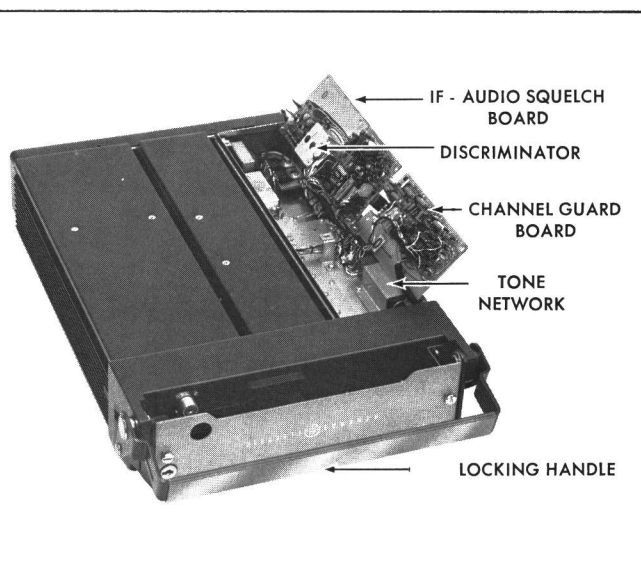


Figure 4 - Removing Bottom Cover

To service the receiver from the bottom--

1. Pull locking handle down. Pull radio out of mounting frame.
2. Remove screws in bottom cover. Pry up cover at back of receiver.
3. Slide cover back and lift off.



## FRONT END ALIGNMENT

### EQUIPMENT REQUIRED

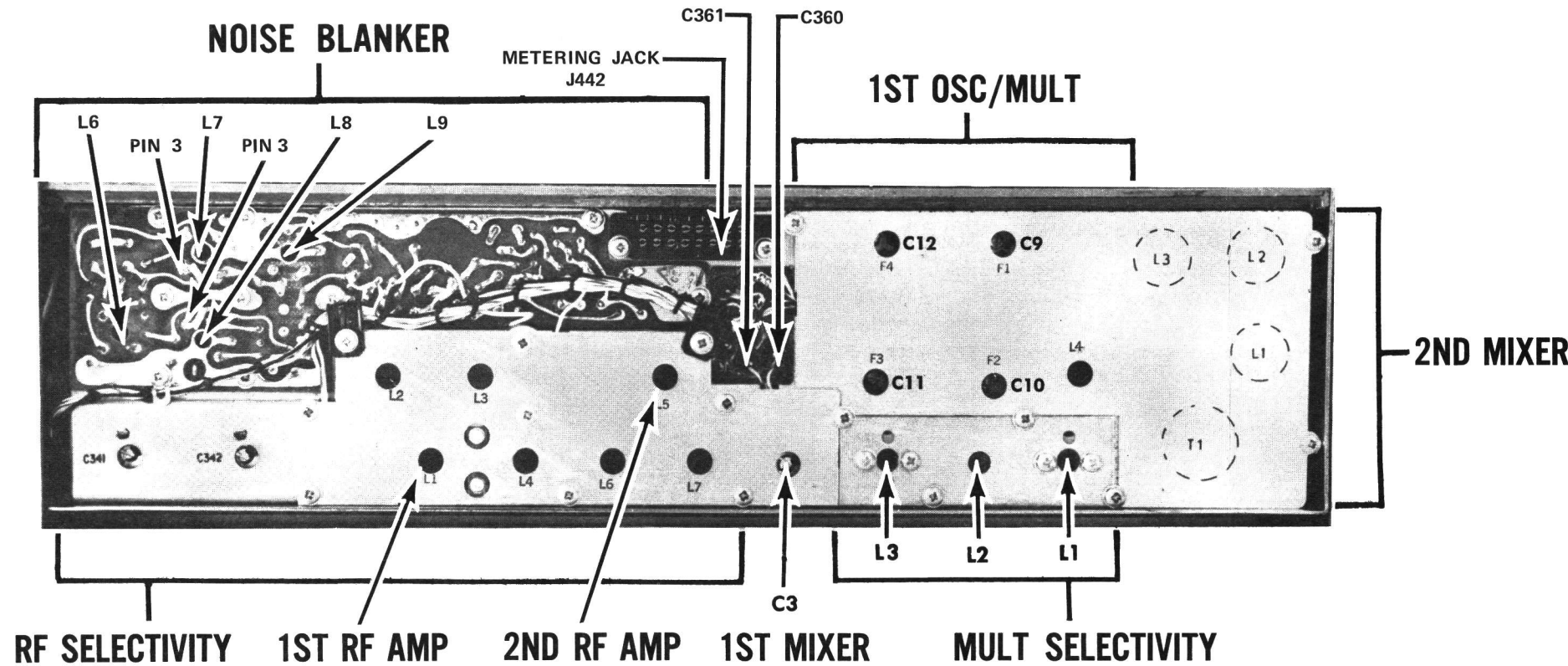
- GE Test Set Models 4EX3A10, 4EX8K10, 11 (or 20,000 ohms-per-volt Multimeter with a 1-volt scale).
- A 455 kHz and 25-50 MHz signal source. Connect a one-inch piece of insulated wire no larger than .065-inch diameter to generator output probe.

### PRELIMINARY CHECKS AND ADJUSTMENTS

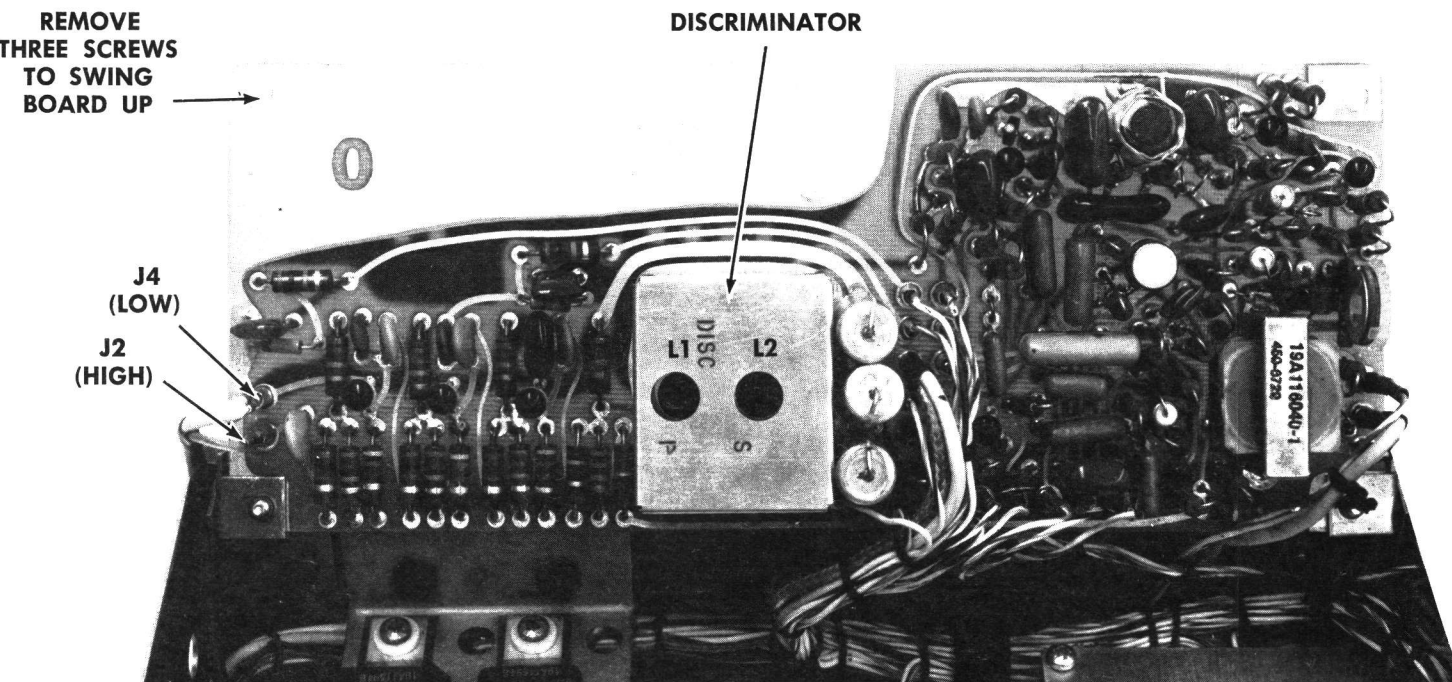
- Connect Test Set to Receiver Centralized Metering Jack J442 and set meter sensitivity switch to the TEST 1 position (or 1-volt position on 4EX8K10, 11).
- With Test Set in Position J, check for regulated +10 volts. If using Multimeter, measure from C360 to C361.
- If using Multimeter, connect the positive lead to J442-16 (Ground).
- Disable Channel Guard.

### ALIGNMENT PROCEDURE

STEP	METERING POSITION		TUNING CONTROL	METER READING	PROCEDURE
	GE Test Set	Multimeter – at J442			
OSCILLATOR/MULTIPLIER					
1.	D (MULT-1)	Pin 4	L4 (on 1st OSC/MULT) and L1, L2 (on MULT SELECTIVITY)	See Procedure	Tune L4 on 1st OSC/MULT and L1 on MULT SELECTIVITY for maximum meter reading. Next tune L2 for minimum meter reading. Then tune L3 for maximum meter reading. Repeat step 1, changing voltage scale if necessary.
RF AMPLIFIER & SELECTIVITY					
2.	A (DISC)	Pin 10		Zero	Apply an on-frequency signal adjacent to L7. Adjust the signal generator for discriminator zero.
3.	B (2nd IF Amp)	Pin 2	L1 (1st RF Amp), L6, L7, C341 and C342 (RF SELECTIVITY)	Maximum	Apply an on-frequency signal to the antenna jack, keeping below saturation. Tune L1 thru L7, C341, and C342 for maximum meter reading.
4.	"	"	L4 (1st OSC/MULT) and L1 and L2 (MULT SELECTIVITY)	Maximum	Apply an on-frequency signal as above, keeping below saturation. Tune L4 on 1st OSC/MULT and L1, L2 and L3 on MULT SELECTIVITY for maximum meter reading.
FREQUENCY ADJUSTMENT					
5.	A (DISC)	Pin 10	C9 on 1st OSC (C10, C11 or C12 for multi-frequency)	Zero	Apply an on-frequency signal to the antenna jack. Tune C9 for zero discriminator reading. In multi-frequency units, tune C10, C11 or C12 as required.  —————NOTE—————  For proper frequency control of the receiver, it is recommended that all frequency adjustments be made when the equipment is at a temperature of approximately 75°F. In no case should frequency adjustments be made when the equipment is outside the temperature range of 50° to 90° F.



## IF-AUDIO & SQUELCH



## COMPLETE RECEIVER & NOISE BLANKER ALIGNMENT

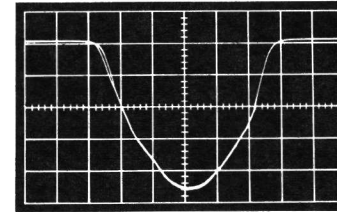
### EQUIPMENT REQUIRED

- GE Test Set Models 4EX3A10, 4EX8K10, 11 (or 20,000 ohms-per-volt Multimeter with a 1-volt scale).
- A 455 kHz signal source (GE Test Set Model 4EX7A10) and 25-50 MHz signal source. Connect a one-inch piece of insulated wire no larger than .065-inch diameter to generator output probe.

### PRELIMINARY CHECKS AND ADJUSTMENTS

- Connect Test Set to Receiver Centralized Metering Jack J442, and set meter sensitivity switch to the TEST 1 position (or 1-volt position on 4EX8K10, 11).
- For large changes in frequency or a badly mis-aligned receiver, set crystal trimmer C9 to mid-capacity. In multi-frequency receivers, set C10, C11 or C12 to mid-capacity as required. Where the maximum frequency spacing is less than 100 kHz, align the unit on channel F1. If the frequency spacing is greater than 100 kHz, align the receiver on the center frequency.
- With Test Set in Position J, check for regulated +10 volts. If using Multimeter, measure from C360 to C361.
- If using Multimeter, connect the positive lead to J442-16 (Ground).
- For large changes in frequency or a badly mis-aligned receiver, adjust all slugs on the Noise Blanker to the bottom of the coil form (closest to printed wiring board).
- Disable the Channel Guard.

### ALIGNMENT PROCEDURE

STEP	METERING POSITION		TUNING CONTROL	METER READING	PROCEDURE
	GE Test Set	Multimeter - at J442			
DISCRIMINATOR & OSCILLATOR					
1.	A (DISC)	Pin 10	L1 and L2 (on IF-AUDIO SQUELCH board)	Zero	Remove three screws and swing open the IF-AUDIO & SQUELCH board. Adjust L1 (disc primary) 1/2 turn counterclockwise from the bottom of coil. Next, apply a 455-kHz signal to J2 and J4 and adjust L2 (disc secondary) for zero meter reading.
2.	A (DISC)	Pin 10		See Procedure	Alternately apply a 450-kHz and 460-kHz signal and check for readings of at least 0.3 volt, but not more than 0.5 volt on GE Test Set. Both readings must be within .05 volt. Do not attempt to balance readings any closer than 0.05 V.
3.	D (MULT-1)	Pin 4	L4 (on 1st OSC/MULT) and L1, L2 & L3 (on MULT SELECTIVITY)	See Procedure	Tune L4 on 1st OSC/MULT and L1 on MULT SELECTIVITY for maximum meter reading. Tune L2 for minimum meter reading. Change voltage scale if necessary. Then tune L3 for maximum meter reading. Repeat step 3.
RF AMPLIFIERS & SELECTIVITY					
4.	A (DISC)	Pin 10		Zero	Apply an on-frequency signal adjacent to L6 (RF SELECTIVITY). Adjust the signal generator for discriminator zero.
5.	B 2nd IF AMP	Pin 2	L7, L6, L4, L3 and L2 (RF SELECTIVITY) L5 (2nd RF AMP)	Maximum	Apply an on-frequency signal and tune as shown below, keeping signal below saturation.  Apply Signal Generator Probe To: <div><div>L6 L4 L1 (1st RF AMP)</div><div>Tune: L7 L6 and L5 L4, L3 and L2</div></div>
6.	B 2nd IF AMP	Pin 2	C341, C342 (RF SELECTIVITY) and L1 (1st RF AMP)	Maximum	Apply an on-frequency signal to antenna jack J441. Tune C341, C342 and L1 for maximum meter reading, keeping signal below saturation.
7.	"	"	L7, L6, L4, L3, L2, C342 and C341 (RF SELECTIVITY), L5 (2nd RF AMP), L1 (1st RF AMP)	Maximum	Apply an on-frequency signal as above, keeping below saturation. Tune L7, L6, L5, L4, L3, L2, L1, C342 and C341 for maximum meter reading.
8.	"	"	L3 on MULT SELECTIVITY	Maximum	Apply an on-frequency signal as above, keeping below saturation. Tune L2 and L3 on MULT SELECTIVITY Board for maximum meter reading.
2ND MIXER & LO IF					
The 1st and 2nd mixer, and low IF circuits have been aligned at the factory and will normally require no further adjustment. If adjustment is necessary, use the procedure outlined in STEPS 9, 10, and 11. C3 does not peak, but provides impedance matching for the crystal filter input and should only be tuned when observing IF trace on oscilloscope.					
NOTE Refer to DATAFILE BULLETIN 1000-6 IF Alignment of Two-Way Radio FM Receivers for helpful suggestions on how to determine when IF Alignment is required.					
9.	B (2nd IF AMP)	Pin 2	L3, L2, L1, T1 (2nd Mixer)	Maximum	Apply on-frequency, unmodulated signal and tune L3, L2, L1, and T1 for maximum meter reading, keeping signal below saturation.
10.			A347-L3, L2, L1, T1 (2nd Mixer) 		Connect scope, signal generator, and detector as shown in Figure 5. Set signal generator level for 30-50 µV and modulate with 10 kHz at 20 Hz. With detector at the collector of Q3 (2nd mixer board output), tune for double trace as shown on scope pattern.
11.	A (DISC)	Pin 10		See Procedure	Check to see that discriminator idling voltage is within ±.05 volt of zero with no signal applied. Check to see that modulation acceptance bandwidth is between 7 and 9 kHz.

### ALIGNMENT PROCEDURE

METERING POSITION			TUNING CONTROL	METER READING	PROCEDURE					
STEP	GE Test Set	Multimeter - at J442								
NOISE BLANKER										
12.	H (BLANKER)	Pin 11 (-) and Pin 16 (+)	L9, L8, L7 and L6 on NOISE BLANKER	Maximum	Apply a signal according to the following table:					
					<table><tr><th>Receiver operating frequency</th><th>Frequency of applied signal</th></tr><tr><td>25-27 MHz</td><td>4 MHz above operating freq.</td></tr><tr><td>27-33 MHz</td><td>4 MHz below operating freq.</td></tr><tr><td>33-42 MHz</td><td>4 MHz below operating freq.</td></tr><tr><td>42-50 MHz</td><td>4 MHz above operating freq.</td></tr></table> Apply signal generator probe to: Pin 3 of L8 Pin 3 of L7 Antenna Jack  Tune: L9 (2nd peak) L8 (1st peak) 25-33 MHz (L7, 1st peak; L6 2nd peak) 33-50 MHz (L7 and L6; 1st peak)	Receiver operating frequency	Frequency of applied signal	25-27 MHz	4 MHz above operating freq.	27-33 MHz
Receiver operating frequency	Frequency of applied signal									
25-27 MHz	4 MHz above operating freq.									
27-33 MHz	4 MHz below operating freq.									
33-42 MHz	4 MHz below operating freq.									
42-50 MHz	4 MHz above operating freq.									
13.	"	"	"	Maximum	Apply signal on blanker frequency to the antenna jack. Retune L6, L7, L8 and L9 for maximum meter reading.					
14.	"	"	"	0.1 v	Apply a 1,000-microvolt signal on blanker frequency to antenna jack. Reading should be approximately 0.1 volt.					
FREQUENCY ADJUSTMENT										
15.	A (DISC)	Pin 10	C9 on 1st OSC (C10, C11 or C12 for multi-frequency	Zero	Apply an on-frequency signal to the antenna jack. Tune C9 for zero discriminator reading. In multi-frequency units, tune C10, C11 or C12 as required.  NOTE  For proper frequency control of the receiver, it is recommended that all frequency adjustments be made when the equipment is at a temperature of approximately 75°F. In no case should frequency adjustments be made when the equipment is outside the temperature range of 50° to 90°F.					

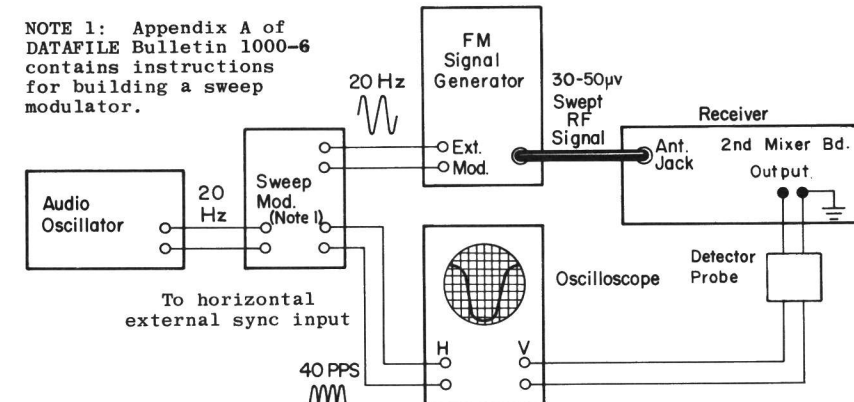


Figure 5 - Test Setup for 20-Hz Double-Trace Sweep Alignment

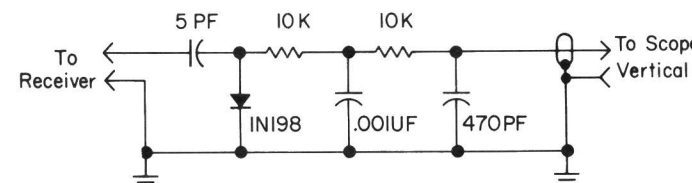


Figure 6 - Detector Probe for Sweep Alignment

## ALIGNMENT PROCEDURE

25—50 MHz MASTR RECEIVER  
MODELS 4ER39C28-45



TEST PROCEDURES

These Test Procedures are designed to help you to service a receiver that is operating---but not properly. The problems encountered could be low power, poor sensitivity, distortion, limiter not operating properly, and low gain. By following the sequence of test steps starting with Step 1, the defect can be quickly localized.

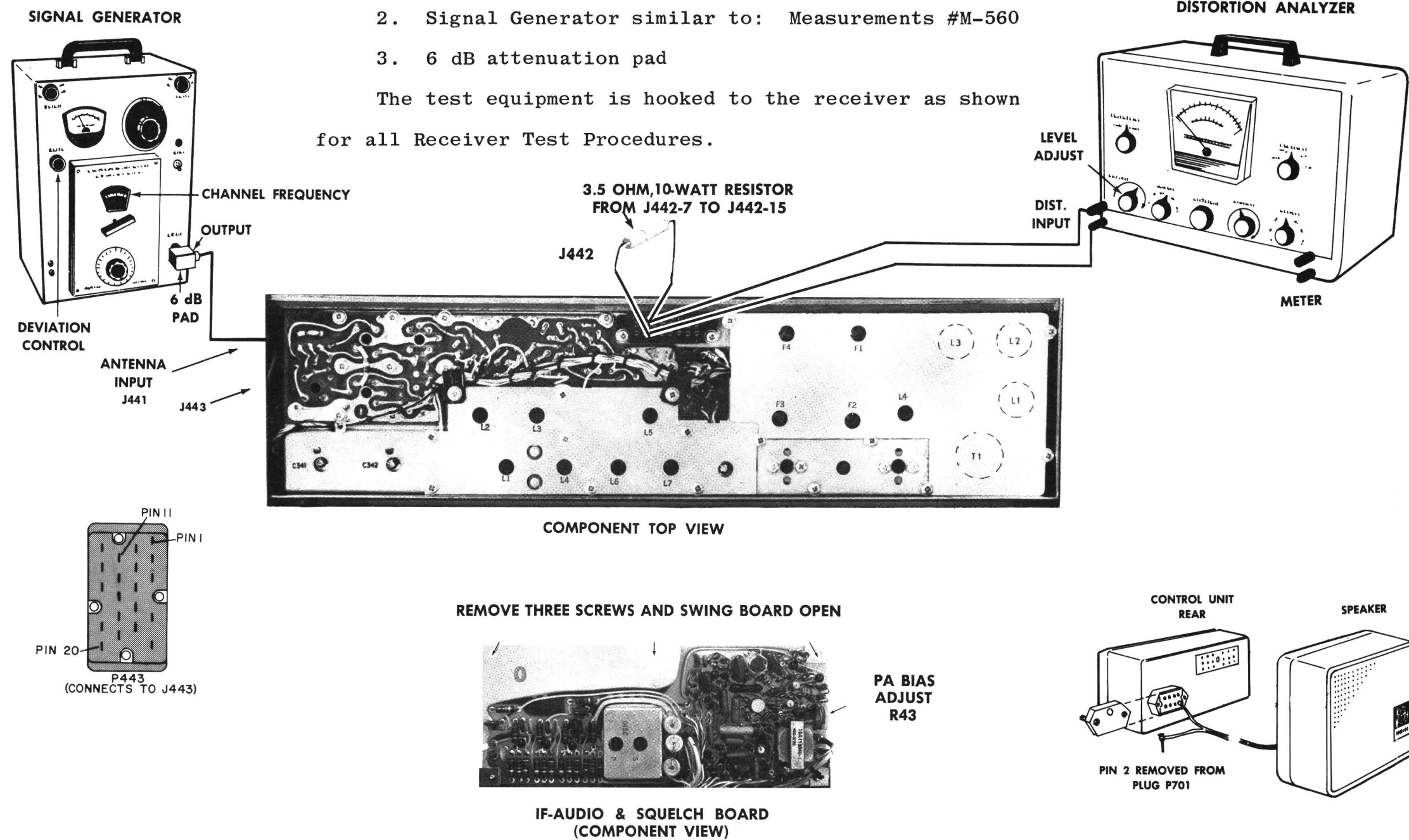
Once the defective stage is pin-pointed, refer to the "Service Check" listed to correct the problem. Additional corrective measures are included in the Troubleshooting Procedure. Before starting with the Receiver Test Procedures, be sure the receiver is tuned and aligned to the proper operating frequency.

TEST EQUIPMENT REQUIRED

for test hookup shown:

- 1. Distortion Analyzer similar to: Heath #1M-12
- 2. Signal Generator similar to: Measurements #M-560
- 3. 6 dB attenuation pad

The test equipment is hooked to the receiver as shown for all Receiver Test Procedures.



STEP 1

AUDIO POWER OUTPUT AND DISTORTION

TEST PROCEDURE

Measure Audio Power Output as follows:

- A. Connect a 1,000-microvolt test signal modulated by 1,000 hertz  $\pm 3.3$  kHz deviation to the antenna jack J441.
- B. With Five-Watt Speaker:

Disconnect speaker lead pin from J701-2 (on rear of Control Unit).

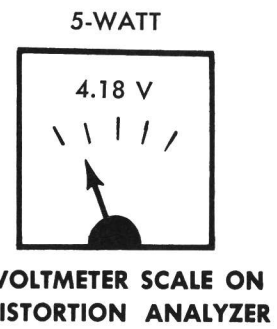
Connect a 3.5-ohm load resistor from J442-15 to J442-7. Connect the Distortion Analyzer input across the resistor as shown.

OR

With Handset:

Lift the handset off of the hookswitch. Connect the Distortion Analyzer input from J442-15 to J442-7.

- C. Set the VOLUME control for five-watt output (4.18 VRMS).
- D. Make distortion measurements according to manufacturer's instructions. Reading should be less than 5%.



SERVICE CHECK

If the distortion is more than 5%, or maximum audio output is less than five watts, make the following checks:

- E. Battery and regulator voltage---low voltage will cause distortion. (Refer to Receiver Schematic Diagram for voltages.)
- F. P.A. Bias Adjust (R43) -- Turn the SQUELCH control fully counterclockwise. Then connect a milliammeter in series with the +12-volt lead at P443-11. With no signal in, adjust R43 for a reading of approximately 20 milliamps. This adjustment should not be necessary unless an output transistor has been replaced.
- G. Audio Gain (Refer to Receiver Troubleshooting Procedure).
- H. Discriminator Alignment (Refer to Receiver Alignment on reverse side of page).

STEP 2

USABLE SENSITIVITY (12 db SINAD)

TEST PROCEDURE

Measure sensitivity of the receiver modulated at the standard test modulation as follows:

- A. Be sure Test Step 1 checks out properly.
- B. Reduce the Signal Generator output from setting in Test Step 1A.
- C. Adjust Distortion Analyzer LEVEL control for a +2 dB reading.
- D. Set CONTROL from LEVEL to DISTORTION reading. Repeat Steps 2B and 2C until difference in reading is 12 dB (+2 dB to -10 dB).
- E. The 12-dB difference (Signal plus Noise and Distortion to noise plus distortion ratio) is "usable" sensitivity level. Reading should be less than 0.25 microvolts with audio output at least 2.5 watts (2.9 volts RMS across the 3.5-ohm receiver load).

SERVICE CHECK

If the sensitivity level is more than 0.25 microvolts, make the following checks:

- F. Alignment of RF stages (Refer to RF Alignment in Receiver Alignment on reverse side of page).
- G. Gain measurements as shown on the Receiver Troubleshooting Procedure.

STEP 3

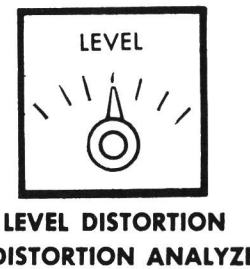
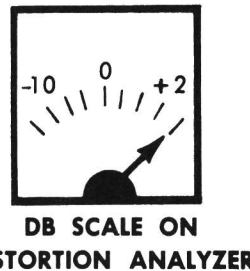
MODULATION ACCEPTANCE BANDWIDTH (IF BANDWIDTH)

TEST PROCEDURE

- A. Be sure Test Steps 1 and 2 check out properly.
- B. Set Signal Generator output for twice the microvolt reading obtained in Test Step 2D.
- C. Increase Signal Generator frequency deviation.
- D. Adjust LEVEL Control for +2 dB.
- E. Set CONTROL from LEVEL to DISTORTION reading. Repeat Steps 3C, 3D and 3E until difference between readings becomes 12 dB (from +2 dB to -10 dB).
- F. Deviation control reading for the 12-dB difference is the Modulation Acceptance Bandwidth of the receiver. It should be more than  $\pm 7$  kHz (but less than  $\pm 9$  kHz).

SERVICE CHECK

If the Modulation Acceptance Bandwidth test does not indicate the proper width, make gain measurements as shown on the Receiver Troubleshooting Procedure.



TROUBLESHOOTING PROCEDURE

Before starting the Noise Blanker troubleshooting procedure, make sure the receiver is operating properly. Align the Noise Blanker as described on the ALIGNMENT PROCEDURE Sheet. Then make the following Troubleshooting checks:

STEP 1—PERFORMANCE CHECK

Equipment Required:

- RF Signal Generator coupled through a 6 db pad.
- Pulse Generator with repetition rate and level controls (similar to General Electric Model 4EX4A10)
- AC VTVM

Procedure:

1. Connect Pulse Generator and RF Signal Generator to receiver antenna jack through a T-connector and connect VTVM to receiver output as shown in Figure 1.

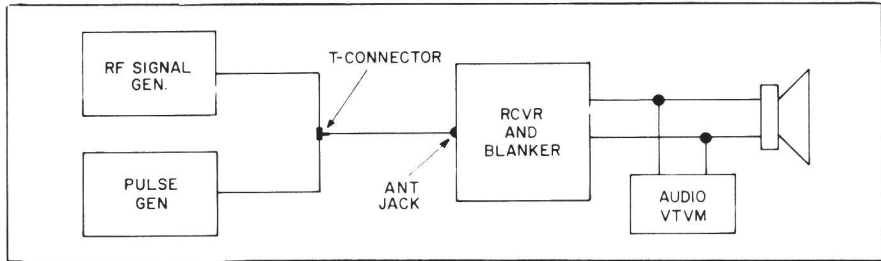


Figure 1 - Equipment Connection Diagram RC-1388

2. Apply an unmodulated RF Signal and check the 20 db quieting sensitivity of the receiver. (Measure with Model 4EX4A10 Pulse Generator connected but turned off).
3. Disable pulse section of the noise blanker by shorting Q4 base to emitter. (A yellow dot is located between the base and emitter connections on solder side of the noise blanker board).
4. Set the pulse generator (Model 4EX4A10) repetition rate to 1500 Hz and adjust the output level control on pulse generator until receiver sensitivity is degraded as much as possible (approximately 45 db).
5. Remove base-emitter short from Q4. The receiver sensitivity should restore to within 5 db of 20 db quieting level obtained in step 2 above.

STEP 2—QUICK CHECKS

Equipment Required:

- Audio Voltmeter (VTVM)
- Audio Oscillator (sine wave)

SYMPTOMS	PROCEDURE
No regulated 10-volts	Check the 12-volt supply. Then check regulator circuit. (Refer to troubleshooting procedure for power supply.
No blanking	Check waveforms (STEP 3) and voltage ratios (STEP 4).
Partial or no blanking	a. Check RF attenuation as follows: Connect signal generator to Antenna Jack. Adjust the output of the signal generator for 0.2 volts on the 2nd IF amplifier (position B on test set) and note the signal generator reading. Short the Q5 base to emitter pattern (identified by red ink dot) and increase the signal generator output until the same 2nd IF amplifier reading is obtained. Signal level must increase 60 db or more.
	b. Check repetition rate switch. Connect a 6-kHz sine wave signal from audio oscillator through a 0.33-μf capacitor to point "A" located on the noise blanker board. Adjust the output of the audio oscillator for 2-volts, peak-to-peak. Observe the output of the pulse generator (on noise blanker) with an oscilloscope. The repetition rate of the pulse generator should not increase over 2 kHz or decrease under 1 kHz. (This is true for sine wave inputs like intermodulation in the blanker channel but not for strong impulse noise from antenna.)
	c. Check vehicle ignition system. Worn-out points, bad spark plugs, or breaks in ignition wiring can cause a "dirty" ignition pulse to be generated causing the blanker to operate incorrectly.

STEP 4—VOLTAGE RATIO READINGS

Equipment Required:

- RF Voltmeter (similar to Boonton Model 91-CA
- or Millivac Type MV-18 C)

Procedure:

1. Apply probe to input of stage (for example, base of 1st RF Amp). Peak resonant circuit of stage being measured and take voltage reading (E<sub>1</sub>).
2. Move probe to input of following stage (2nd RF Amp). Repeak first resonant circuit. Then peak circuit being measured and take reading (E<sub>2</sub>).
3. Convert readings by means of the following formula.

$$\text{Voltage Ratio} = \frac{E_2}{E_1}$$

4. Check results with typical voltage ratios shown on diagram for each stage.

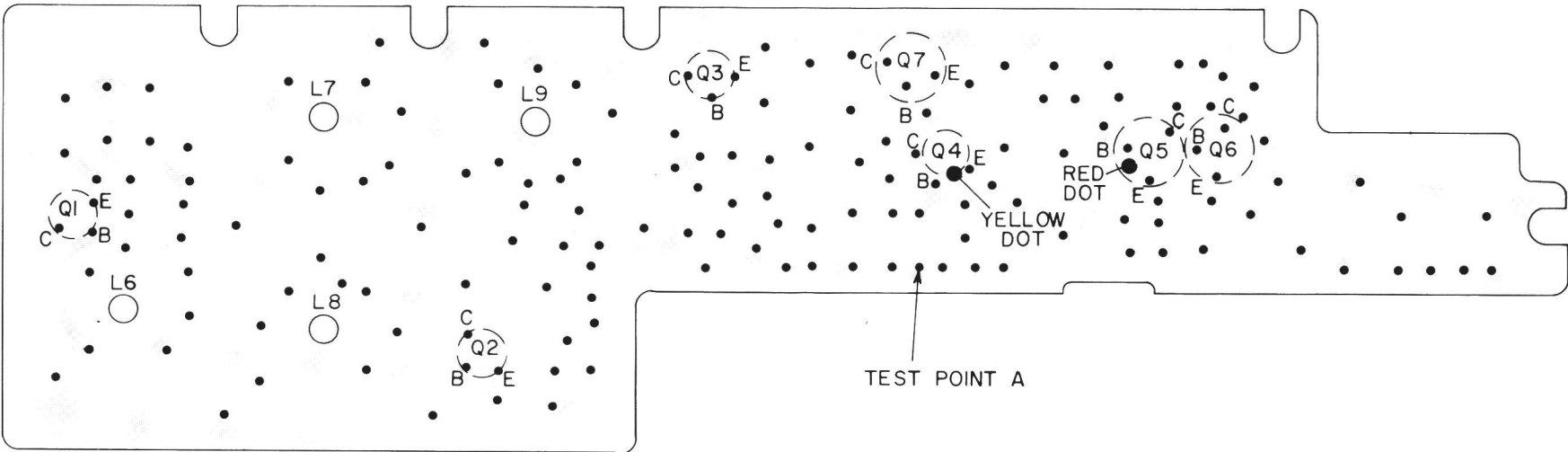
STEP 3—WAVE FORMS

Equipment Required:

- Oscilloscope
- Noise Generator

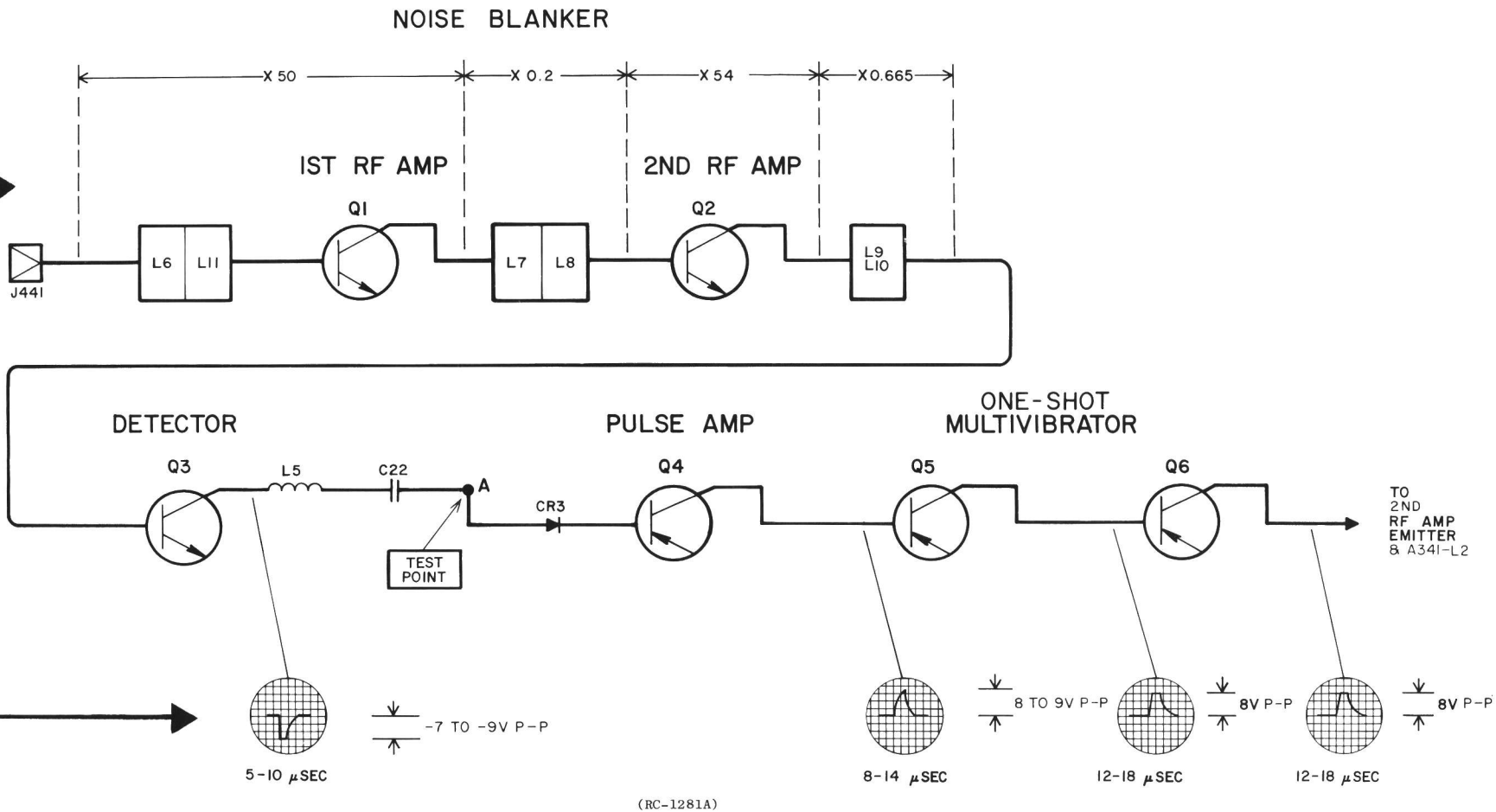
Procedure:

Adjust noise generator for maximum output level and observe waveforms on oscilloscope at the indicated points.



Denotes Solder Side

(RC-1693)  
(19B204655, Sh. 2, Rev. 3)



TROUBLESHOOTING PROCEDURE

NOISE BLANKER FOR 25—50 MHZ RECEIVER  
TYPE ER-39-C

STEP 1 - QUICK CHECKS

TEST SET CHECKS

These checks are typical voltage readings measured with GE Test Set Model 4EX3A10 in the Test 1 position, or Model 4EX8K10 or 11 in the 1-volt position.

Metering Position	Reading With No Signal In	Reading with 1 Micro-volt Unmodulated
A (Disc Idling)	Less than ±.05 VDC	
B (2nd IF)	.15 VDC	.7 VDC
C (1st Lim)	.7 VDC	0.8 VDC
D (Mult-1)	0.6 VDC	
J (Reg. +10 volts)	+10 VDC	

SYMPTOM CHECKS

SYMPTOM	PROCEDURE
NO SUPPLY VOLTAGE	<ul style="list-style-type: none"><li>Check power connections and continuity of supply leads, and check fuse in power supply. If fuse is blown, check receiver for short circuits.</li></ul>
NO REGULATED 10-VOLTS	<ul style="list-style-type: none"><li>Check the 12-volt supply. Then check regulator circuit. (See Troubleshooting Procedure for Power Supply).</li></ul>
LOW 1ST LIM READING	<ul style="list-style-type: none"><li>Check supply voltages and then check oscillator reading at J442-4 &amp; 5 as shown in STEP 2A.</li><li>Make SIMPLIFIED VTVM GAIN CHECKS from 2nd Mixer through 1st Limiter stages as shown in STEP 2A.</li></ul>
LOW OSCILLATOR/MULTIPLIER READINGS	<ul style="list-style-type: none"><li>Check alignment of Oscillator. (Refer to Front End Alignment Procedure).</li><li>Check voltage and resistance readings of 1st Oscillator/Multiplier Q1/Q2.</li><li>Check crystal Y1.</li></ul>
LOW RECEIVER SENSITIVITY	<ul style="list-style-type: none"><li>Check Front End Alignment. (Refer to Receiver Alignment Procedure).</li><li>Check antenna connections, cable and relay.</li><li>Check 1st and 2nd Oscillator injection voltage.</li><li>Check voltage and resistance readings of 1st Mixer, HI IF Amp and 2nd Mixer.</li><li>Make SIMPLIFIED GAIN CHECKS (STEP 2A).</li></ul>
LOW AUDIO	<ul style="list-style-type: none"><li>Check Audio PA (Q341 &amp; Q342) voltage readings on schematic diagram.</li><li>Make simplified gain and waveform checks of audio and squelch stages. (Steps 2A and 2B).</li><li>Make unsquelched voltage readings in Audio section. (Refer to Receiver Schematic Diagram).</li><li>Check voltage and resistance readings on Channel Guard board.</li></ul>
HIGH DISTORTION AT LOW AUDIO LEVELS (50 MW)	<ul style="list-style-type: none"><li>Set PA bias adjust R43 as specified under Service.</li><li>Checks in STEP 1 of TEST PROCEDURES.</li></ul>
IMPROPER SQUELCH OPERATION	<ul style="list-style-type: none"><li>Check voltage and resistance readings of Squelch circuit. (Refer to Receiver Schematic Diagram).</li><li>Make gain and waveform checks of audio and squelch stages. (Steps 2A and 2B).</li></ul>
DISCRIMINATOR IDLING TOO FAR OFF ZERO	<ul style="list-style-type: none"><li>See if discriminator zero is in center of IF bandpass.</li></ul>

STEP 3-VOLTAGE RATIO READINGS

EQUIPMENT REQUIRED:

- RF VOLT METER (SIMILAR TO BOONTON MODEL 91-CA OR MILLIVAC TYPE MV-18 C.
- SIGNAL ON RECEIVER FREQUENCY (BELOW SATURATION). CORRECT FREQUENCY CAN BE DETERMINED BY ZEROING THE DISCRIMINATOR. USE 1,000 HERTZ SIGNAL WITH 3.3 KHZ DEVIATION.

PROCEDURE:

- APPLY PROBE TO INPUT OF STAGE (FOR EXAMPLE, BASE OF RF AMP). PEAK RESONANT CIRCUIT OF STAGE BEING MEASURED AND TAKE VOLTAGE READING (E<sub>1</sub>).
- MOVE PROBE TO INPUT OF FOLLOWING STAGE. REPEAK FIRST RESONANT CIRCUIT THEN PEAK CIRCUIT BEING MEASURED AND TAKE READING (E<sub>2</sub>).
- CONVERT READINGS BY MEANS OF THE FOLLOWING FORMULA.

$$\text{VOLTAGE RATIO} = \frac{E_2}{E_1}$$

- CHECK RESULTS WITH TYPICAL VOLTAGE RATIOS SHOWN ON DIAGRAM.

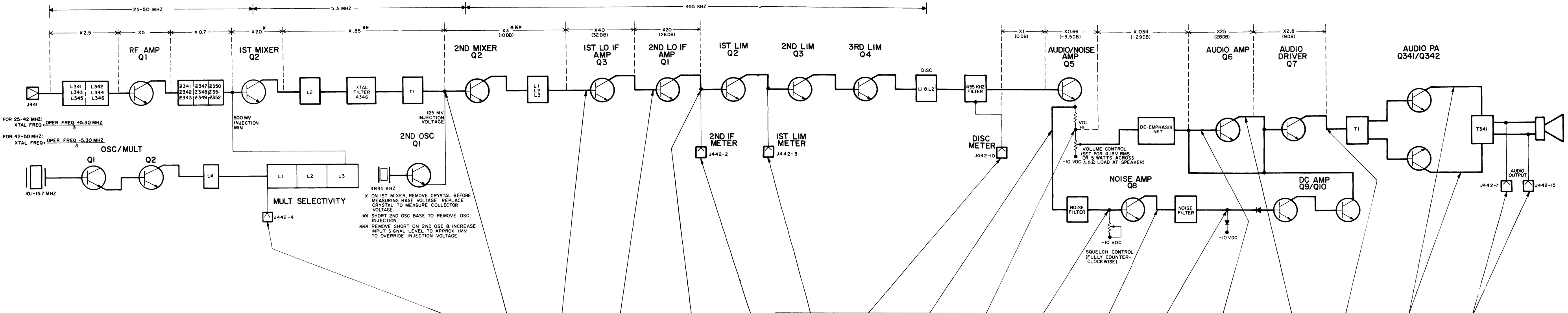
STEP 2A-SIMPLIFIED VTVM GAIN CHECKS

EQUIPMENT REQUIRED:

- Oscilloscope.
- Signal generator (Measurements M560 to equivalent).

PRELIMINARY STEPS:

- Set VOLUME control for 4.18 volts across 3.5-ohm load. If this cannot be obtained, set to approx. 70% of max. rotation.
- Set SQUELCH control fully counterclockwise.
- Receiver should be properly aligned.
- Connect oscilloscope between system negative and points indicated by arrow.



		UNMODULATED	UNMODULATED	UNMODULATED	UNMODULATED	1 MICROVOLT UNMODULATED	NO SIGNAL INPUT	STANDARD SIGNAL-1 (1 MILLIVOLT AT RCVR FREQ MODULATED BY 1KHZ WITH 3.3KHZ DEVIATION)	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL
SIGNAL GENERATOR INPUT AT J441 MAINTAIN SETTING AT DISCRIMINATOR ZERO		INCREASE GENERATOR OUTPUT UNTIL VTVM READING ON 1.5 V SCALE DECREASES BY 50 MV	INCREASE SIGNAL GENERATOR OUTPUT FROM ZERO UNTIL VTVM READING DECREASES BY 5%	INCREASE SIGNAL GENERATOR OUTPUT FROM ZERO UNTIL VTVM READING DECREASES BY 5%	INCREASE SIGNAL GENERATOR OUTPUT FROM ZERO UNTIL VTVM READING DECREASES BY 5%													
PROCEDURE		GENERATOR OUTPUT SHOULD BE APPROX 20 MILLIVOLTS	GENERATOR OUTPUT SHOULD BE APPROX 600 MICROVOLTS	GENERATOR OUTPUT SHOULD BE APPROX 5 MICROVOLTS	GENERATOR OUTPUT SHOULD BE APPROX 0.3 MICROVOLTS	-0.6 VDC	-2 VDC	0.8 VAC	0.75 VAC	0.55 VAC	0.15 VAC	2.3 VAC	0.05 VAC		0.5 VAC	1.4 VAC	10 VAC	4.18 VAC
READING	2.4 VDC																	

STEP 2B-AUDIO & SQUELCH WAVEFORMS

EQUIPMENT REQUIRED:

- VTVM - AC & DC
- Signal generator (Measurements M560 to equivalent).

PRELIMINARY STEPS:

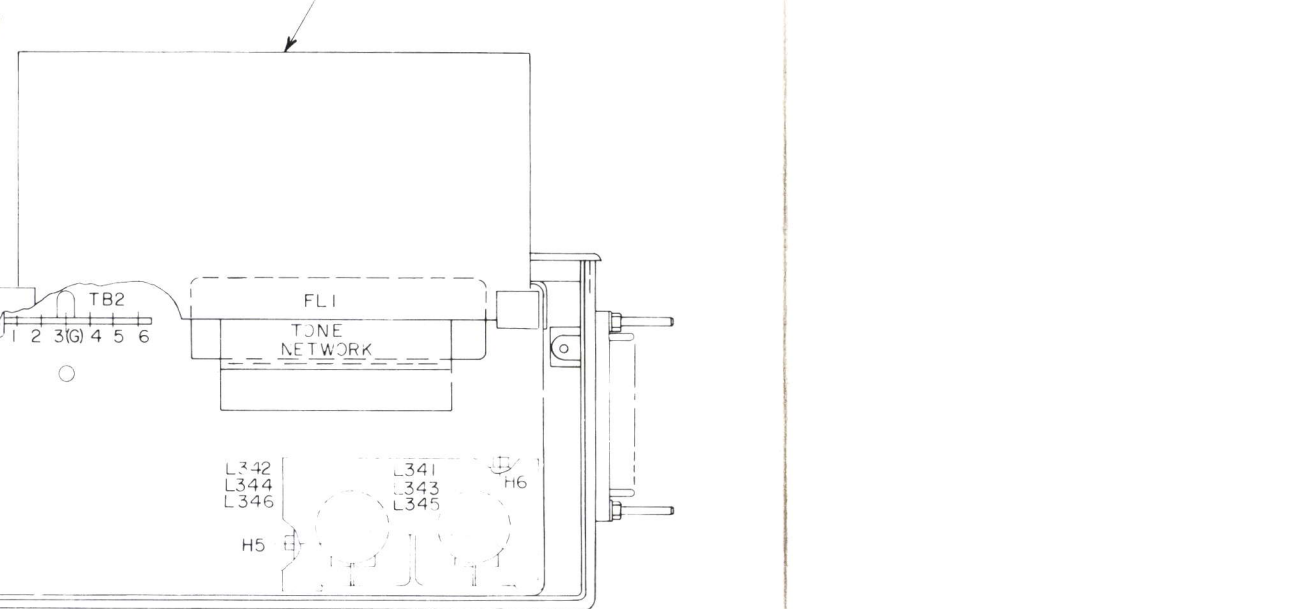
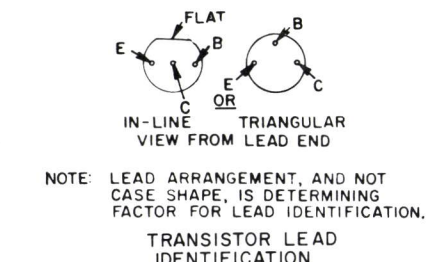
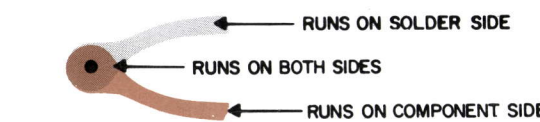
- Set VOLUME control for 4.18 volts across 3.5-ohm load. If this cannot be obtained, set to approx. 70% of max. rotation.
- Set SQUELCH control fully counterclockwise.
- Receiver should be properly aligned.
- Connect VTVM between system negative and points indicated by arrow.

SCOPE SETTING	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV
	1 VOLT/DIV	1 VOLT/DIV	1 VOLT/DIV	2 VOLTS/DIV	0.5 VOLTS/DIV	50 MILLIVOLTS/DIV	1 VOLT/DIV	2 VOLTS/DIV	1 V P-P	2 VOLTS/DIV	1 V P-P	2 VOLTS/DIV	1 V P-P	2 VOLTS/DIV	1 V P-P	2 VOLTS/DIV	1 V P-P	2 VOLTS/DIV
STANDARD SIGNAL (1 MILLIVOLT AT RECEIVER FREQ MODULATED BY 1KHZ WITH 3.3 KHZ DEVIATION)																		
NOISE WAVE FORM (NO SIGNAL INPUT)																		

TROUBLESHOOTING PROCEDURE

25—50 MHz, MASTR RECEIVER  
MODELS 4ER39C28-45







PARTS LIST		
LBI-3915B		
25-50 MHz RECEIVER MODELS 4ER39C28 - 4ER39C45		
SYMBOL	G-E PART NO.	DESCRIPTION
A341		RF AMPLIFIER ASSEMBLY 19B204772-G1
		----- CAPACITORS -----
		C1 5494481-P12 Ceramic disc: .001 $\mu$ f $\pm$ 10%, 1000 VDCW; sim to RMC Type JF Discap.
		C2 5494481-P14 Ceramic disc: .002 $\mu$ f $\pm$ 10%, 1000 VDCW; sim to RMC Type JF Discap.
C3 and C4		5493392-P7 Ceramic, feed-thru: .001 $\mu$ f $\pm$ 100% -0%, 500 VDCW; sim to Allen-Bradley Type FASC.
		----- TRANSISTORS -----
		Q1 19A115342-P1 Silicon, NPN.
		----- RESISTORS -----
R1		3R152-P123K Composition: 12,000 ohms $\pm$ 10%, 1/4 w.
		R2 3R152-P302J Composition: 3000 ohms $\pm$ 5%, 1/4 w.
		R3 3R152-P102K Composition: 1000 ohms $\pm$ 10%, 1/4 w.
		R4 3R152-P391K Composition: 390 ohms $\pm$ 10%, 1/4 w.
XQ1		----- SOCKETS -----
		Transistor: 4 contacts rated at 1 amp at 400 VMS; sim to Eico 3303.
		A344 RF AMPLIFIER ASSEMBLY 19B204770-G1
		----- CAPACITORS -----
C1		5494481-P14 Ceramic disc: .002 $\mu$ f $\pm$ 10%, 1000 VDCW; sim to RMC Type JF Discap.
		----- DIODES AND RECTIFIERS -----
		CR1 4038056-P1 Germanium.
		----- TRANSISTORS -----
Q1		19A115342-P1 Silicon, NPN.
		----- RESISTORS -----
		R1 3R152-P510J Composition: 51 ohms $\pm$ 5%, 1/4 w.
		----- TERMINAL BOARDS -----
TB1		7487424-P19 Miniature, phen: 3 terminals.
		A346 CRYSTAL FILTER 19B204616-G3
		----- FILTERS -----
		FL5 19B206692-G1 Bandpass.
R7		3R152-P562K Composition: 5600 ohms $\pm$ 10%, 1/4 w.
		R8 3R152-P103K Composition: 10,000 ohms $\pm$ 10%, 1/4 w.
		A347 SECOND MIXER 19B216119-G1 REV A
		----- CAPACITORS -----
C1		19C301540-P261 Ceramic disc: 82 pf $\pm$ 5%, 200 VDCW, temp coef -80 PPM.
		5491798-P3 Tuning slug.
		----- CRYSTALS -----
		Y1 19A110192-P3 Quartz: freq 4845 KHz $\pm$ 100 Hz at 25°C, temperature range -30°C to +75°C.

SYMBOL	G-E PART NO	DESCRIPTION
C2	19B209243-P7	Polyester: 0.1 $\mu$ f $\pm$ 20%, 50 VDCW.
C3	5494481-P112	Ceramic disc: .001 $\mu$ f $\pm$ 10%, 1000 VDCW; sim to RMC Type JF Discap.
C4 and C5	5490008-P35	Silver mica: 220 pf $\pm$ 5%, 500 VDCW; sim to Electro Motive Type DM-15.
C6	5490008-P9	Silver mica: 18 pf $\pm$ 5%, 500 VDCW; sim to Electro Motive Type DM-15.
C7 and C8	19B209243-P5	Polyester: 0.047 $\mu$ f $\pm$ 20%, 50 VDCW.
C9	5496219-P369	Ceramic disc: 180 pf $\pm$ 5%, 500 VDCW, temp coef -150 PPM.
C10	19B209243-P7	Polyester: 0.1 $\mu$ f $\pm$ 20%, 50 VDCW.
C11	5496219-P40	Ceramic disc: 9 pf $\pm$ 0.25 pf, 500 VDCW, temp coef 0 PPM.
C12	5496219-P369	Ceramic disc: 180 pf $\pm$ 5%, 500 VDCW, temp coef -150 PPM.
C13	5496219-P40	Ceramic disc: 9 pf $\pm$ 0.25 pf, 500 VDCW, temp coef 0 PPM.
C14	5496219-P471	Ceramic disc: 220 pf $\pm$ 5%, 500 VDCW, temp coef -220 PPM.
C15	7491385-P109	Ceramic disc: .001 $\mu$ f $\pm$ 10%, 500 VDCW; sim to RMC Type JF.
C16	19B209243-P5	Polyester: 0.047 $\mu$ f $\pm$ 20%, 50 VDCW.
C17*	19B209243-P1	Polyester: 0.01 $\mu$ f $\pm$ 20%, 50 VDCW. Added by Rev A.
J1	4033513-P4	Contact, electrical; sim to Bead Chain L93-3.
L1 thru L3	19C311181-G3	Coil. Includes tuning slug 4038368-P1.
P1	4029840-P2	Contact, electrical: sim to Amp 42827-2.
P2	4029840-P1	Contact, electrical: sim to AMP 41854.
Q1	19A115889-P1	Silicon, NPN.
Q2	19A115245-P1	Silicon, NPN.
Q3	19A115123-P1	Silicon, NPN; sim to Type 2N2712.
R1 and R2	3R77-P103K	Composition: 10,000 ohms $\pm$ 10%, 1/2 w.
R3	3R77-P512J	Composition: 5100 ohms $\pm$ 5%, 1/2 w.
R4	3R152-P333K	Composition: 33,000 ohms $\pm$ 5%, 1/4 w.
R5	3R152-P103J	Composition: 10,000 ohms $\pm$ 5%, 1/4 w.
R6	3R77-P332K	Composition: 3300 ohms $\pm$ 10%, 1/2 w.
R7	3R77-P123K	Composition: 12,000 ohms $\pm$ 10%, 1/2 w.
R8	3R77-P622J	Composition: 6200 ohms $\pm$ 5%, 1/2 w.
R9	3R77-P302J	Composition: 3000 ohms $\pm$ 5%, 1/2 w.
R10	3R77-P202J	Composition: 2000 ohms $\pm$ 5%, 1/2 w.
R11	3R77-P201J	Composition: 200 ohms $\pm$ 5%, 1/2 w.
T1		----- TRANSFORMERS -----
C1		19C301540-P261 Ceramic disc: 82 pf $\pm$ 5%, 200 VDCW, temp coef -80 PPM.
		5491798-P3 Tuning slug.
		----- CAPACITORS -----
		Y1 19A110192-P3 Quartz: freq 4845 KHz $\pm$ 100 Hz at 25°C, temperature range -30°C to +75°C.

SYMBOL	G-E PART NO	DESCRIPTION
A348		IF AUDIO AND SQUELCH 19D413129-G1 REV A
C1	5494481-P111	----- CAPACITORS ----- Ceramic disc: .001 $\mu$ f $\pm$ 20%, 1000 VDCW; sim to RMC Type JF Discap.
C2	5496219-P717	Ceramic disc: 47 pf $\pm$ 10%, 500 VDCW, temp coef -750 PPM.
C3	5494481-P111	Ceramic disc: .001 $\mu$ f $\pm$ 20%, 1000 VDCW; sim to RMC Type JF Discap.
C4	5496219-P717	Ceramic disc: 47 pf $\pm$ 10%, 500 VDCW, temp coef -750 PPM.
C5 and C8	5494481-P111	Ceramic disc: .001 $\mu$ f $\pm$ 20%, 1000 VDCW; sim to RMC Type JF Discap.
C7	19B209243-P5	Polyester: 0.047 $\mu$ f $\pm$ 20%, 50 VDCW.
C8	5496219-P369	Ceramic disc: 180 pf $\pm$ 5%, 500 VDCW, temp coef -150 PPM.
C9 and C10	5490008-P37	Silver mica: 270 pf $\pm$ 5%, 500 VDCW; sim to Electro Motive Type DM-15.
C11	5496219-P656	Ceramic disc: 51 pf $\pm$ 5%, 500 VDCW, temp coef -470 PPM.
C12	5494481-P108	Ceramic disc: 470 pf $\pm$ 10%, 1000 VDCW; sim to RMC Type JF Discap.
C13	19A115680-P107	Electrolytic: 100 $\mu$ f $\pm$ 150% -10%, 15 VDCW; sim to Mallory Type TT.
C14 and C15	19A115680-P104	Electrolytic: 50 $\mu$ f $\pm$ 150% -10%, 25 VDCW; sim to Mallory Type TT.
C16	5494481-P112	Ceramic disc: .001 $\mu$ f $\pm$ 10%, 500 VDCW; sim to RMC Type JF Discap.
C17	19B209243-P7	Polyester: 0.1 $\mu$ f $\pm$ 20%, 50 VDCW.
C18	5494481-P108	Ceramic disc: 470 pf $\pm$ 10%, 1000 VDCW; sim to RMC Type JF Discap.
C19 and C20	19B209243-P5	Polyester: 0.047 $\mu$ f $\pm$ 20%, 50 VDCW.
C21*	19B209243-P3	Polyester: 0.022 $\mu$ f $\pm$ 20%, 50 VDCW. Earlier than REV A.
C22	19B209243-P116	Polyester: 0.01 $\mu$ f $\pm$ 20%, 50 VDCW.
C23	19B209243-P107	Polyester: 0.15 $\mu$ f $\pm$ 10%, 50 VDCW.
C24*	19B209243-P106	Polyester: .068 $\mu$ f $\pm$ 10%, 50 VDCW. Deleted by REV A.
C25	5496267-P6	Tantalum: 33 $\mu$ f $\pm$ 20%, 10 VDCW; sim to Sprague Type 150D.
C26*	5496267-P28	Tantalum: 0.47 $\mu$ f $\pm$ 20%, 35 VDCW; sim to Sprague Type 150D. Earlier than REV A.
C27	5496267-P14	Polyester: 0.33 $\mu$ f $\pm$ 20%, 50 VDCW.
C28*	5496267-P229	Tantalum: 33 $\mu$ f $\pm$ 20%, 10 VDCW; sim to Sprague Type 150D.
C29*	5496267-P17	Tantalum: 1.0 $\mu$ f $\pm$ 20%, 35 VDCW; sim to Sprague Type 150D. Deleted by REV A.
C30	19B209243-P16	Polyester: 0.15 $\mu$ f $\pm$ 20%, 50 VDCW.
C31	19B209243-P102	Polyester: 0.015 $\mu$ f $\pm$ 20%, 50 VDCW.
C32	19B209243-P7	Polyester: 0.1 $\mu$ f $\pm$ 20%, 50 VDCW.
C33	19B209243-P17	Polyester: 0.22 $\mu$ f $\pm$ 20%, 50 VDCW.
C34	4029003-P207	Silver mica: 1830 pf $\pm$ 2%, 500 VDCW; sim to Electro Motive Type DM-20.
C35	19B209243-P5	Polyester: 0.047 $\mu$ f $\pm$ 20%, 50 VDCW.
C36	19B209243-P7	Polyester: 0.1 $\mu$ f $\pm$ 20%, 50 VDCW.
C37*	5496267-P28	Tantalum: 0.47 $\mu$ f $\pm$ 20%, 35 VDCW; sim to Sprague Type 150D. Earlier than REV A.
	5496267-P17	Tantalum: 1.0 $\mu$ f $\pm$ 20%, 35 VDCW; sim to Sprague Type 150D.

SYMBOL	G-E PART NO	DESCRIPTION
C38*	5496267-P10	Tantalum: 22 $\mu$ f $\pm$ 20%, 15 VDCW; sim to Sprague Type 150D.
R11	3R77-P223K	Composition: 82,000 ohms $\pm$ 10%, 1/2 w.
C39	19B209243-P1	Polyester: 0.01 $\mu$ f $\pm$ 20%, 50 VDCW.
C40*	5496267-P28	Tantalum: 0.47 $\mu$ f $\pm$ 20%, 35 VDCW; sim to Sprague Type 150D. Earlier than REV A.
C41	5490008-P129	Silver mica: 120 pf $\pm$ 10%, 500 VDCW; sim to Electro Motive Type DM-15.
C42*	19B209243-P4	Polyester: 0.033 $\mu$ f $\pm$ 20%, 50 VDCW. Deleted by REV A.
C43	5496267-P213	Tantalum: 2.2 $\mu$ f $\pm$ 10%, 20 VDCW; sim to Sprague Type 150D. Deleted by REV A.
C49*	5496267-P9	Tantalum: 3.3 $\mu$ f $\pm$ 15%, VDCW; sim to Sprague Type 150D. Added by REV A.
C50*	19B209243-P7	Polyester: 0.1 $\mu$ f $\pm$ 20%, 50 VDCW. Added by REV A.
C51*	5494481-P127	Ceramic disc: 2700 pf $\pm$ 20%, 1000 VDCW; sim to RMC Type JF Discap. Added by REV A.
C52*	19B209243-P117	Polyester: 0.22 $\mu$ f $\pm$ 10%, 50 VDCW. Added by REV A.
C53* and C54*	5496267-P213	Tantalum: 2.2 $\mu$ f $\pm$ 10%, 20 VDCW; sim to Sprague Type 150D. Added by REV A.
CR1 and CR2	19A115250-P1	Silicon.
CR3 and CR4	4038056-P1	Germanium.
CR5 thru CR7	19A115250-P1	Silicon.
CR8*	19A115250-P1	Silicon. Added by REV A.
J1 thru J22	4033513-P4	Contact, electrical: sim to Bead Chain L93-3.
L1	19C311181-G1	Coil.
L2	19C311181-G2	Coil. Includes tuning slug 4038368-P1.
L3	19A127134-G1	Choke. Includes tuning slug 7486872-P7.
Q1 thru Q6	19A115123-P1	Silicon, NPN; sim to Type 2N2712.
Q7	19A115300-P4	Silicon, NPN; sim to Type 2N3053.
Q8	19A115123-P1	Silicon, NPN; sim to Type 2N2712.
Q9	19A115362-P1	Silicon, NPN; sim to Type 2N2925.
Q10	19A115123-P1	Silicon, NPN; sim to Type 2N2712.
R1	3R77-P102K	Composition: 1000 ohms $\pm$ 10%, 1/2 w.
R2	3R77-P153J	Composition: 15,000 ohms $\pm$ 5%, 1/2 w.
R3	3R77-P823K	Composition: 82,000 ohms $\pm$ 10%, 1/2 w.
R4	3R77-P472K	Composition: 4700 ohms $\pm$ 10%, 1/2 w.
R5	3R77-P102K	Composition: 1000 ohms $\pm$ 10%, 1/2 w.
R6	3R77-P153J	Composition: 15,000 ohms $\pm$ 5%, 1/2 w.
R7	3R77-P823K	Composition: 82,000 ohms $\pm$ 10%, 1/2 w.
R8	3R77-P472K	Composition: 4700 ohms $\pm$ 10%, 1/2 w.
R9	3R77-P102K	Composition: 1000 ohms $\pm$ 10%, 1/2 w.

SYMBOL	G-E PART NO	DESCRIPTION
R10	3R77-P153J	Composition: 15,000 ohms $\pm$ 5%, 1/2 w.
R11	3R77-P223K	Composition: 82,000 ohms $\pm$ 10%, 1/2 w.
R12	3R77-P472K	Composition: 4700 ohms $\pm$ 10%, 1/2 w.
R13	3R77-P222K	Composition: 2700 ohms $\pm$ 10%, 1/2 w.
R14	3R77-P103J	Composition: 10,000 ohms $\pm$ 5%, 1/2 w.
R15	3R77-P333J	Composition: 33,000 ohms $\pm$ 5%, 1/2 w.
R16	3R77-P181K	Composition: 180 ohms $\pm$ 10%, 1/2 w.
R17	3R152-P471J	Composition: 470 ohms $\pm$ 5%, 1/4 w.
R18 and R19	3R152-P513J	Composition: 51,000 ohms $\pm$ 5%, 1/4 w.
R20	3R152-P472K	Composition: 4700 ohms $\pm$ 10%, 1/4 w.
R21 and R22	3R77-P362J	Composition: 3600 ohms $\pm$ 5%, 1/2 w.
R23	3R77-P104K	Composition: 0.1 megohms $\pm$ 10%, 1/2 w.
R24	3R152-P102J	Composition: 1000 ohms $\pm$ 5%, 1/4 w.
R25 and R26	3R77-P103K	Composition: 10,000 ohms $\pm$ 10%, 1/2 w.
R27 and R28	3R77-P753J	Composition: 75,000 ohms $\pm$ 5%, 1/2 w.
R29	3R77-P182J	Composition: 1800 ohms $\pm$ 5%, 1/2 w.
R30	3R77-P102J	Composition: 1000 ohms $\pm$ 5%, 1/2 w.
R31	3R77-P821J	Composition: 820 ohms $\pm$ 5%, 1/2 w.
R32*	3R77-P752J	Composition: 7500 ohms $\pm$ 5%, 1/2 w. Deleted by REV A.
R33*	3R77-P912J	Composition: 9100 ohms $\pm$ 5%, 1/2 w. Earlier than REV A.
R34	3R77-P203J	Composition: 20,000 ohms $\pm$ 5%, 1/2 w.
R35	3R77-P330K	Composition: 3300 ohms $\pm$ 10%, 1/2 w.
R36	3R77-P681J	Composition: 680 ohms $\pm$ 5%, 1/2 w.
R37*	3R77-P822J	Composition: 8200 ohms $\pm$ 5%, 1/2 w. Deleted by REV A.
R38*	3R77-P752J	Composition: 7500 ohms $\pm$ 5%, 1/2 w. Earlier than REV A.
R39*	3R77-P820J	Composition: 8200 ohms $\pm$ 5%, 1/2 w. Earlier than REV A.
R40	3R77-P131J	Composition: 130 ohms $\pm$ 5%, 1/2 w.
R41*	3R77-P241J	Composition: 240 ohms $\pm$ 5%, 1/2 w.
R42*	3R77-P200J	Composition: 24 ohms $\pm$ 5%, 1/2 w. Earlier than REV A.
R43	19B209358-P101	Variable, carbon film: approx 25 to 250 ohms $\pm$ 10%, 0.2 w; sim to CTS Type X-201.
R44	19B209022-P101	Wirewound: .27 ohms $\pm$ 105%, 2 w; sim to IRC Type BWH.
R45	3R77-P123J	Composition: 12,000 ohms $\pm$ 5%, 1/2 w.
R46	3R77-P913J	Composition: 91,000 ohms $\pm$ 5%, 1/2 w.
R48*	3R77-P302J	Composition: 3000 ohms $\pm$ 5%, 1/2 w. Earlier than REV A.
R49	3R77-P103J	Composition: 10,000 ohms $\pm$ 5%, 1/2 w.
R50	3R77-P222J	Composition: 2200 ohms $\pm$ 5%, 1/2 w.
R51	3R77-P103J	Composition: 10,000 ohms $\pm$ 5%, 1/2 w.
R52	5496267-P1	Composition: 6800 ohms $\pm$ 5%, 1/2 w.
R53*	3R77-P473J	Composition: 47,000 ohms $\pm$ 5%, 1/2 w. Earlier than REV A.
	3R77-P303J	Composition: 30,000 ohms $\pm$ 5%, 1/2 w.
R54	3R77-P822J	Composition: 8200 ohms $\pm$ 5%, 1/2 w.

SYMBOL	G-E PART NO	DESCRIPTION
R55	3R77-P103K	Composition: 10,000 ohms $\pm$ 10%, 1/2 w.
R56	3R77-P224J	Composition: 0.22 megohms $\pm$ 5%, 1/2 w.
R57	3R77-P103K	Composition: 10,000 ohms $\pm$ 10%, 1/2 w.
R58	3R77-P181K	Composition: 180 ohms $\pm$ 10%, 1/2 w.
R59	3R77-P393K	Composition: 39,000 ohms $\pm$ 10%, 1/2 w.
R60 and R61	3R77-P103K	Composition: 10,000 ohms $\pm$ 10%, 1/2 w.
R62*	3R77-P103K	Composition: 10,000 ohms $\pm$ 10%, 1/2 w. Earlier than REV A.
R63*	3R77-P432J	Composition: 4300 ohms $\pm$ 5%, 1/2 w. Deleted by REV A.
R64	3R77-P180J	Composition: 18 ohms $\pm$ 5%, 1/2 w.
R65*	3R77-P154K	Composition: 0.15 megohms $\pm$ 10%, 1/2 w. Deleted by REV A.
R66	3R77-P472K	Composition: 4700 ohms $\pm$ 10%, 1/2 w.
R75*	3R77-P473J	Composition: 47,000 ohms $\pm$ 5%, 1/2 w. Added by REV A.
R76*	3R152-P912J	Composition: 9100 ohms $\pm$ 5%, 1/4 w. Added by REV A.
R77*	3R152-P652J	Composition: 5600 ohms $\pm$ 5%, 1/4 w. added by REV A.
R78*	3R77-P100J	Composition: 10 ohms $\pm$ 5%, 1/2 w. Added by REV A.
R79*	3R152-P393J	Composition: 39,000 ohms $\pm$ 5%, 1/4 w. Added by REV A.
RT1	5490828-P41	Thermistor: 30 ohms $\pm$ 10%, color code black, white; sim to Global Type 5121H-4.
RT2	5490828-P9	Thermistor: 10,000 ohms $\pm$ 10%, color code yellow; sim to Global Type 551H8.
RT3*	5490828-P9	Thermistor: 10,000 ohms $\pm$ 10%, color code yellow; sim to Global Type 551H8. Added by REV A.
T1	19A116040-P1	----- TRANSFORMERS ----- Audio: Pri: 19.3 ohms $\pm$ 10% DC res, Sec: 23.5 ohms $\pm$ 10% DC res.
A350		ENCODER/DECODER 48K16A10 19C311797-G1 REV A
C1	19B209243-P17	Polyester: 0.22 $\mu$ f $\pm$ 20%, 50 VDCW.
C2 and C3	19B209243-P205	Polyester: 0.047 $\mu$ f $\pm$ 5%, 50 VDCW.

### VOLTAGE READINGS

VOLTAGE READINGS ARE TYPICAL READINGS  
MEASURED TO SYSTEM NEGATIVE (J442-8)  
WITH TEST SET MODEL 46X3A/O OR A  
20,000 OHM-PER-VOLT METER

S= NO SIGNAL IN WITH SQUELCH CONTROL  
FULLY COUNTERCLOCKWISE (MAXIMUM SQUELCH)

US= SQUELCH CONTROL FULLY CLOCKWISE  
WITH A ONE WATT UNMODULATED  
SIGNAL (UNSQUELCHED) AND 5 WATT  
AUDIO OUTPUT

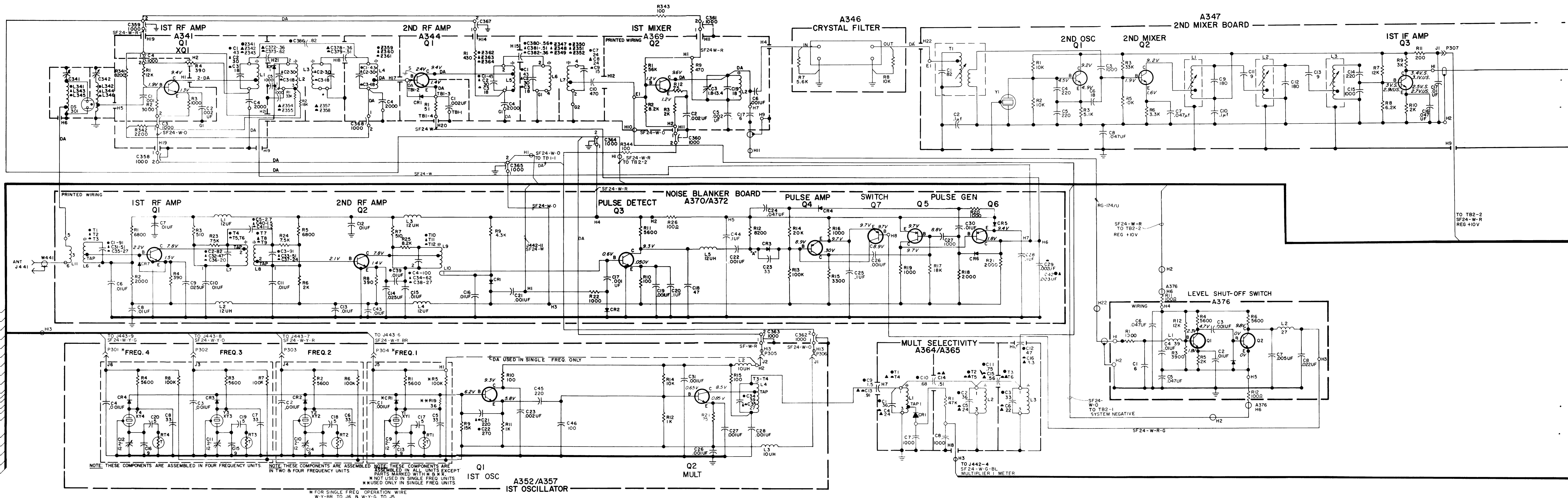
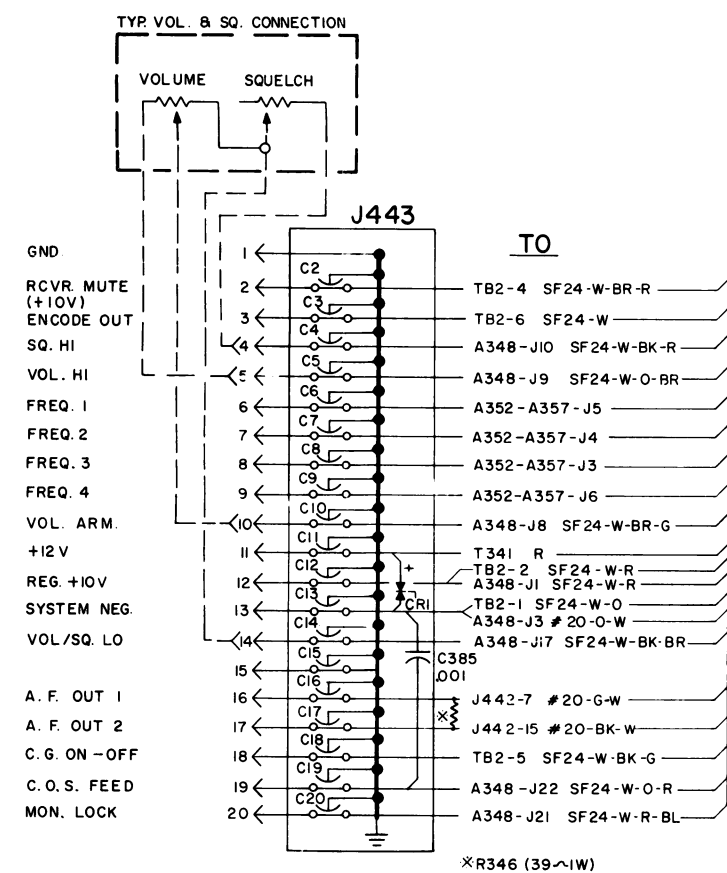
MODEL	FREQ RANGE	NO FREQ	CHAN GUARD
4ER39C28	25 – 33 MHz	1	
4ER39C29	33 – 42 MHz	1	
4ER39C30	42 – 50 MHz	1	
4ER39C31	25 – 33 MHz	2	
4ER39C32	25 – 42 MHz	2	
4ER39C33	42 – 50 MHz	2	
4ER39C34	25 – 33 MHz	4	
4ER39C35	33 – 42 MHz	4	
4ER39C36	42 – 50 MHz	4	
4ER39C37	25 – 33 MHz	1	X
4ER39C38	33 – 42 MHz	1	X
4ER39C39	42 – 50 MHz	1	X
4ER39C40	25 – 33 MHz	2	X
4ER39C41	33 – 42 MHz	2	X
4ER39C42	42 – 50 MHz	2	X
4ER39C43	25 – 33 MHz	4	X
4ER39C44	33 – 42 MHz	4	X
4ER39C45	42 – 50 MHz	4	X

REV. LTR. BLOCK		REV
	PLI9E500873G4	D
	PLI9E500873G5	D
	PLI9E500873G6	D
A347	PLI9B2I6I19G1	A
A350	4EK16A10	A
A348	PLI9D4I3I29G1	A
A402	PLI9C3I1797G2	

- LOW SPLIT 25-33MHZ
- ▲ MID SPLIT 33-42 MHZ
- ◆ HIGH SPLIT 42-50 MHZ
- VALUE OF R47 IS DETERMINED BY TEST (SEE TEST SPEC 19A127182).
- ⊖ THESE ARE ONLY PARTS PRESENT ON A402.

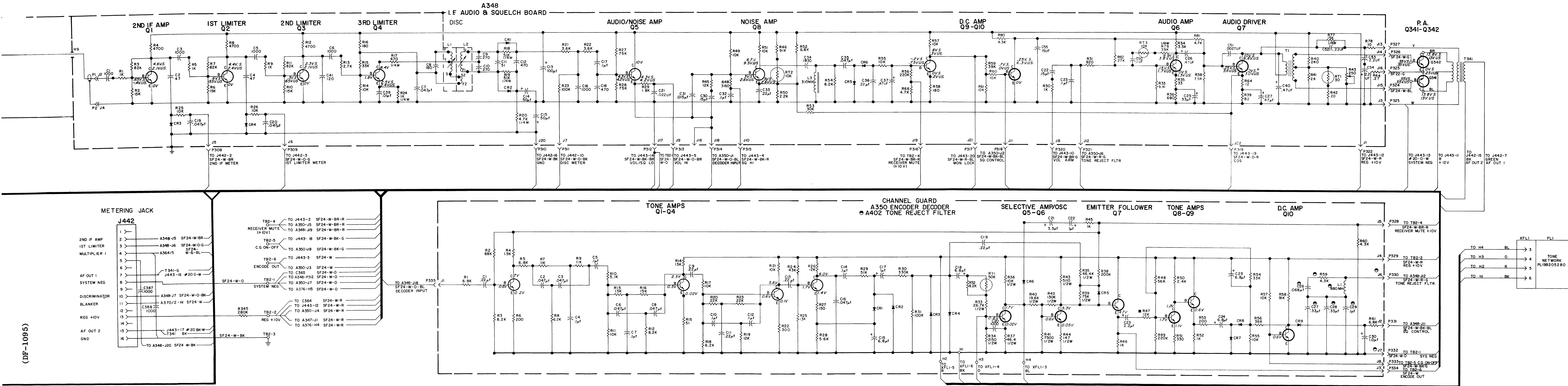
IN ORDER TO RETAIN RATED EQUIPMENT PERFORMANCE, REPLACEMENT OF ANY SERVICE PART SHOULD BE MADE ONLY WITH A COMPONENT HAVING THE SPECIFICATIONS SHOWN ON THE PARTS LIST FOR THAT PART.

ALL RESISTORS ARE 1/2 WATT UNLESS OTHERWISE SPECIFIED AND RESISTOR VALUES IN OHMS UNLESS FOLLOWED BY K=1000 OHMS OR MEG=1,000,000 OHMS. CAPACITOR VALUES IN PICOFARADS (EQUAL TO MICROMICROFARADS) UNLESS FOLLOWED BY UF= MICROFARADS. INDUCTANCE VALUES IN MICROHENRYS UNLESS FOLLOWED BY MH= MILLIHENRYS OR H=HENRYS.



### SCHEMATIC DIAGRAM

25—50 MHZ MASTR RECEIVER  
MODELS 4ER39C28-45



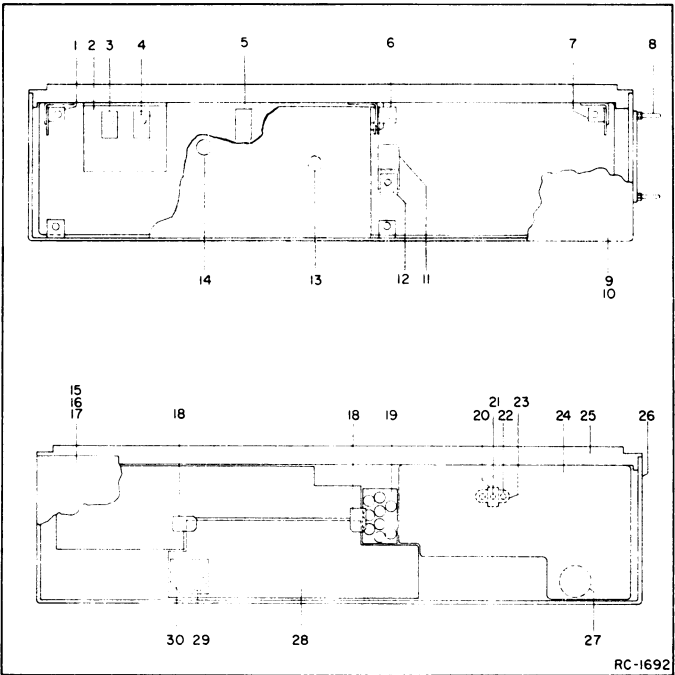
**SCHEMATIC DIAGRAM**

25—50 MHZ MASTR RECEIVER  
MODELS 4ER39C28-45



[illegible]

SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION
J442	19B205689G2	----- JACKS AND RECEPTACLES ----- Connector: 18 contacts.	C2	5496218P250	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -80 PPM.	Z357 and Z358		COIL ASSEMBLY Z357 19B204783G2 Z358 19B204783G3			CHANNEL GUARD MODIFICATION KIT 19A127178G2 (Used with A402)
J443	19C303426G1	Connector: 20 pin contacts.	C3	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.			----- CAPACITORS -----		19B216177G1	----- MISCELLANEOUS ----- Harness (Tone Reject Filter). Includes:
L341 thru L346		----- INDUCTORS ----- COIL ASSEMBLY L341 19B204820G5, L342 19B204820G6 L343 19B204820G1, L344 19B204820G2 L345 19B204820G3, L346 19B204820G4	C4	5494481P14	Ceramic disc: .002 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.	C2	5496218P250	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -80 PPM.	P321	4029840P2	Contact, electrical; sim to Amp 42827-2.
C341 and C342	19B209159P3	----- CAPACITORS ----- Variable, subminiature: approx 1.70-6.9 pf, 750 v peak; sim to EF Johnson 189.		5491798P1	----- MISCELLANEOUS ----- Tuning slug. (Used in Z341).	C3	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.	P330	4029840P2	Contact, electrical; sim to Amp 42827-2.
DS301	19B209067P1	----- INDICATING DEVICES ----- Lamp, glow: 0.3 ma; sim to GE NE-2T.		5491798P4	Tuning slug. (Used in Z342).		5491798P4	----- MISCELLANEOUS ----- Tuning slug. (Used in Z357).	P332	4029840P2	Contact, electrical; sim to Amp 42827-2.
				5491798P5	Tuning slug. (Used in Z343).	Z359 thru Z361	5491798P5	Tuning slug. (Used in Z358).			----- MECHANICAL PARTS ----- (SEE RC-1692)
			Z347 thru Z349		COIL ASSEMBLY Z347 19B204787G1 Z348 19B204787G2 Z349 19B204787G3			COIL ASSEMBLY Z359 19B204785G1 Z360 19B204785G2 Z361 19B204785G3	1	19B204583G3	Hinge.
					----- CAPACITORS -----	C1	5496218P254	----- CAPACITORS ----- Ceramic disc: 43 pf ±5%, 500 VDCW, temp coef -80 PPM.	2	19B216727P1	Support. (Used with Q341 and Q342).
P301 thru P313	4029840P2	----- PLUGS ----- Contact, electrical; sim to Amp 42827-2.	C1	5496218P254	Ceramic disc: 43 pf ±5%, 500 VDCW, temp coef -80 PPM.	C2	5496218P250	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -80 PPM.	3	19A116023P2	Plate, insulated. (Used with Q341 and Q342).
P315 thru P317	4029840P2	Contact, electrical; sim to Amp 42827-2.	C2	5496218P250	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -80 PPM.	C3	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.	4	19A116022P1	Insulator. (Used with Q341 and Q342).
P319 and P320	4029840P2	Contact, electrical; sim to Amp 42827-2.	C3	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.	C4	5494481P14	Ceramic disc: .002 pf ±10%, 10000 VDCW; sim to RMC Type JF Discap.	5	4029851P6	Clip, loop.
P322	4029840P2	Contact, electrical; sim to Amp 42827-2.		5491798P1	----- MISCELLANEOUS ----- Tuning slug. (Used in Z347).		5491798P1	----- MISCELLANEOUS ----- Tuning slug. (Used in Z359).	6	19B204583G1	Hinge.
P323	4029840P1	Contact, electrical: sim to AMP 41854.		5491798P4	Tuning slug. (Used in Z348).		5491798P4	Tuning slug. (Used in Z360).	7	19B204583G2	Hinge.
P324	4029840P2	Contact, electrical; sim to Amp 42827-2.		5491798P5	Tuning slug. (Used in Z349).		5491798P5	Tuning slug. (Used in Z361).	8	19A121676P1	Guide pin.
P325	4029840P1	Contact, electrical: sim to AMP 41854.	Z350 thru Z352		COIL ASSEMBLY Z350 19B204784G4 Z351 19B204784G5 Z352 19B204784G6			COIL ASSEMBLY Z362 19B204787G1 Z363 19B204787G2 Z364 19B204787G3	9	19C303396G4	Bottom cover. (Station)
P326	4029840P2	Contact, electrical; sim to Amp 42827-2.			----- CAPACITORS -----			----- CAPACITORS ----- Ceramic disc: 43 pf ±5%, 500 VDCW, temp coef -80 PPM.	10	19C303385G1	Bottom cover. (Mobile)
P327	4029840P1	Contact, electrical: sim to AMP 41854.			----- MISCELLANEOUS -----			----- MISCELLANEOUS ----- Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.	11	19A121297P1	Angle.
Q341* and Q342*	19A116203P2	----- TRANSISTORS ----- Silicon, NPN.	C7 and C8	5496218P248	Ceramic disc: 24 pf ±5%, 500 VDCW, temp coef -80 PPM.			----- CAPACITORS -----	12	7160861P4	Nut. (Used to secure cover).
	19A115948P1	Earlier than REV D: Silicon, NPN.	C9	5496218P244	Ceramic disc: 15 pf ±5%, 500 VDCW, temp coef -80 PPM.	C1	5496218P254	Ceramic disc: 43 pf ±5%, 500 VDCW, temp coef -80 PPM.	13	4036555P1	Insulator disc. (Used with Q7 on A348).
			C10	5494481P7	Ceramic disc: 470 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.	C2	5496218P250	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -80 PPM.	14	4035267P2	Button, plug. (Used with A348, A350 and A402).
R341	3R152P822K	----- RESISTORS ----- Composition: 8200 ohms ±10%, 1/4 w.			----- MISCELLANEOUS -----	C3	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.	15	19C303495G3	Top cover. (Station, except Repeaters and VM).
R342	3R152P222K	Composition: 2200 ohms ±10%, 1/4 w.		5491798P1	Tuning slug. (Used in Z350).	C4	5494481P14	Ceramic disc: .002 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.	16	19C303676G2	Top cover. (Station, Repeaters and VM only).
R343 and R344	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.		5491798P4	Tuning slug. (Used in Z351).			----- RESISTORS -----	17	19C303385P2	Top cover. (Mobile)
R345	19A116278P444	Metal film: 0.28 megohm ±2%, 1/2 w.		5491798P5	Tuning slug. (Used in Z352).	R1	3R152P431J	Composition: 430 ohms ±5%, 1/4 w.	18	4029851P3	Clip, loop.
R346*	3R78P390K	Composition: 39 ohms ±10%, 1 w. Added by REV D.	Z354 and Z355		COIL ASSEMBLY Z354 19B204787G4 Z355 19B204787G5			----- MISCELLANEOUS -----	19	19A121383P1	Support.
					----- CAPACITORS -----			----- CAPACITORS ----- Ceramic disc: 43 pf ±5%, 500 VDCW, temp coef -80 PPM.	20	4033089P1	Clip. (Part of XY1-XY4).
T341	19A116041P1	----- TRANSFORMERS ----- Audio freq: 300 to 4000 Hz, Pri: 1.00 ohms ±15% DC res, Sec 1: .23 ohm ±10% DC res, Sec 2: 10.5 ohms ±15% DC res.	C2	5496218P250	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -80 PPM.		5491798P1	Tuning slug. (Used in Z362).	21	19B200525P9	Rivet. (Part of XY1-XY4).
			C3	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.		5491798P4	Tuning slug. (Used in Z363).	22	19A115793P1	Contact. (Part of XY1-XY4).
TB1	7487424P26	----- TERMINAL BOARDS ----- Miniature, phen: 6 terminals.		5494481P12	Ceramic disc: .001 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.		5491798P5	Tuning slug. (Used in Z364).	23	4039307P1	Crystal socket. (Part of XY1-XY4).
			C4 and C5		----- DIODES AND RECTIFIERS -----			----- MISCELLANEOUS ----- Channel Guard Modification Kit 19A127178G1 (Used with A350)	24	19C303541P1	Cover.
W441	19B205634G2	----- CABLES ----- Coaxial: approx 5 inches long.	CR1	7777146P3	Germanium.			----- MISCELLANEOUS ----- Harness (Encoder/Decoder). Includes:	25	19C317344P3	Heat sink.
					----- RESISTORS -----	P314	4029840P2	Contact, electrical; sim to Amp 42827-2.	26	19C303389G1	Chassis.
Z341 thru Z343		----- TUNED CIRCUITS ----- COIL ASSEMBLY Z341 19B204786G1 Z342 19B204786G2 Z343 19B204786G3	R1	3R152P333K	Composition: 33,000 ohms ±10%, 1/4 w.	P318	4029840P2	Contact, electrical; sim to Amp 42827-2.	27	4034252P5	Can (Used with T1 on A347).
			R2	3R152P183K	Composition: 18,000 ohms ±10%, 1/4 w.	P321	4029840P2	Contact, electrical; sim to Amp 42827-2.	28	19B204672P1	Cover.
					----- MISCELLANEOUS -----	P328 thru P335		Contact, electrical; sim to Amp 42827-2.	29	7162414P1	Retainer, transistor. (Used with Q1 on A341).
				5491798P4	Tuning slug. (Used in Z354).				30	19B204917P1	Support.
C1	5496218P254	----- CAPACITORS ----- Ceramic disc: 43 pf ±5%, 500 VDCW, temp coef -80 PPM.		5491798P5	Tuning slug. (Used in Z355).						



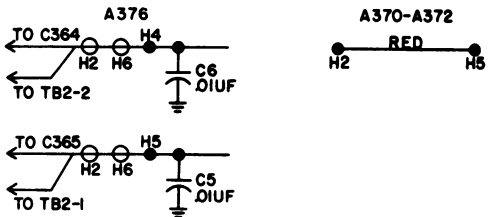
Changes in the equipment to improve performance or to simplify circuits are identified by a "Revision Letter", which is stamped after the model number of the unit. The revision stamped on the unit includes all previous revisions. Refer to the Parts List for descriptions of parts affected by these revisions.

REV. A - 2nd Mixer A347 (19B216119-G1)  
To make receivers compatible with solid-state transmitters. Added C17.

REV. A - Blanker A370-A372 (Part of 19E500873-G4 thru -G6)  
To improve blanking of high repetition rate noise. Changed C23.

REV. B - Level Shut-Off Switch A376 and Blanker A370-A372 (Part of 19E500873-G4 thru -G6)  
To improve receiver selectivity. Changed C5 and C6, and added R11 and R12 in A376. Replaced jumper from H2 to H5 with R26 on A370-A372.

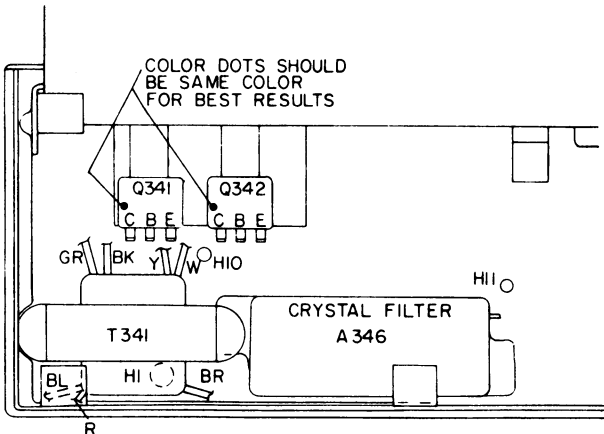
Schematic Diagram Was:



REV. C - 19E500873-G4 thru -G6 (Chassis & RF Assembly)  
To protect the receiver against positive voltage transients. Added thyrector CRI between J443-11 and J443-13.

REV. D - 19E500873-G4 thru -G6 (Chassis & RF Assembly)  
To incorporate new PA transistors. Changed Q341 and Q342 and added R346.

Outline Diagram Was:



PRODUCTION CHANGES

25—50 MHz MASTR RECEIVER  
MODELS 4ER39C10-27

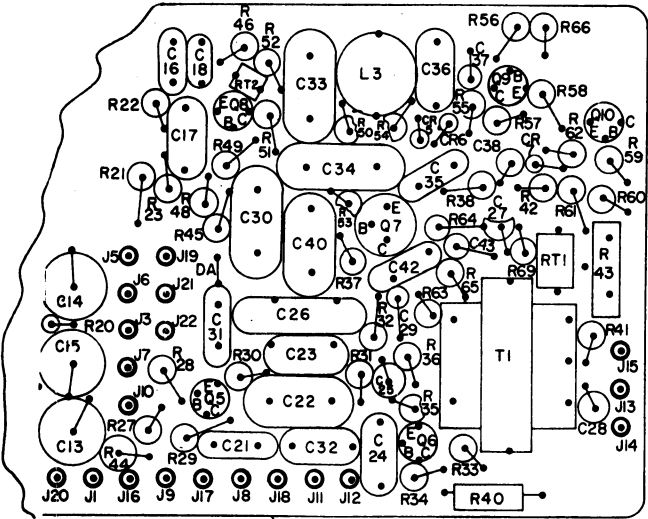
REV. C - 1st Osc/Mult A352 & A353  
REV. A - 1st Osc/Mult A354 thru A357  
These revisions incorporated into initial shipment.

REV. A - Channel Guard Encoder/Decoder Model 4EK16A10  
To obtain correct output level. Changed R8.

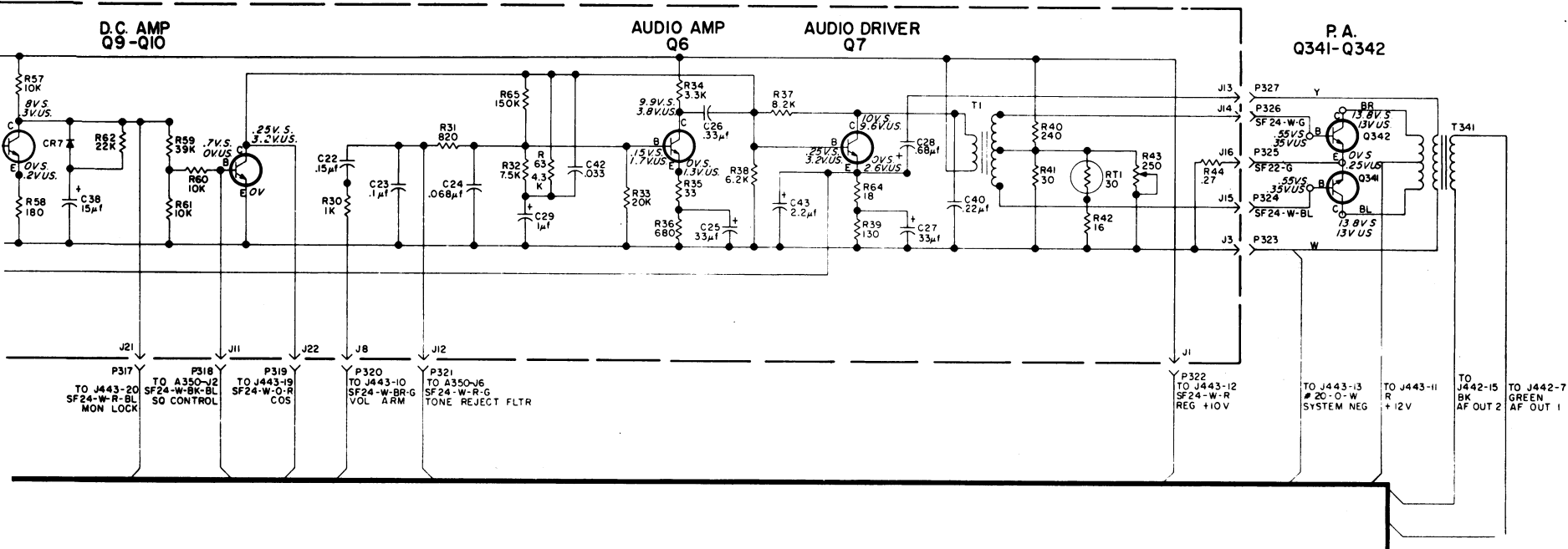
REV. A - IF Audio & Squelch Board A348 (19D413129-G1)  
To make IF Audio & Squelch Board compatible with new PA transistors and to improve squelch operation. Added C49-C54, CR8, R75-R79, and RT3. Deleted C24, C28, C29, C42, C43, R32, R37, R63 and R65. Changed C21, C26, C37, C38, C40 R33, R38, R39, R41, R42, R48, R53 and R62.

Outline Diagram Was:

IF-AUDIO & SQUELCH BOARD  
A348



Schematic Diagram Was:



CHASSIS AND RF ASSEMBLY 19E500873G4 THRU G6

Rev. E - To eliminate squelch opening thump in receivers with Channel Guard. Removed white-orange wire between J443-13 and TB2-1. Added a white-orange wire between P312 (or J17 on IF Audio and Squelch board) and TB2-1.

IF AUDIO AND SQUELCH BOARD A348 (19D413129G1)

Rev. B - To control more closely the squelch control rotation. Changed R48.

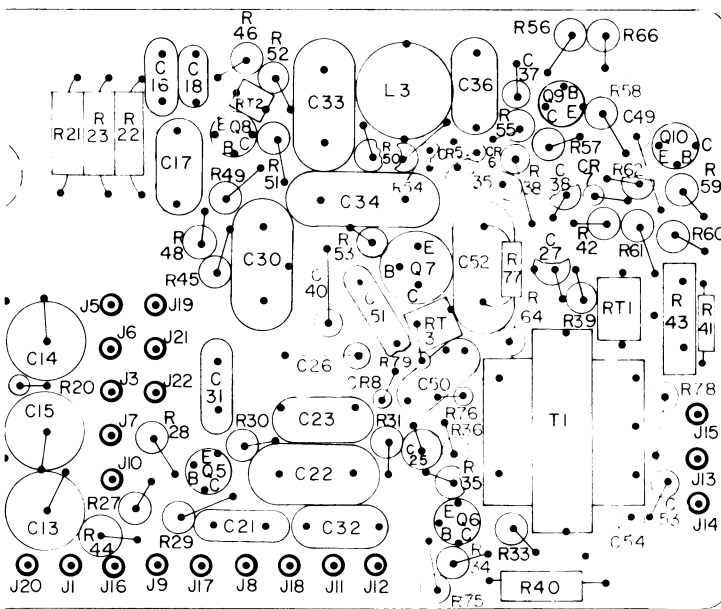
Rev. C - To eliminate barely audible squelch switching transients and to reduce receiver squelch tail.

DELETED C38, C49, CR7, CR8, R62, R75 and R76

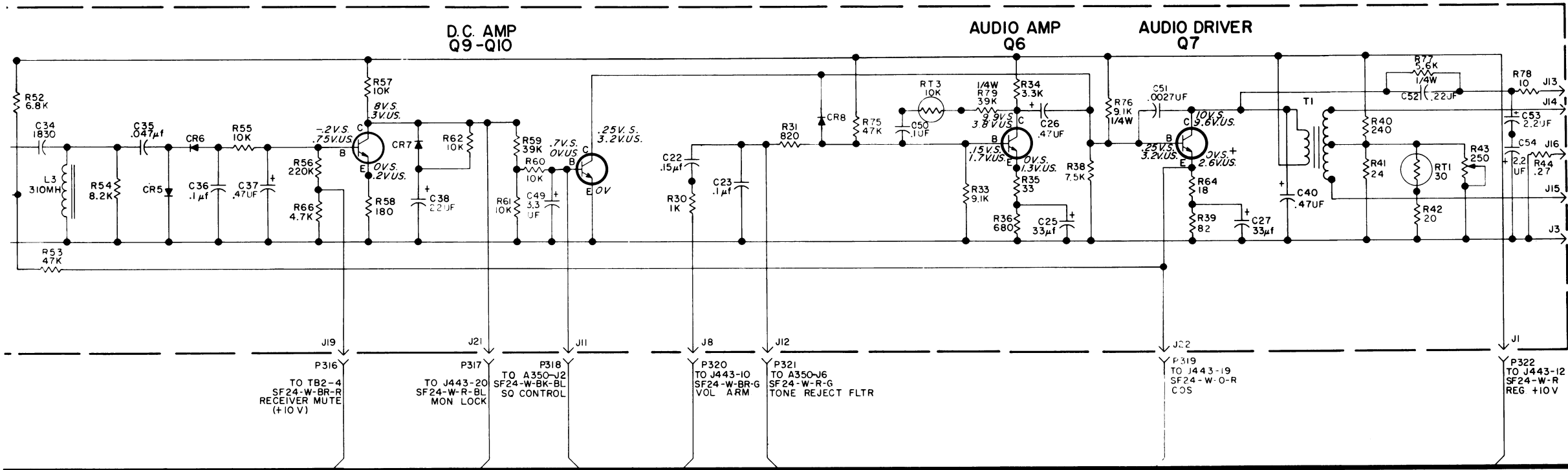
ADDED C55, R80, R81 and R82

CHANGED C27, C36, R53, R64 and R77

Outline Diagram Was:



Schematic Diagram Was:



**PRODUCTION CHANGES**

25—50 MHZ MASTR RECEIVER  
MODELS 4ER39C10-27



The following revision letter changes have been made to improve receiver performance and to facilitate production. The revision stamped on the assemblies includes all previous revisions.

CHASSIS AND RF ASSEMBLY 19E500873-G4 THRU G6

Rev. E - To eliminate squelch opening thump in receivers with Channel Guard. Removed white-orange wire between J443-13 and TB2-1. Added a white-orange wire between P312 (or J17 on IF Audio and Squelch board) and TB2-1.

IF AUDIO & SQUELCH BOARD A348 (19D413129-G1)

Rev. B - To control more closely the squelch control rotation. Changed R48 from 3R77-P332J (3300 ohms  $\pm 5\%$ ) to 19A116278-P249 (3160 ohms  $\pm 2\%$ ).

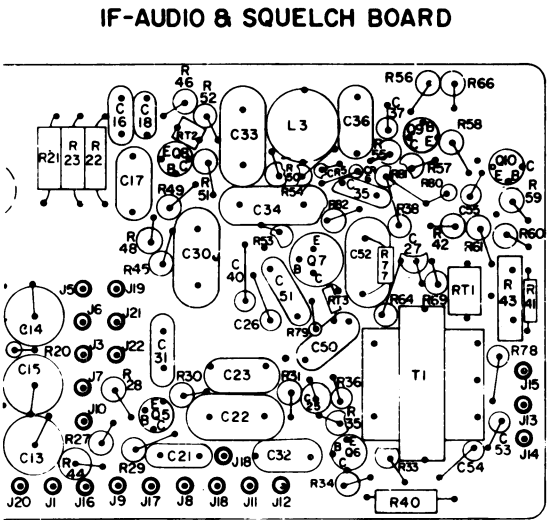
Rev. C - To eliminate barely audible squelch switching transients and to reduce receiver squelch tail.

DELETED: C38, C49, CR7, CR8, R62, R75 and R76

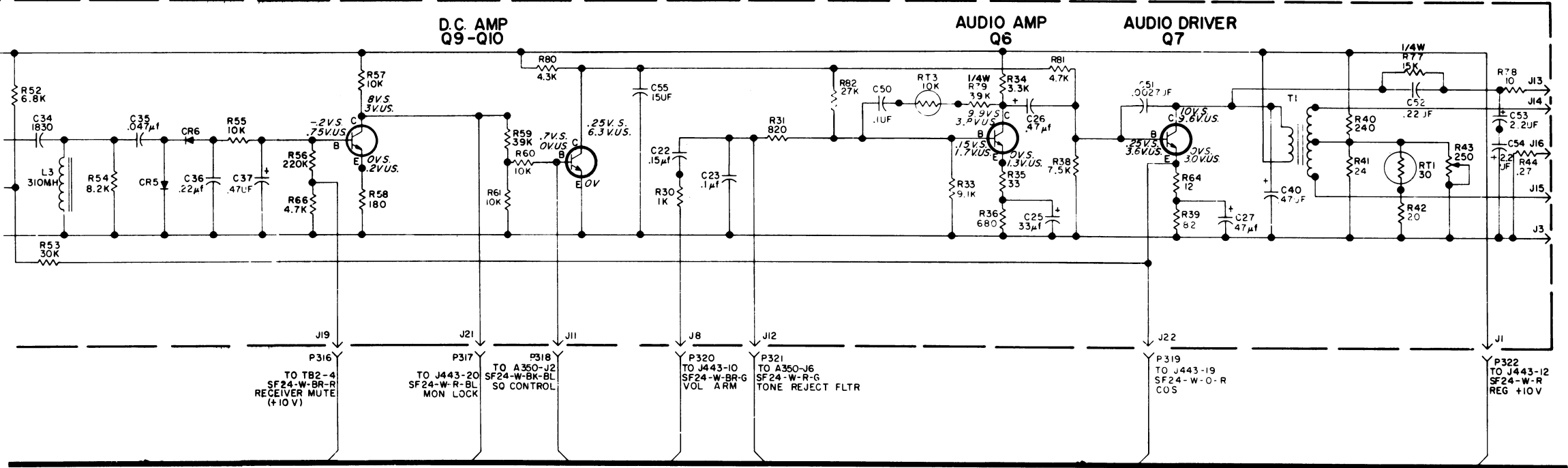
ADDED: C55 (5496267-P14, 15  $\mu$ F)  
R80 (3R152-P432J, 4.3K ohms  $\pm 5\%$ )  
R81 (3R152-P472J, 4.7K ohms  $\pm 5\%$ )  
R82 (3R77-P273J, 27K ohms  $\pm 5\%$ )

CHANGED	FROM	TO
C27	5496267-P6 (33 $\mu$ F)	5496267-P2 (47 $\mu$ F)
C36	19B209243-P7 (0.1 $\mu$ F)	19B209243-P17 (0.22 $\mu$ F)
R53	3R77-P473J (47K ohms)	3R77-P303J (30K ohms)
R64	3R77-P180J (18 ohms)	3R77-P120J (12 ohms)
R77	3R152-P562J (5.6K ohms)	3R152-P153J (15K ohms)

Outline Diagram Changed To:



Schematic Diagram Changed To:



## ORDERING SERVICE PARTS

Each component appearing on the schematic diagram is identified by a symbol number, to simplify locating it in the parts list. Each component is listed by symbol number, followed by its description and GE Part Number.

Service parts may be obtained from Authorized GE Communication Equipment Service Stations or through any GE Radio Communication Equipment Sales Office. When ordering a part, be sure to give:

1. GE Part Number for component
2. Description of part
3. Model number of equipment
4. Revision letter stamped on unit

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These instructions do not purport to cover all details or variations in equipment nor to provide for every possible contingency to be met in connection with installation, operation or maintenance.

Should further information be desired, or should particular problems arise which are not covered sufficiently for the purchaser's purposes, contact the nearest Radio Communication Equipment Sales Office of the General Electric Company.

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**MAINTENANCE MANUAL**

**LBI-3925**

*Progress Is Our Most Important Product*



**MOBILE RADIO DEPARTMENT LYNCHBURG, VIRGINIA 24502**

**(In Canada, Canadian General Electric Company, Ltd., 100 Wingold Ave., Toronto 19, Ontario)**

DF-1095