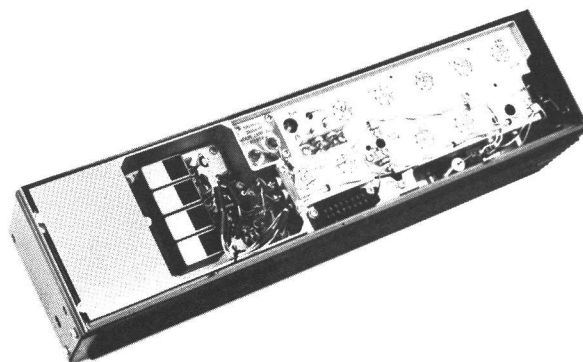


MASTR[®] Progress Line

406—470 MHz, RECEIVER MODELS 4ER42E10-33 & 4ER42G10-33



SPECIFICATIONS *

FCC Filing Designation

Frequency Range

Audio Output

Sensitivity

12-dB SINAD (EIA Method)
20-dB Quieting Method

Intermodulation (EIA)

Selectivity

EIA Two-Signal Method
20-dB Quieting Method

Spurious Response

First Oscillator Stability

Type ER-42-E Receivers
Type ER-42-G Receivers

Modulation Acceptance

Squelch Sensitivity

Critical Squelch
Standard Receiver
UHS Receiver
Maximum Squelch

Maximum Frequency Separation

Frequency Response

ER-42-E & G

406—420 & 450—470 MHz

5 watts at less than 5% distortion

Standard Receiver

0.35 μ V
0.50 μ V

-75 dB

-85 dB (adjacent channel, 25 kHz channels)
-100 dB at ± 20 kHz

-100 dB

$\pm 0.0005\%$ (-30°C to $+60^{\circ}\text{C}$)
 $+0.0002\%$ (-30°C to $+60^{\circ}\text{C}$)

± 7.5 kHz

0.2 μ V
0.15 μ V

Greater than 20 dB quieting (less than 1.5 μ V)

0.4%

+1 and -8 dB of a standard 6-dB per octave de-emphasis curve from 300 to 3000 Hz (1000-Hz reference)

Ultra-High Sensitivity Receiver

0.20 μ V
0.25 μ V

-70 dB

*These specifications are intended primarily for the use of the serviceman. Refer to the appropriate Specification Sheet for the complete specifications.

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WARNING

No one should be permitted to handle any portion of the equipment that is supplied with high voltage; or to connect any external apparatus to the units while the units are supplied with power. **KEEP AWAY FROM LIVE CIRCUITS.**

DESCRIPTION

General Electric MASTR Progress Line Receivers Types ER-42-E & G are double-conversion, superheterodyne FM receivers designed for operation in the 406-420 and 450-470 megahertz bands. The Type ER-42-E Receivers contain a standard oscillator with a frequency stability of $\pm 0.0005\%$, while the Type ER-42-G Receivers contain an Integrated Circuit Oscillator Module (ICOM) with a frequency stability of $\pm 0.0002\%$. Standard and ultra-high sensitivity (UHS) versions are available for both types.

The receivers are of single-unit construction and are completely housed in an aluminum casting for maximum shielding and rigidity. The top part of the casting contains the front end through the 1st low IF amplifier stages. The bottom portion of the casting contains the audio squelch board and the optional Channel Guard encoder-decoder board.

CIRCUIT ANALYSIS

The MASTR Progress Line Receiver is completely transistorized, using silicon transistors throughout for added reliability. Input leads to the receiver are individually filtered by the 20-pin feed-through by-pass connector J443. A regulated +10 Volts is

used for all receiver stages except the audio PA stage which operates from the 12-Volt system supply.

Centralized metering jack J442 is provided for use with General Electric Test Set Models 4EX3A10 or 4EX8K11, for ease of alignment and servicing. The Test Set meters the oscillator, multiplier and limiter stages as well as the discriminator, and regulated 10 Volts.

RF AMPLIFIER (A410)

RF Amplifier A410 is used only in ultra-high sensitivity (UHS) receivers and consists of two tuned helical resonators and an RF amplifier (Q1).

RF from the antenna is coupled through cable W444 to a tap on L410/L412. The tap is positioned to provide the proper impedance match to the antenna. RF energy is coupled to L411/L413 through an opening in the shield wall, and then to the base of Q1. The amplified output is coupled from the collector of Q1 through cable W445 to the input of five helical resonators.

HELICAL RESONATORS

In receivers without the UHS option, the front end RF selectivity is provided by five tuned helical resonators (L414/L419

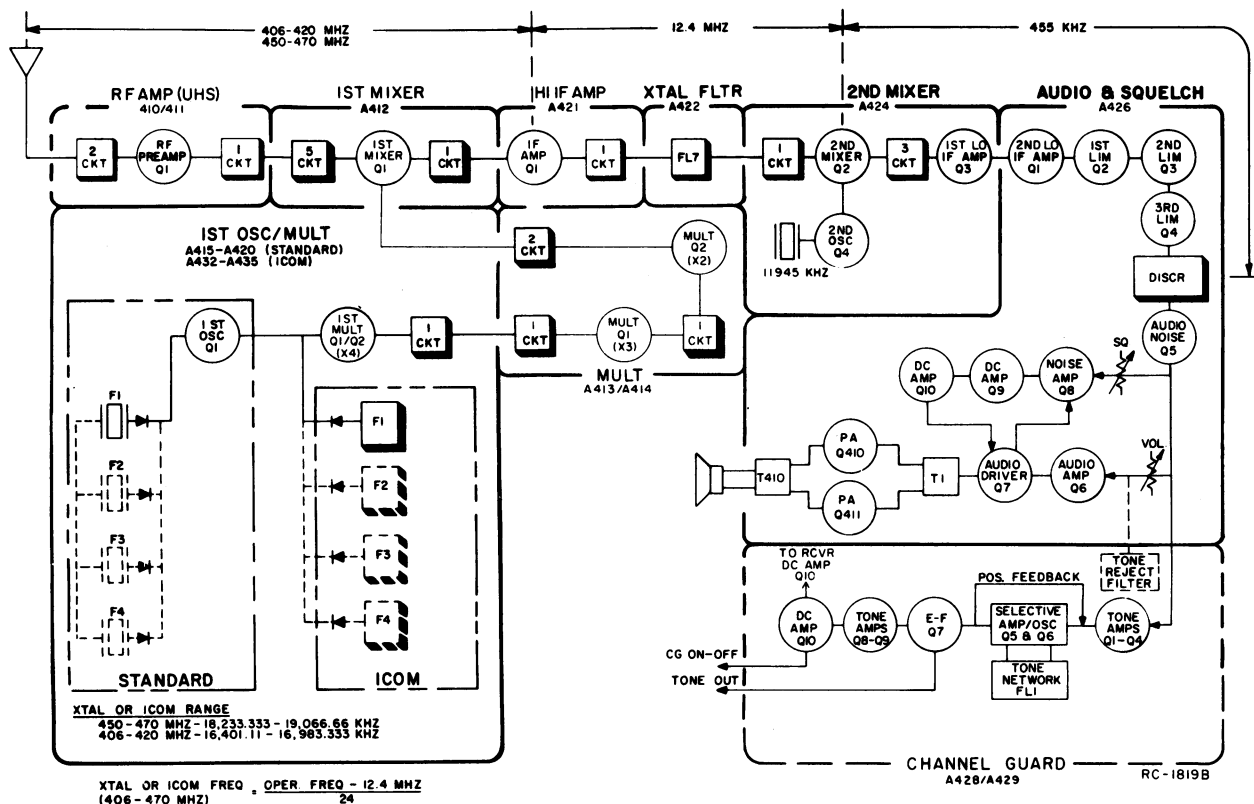


Figure 1 - Receiver Block Diagram

through L418/L423). RF cable W441 connects the RF signal from the antenna to a tap on L414/L419. The tap is positioned to provide the proper impedance match to the antenna. The output of L418/L423 is coupled through capacitor C1 to the 1st Mixer assembly.

1ST OSCILLATOR AND MULTIPLIER

Receiver Models 4ER42E10-33 are equipped with standard Oscillator/Multiplier Boards A415-A420. Receiver Models 4ER42G10-33 are equipped with Oscillator/Multiplier Boards which use the Integrated Circuit Oscillator Module (ICOM).

Standard Oscillator/Multiplier Board (A415-A420)

The oscillator in the standard Oscillator/Multiplier Board is a transistorized Colpitts oscillator. The oscillator crystal operates in a fundamental mode at a frequency of approximately 16 to 19 megahertz. The crystal is cut to provide temperature compensation at the high end of the temperature range and is thermistor compensated at low temperatures. This provides instant warm-up with a frequency stability of $\pm 0.0005\%$ without crystal ovens or warmers.

In single-frequency receivers, a jumper from H1 to H2 connects regulated +10 Volts to the crystal circuit. Feedback for the oscillator is developed across C47.

In multi-frequency receivers, a diode is connected in series with the crystal and up to three additional crystal circuits can be added. The 10-Volt jumper is removed, and the proper frequency is selected by switching the desired crystal circuit to +10 Volts by means of a frequency selector switch on the control unit. Switching the +10 Volts to the crystal circuit forward biases the diode in series with the desired crystal, and the crystal frequency is applied to the base of oscillator transistor Q1. The oscillator output is coupled through C45 to the base of 1st Multiplier Q2.

The 1st multiplier output is coupled through T1/T2 to Multiplier Board A413/A414. T1/T2 is tuned to four times the crystal frequency. The 1st multiplier stage is metered at J442-4 through metering network C38, CR6, R17 and R18.

Oscillator/Multiplier Board With ICOM (A432-A435)

Oscillator/Multiplier Boards A432-A435 uses ICOM Module Model 4EG26A10. The ICOM module consists of a crystal-controlled

Colpitts oscillator, a voltage regulator, and a buffer output stage. The entire module (including crystal) is enclosed in a dust-proof aluminum can, with the ICOM frequency and the receiver operating frequency printed on top. Access to the oscillator trimmer is obtained by prying off the plastic GE decal on the top of the can.

The oscillator frequency is temperature-compensated at both ends of the temperature range to provide instant frequency compensation, with a frequency stability of $\pm 0.0002\%$ without crystal oven or warmers.

In single-frequency receivers, +10 Volts for operating the ICOM is obtained by a jumper from H1 to H2. With the ICOM operating, diode CR1 is forward biased and the oscillator output is applied to the 1st multiplier Q1.

The 1st multiplier output is coupled through T1/T2 to multiplier board A413/A414. T1/T2 is tuned to four times the ICOM frequency. The 1st multiplier stage is metered at J442-4 through metering network C4, CR5, R5 and R6.

In multi-frequency receivers, up to three additional ICOM modules can be plugged into the board. The 10-Volt jumper is removed and the proper frequency is selected by switching the desired ICOM to +10 Volts by means of a frequency selector switch on the control unit.

CAUTION

All ICOM modules are individually compensated at the factory, and cannot be repaired in the field. Any attempt to remove the ICOM cover will void the warranty.

MULTIPLIER BOARD (A413/A414)

Following the oscillator board are two multiplier stages. A413-Q1 operates as a tripler, and Q2 operates as a doubler. Q2 is metered at J442-1 across metering resistor R6.

The output of Q2 is coupled through two helical resonator circuits to the source terminal of the 1st mixer. The helical resonators are tuned to six times the 1st multiplier output for a total multiplication of 24 times the crystal frequency.

1ST MIXER (A412)

The 1st Mixer uses a Field-Effect Transistor (FET) as the active device. A FET may be considered a semiconductor current path (or channel) whose resistance is varied by a voltage applied between the "gate" and "source" terminals. Lead identification

for the FET is shown in Figure 2A. The FET has voltage-controlled characteristics, and may be compared to a vacuum tube in operation (see Figure 2B).

The FET mixer has several advantages over a conventional transistor mixer, including a high input impedance and an output that is relatively free of harmonics (low in intermodulation products).

RF from the helical resonators is applied to the gate of Q1, and injection voltage from the multiplier is applied to the source. The mixer output is taken from the drain with the output tuned to the 12.4 MHz high IF frequency.

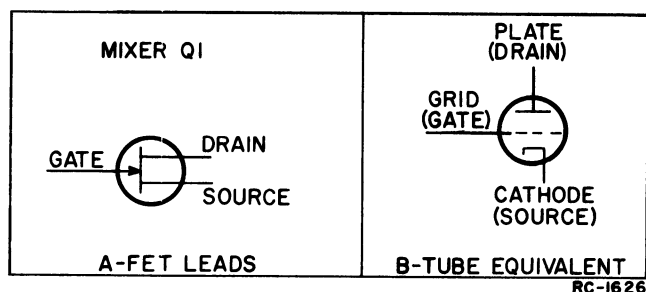


Figure 2 - FET Nomenclature

HI IF AMPLIFIER (A421) AND CRYSTAL FILTER (A422)

A series-resonant circuit (A412-L2 and -C3) couples the mixer output to the emitter of the high IF amplifier A421. The transistor is connected as a grounded-base amplifier which provides a low impedance for the mixer input. The amplifier output is coupled through transformer T1 to the crystal filter.

Highly-selective crystal filter A422 provides the major selectivity for the receiver. The output of the filter is coupled through impedance-matching transformer A424-T2 to the base of the 2nd mixer.

2ND OSCILLATOR, 2ND MIXER AND 1ST LO IF AMPLIFIER (A424)

A424-Q4 operates in a Colpitts Oscillator circuit, with feedback supplied through C18. The oscillator low-side injection voltage (11,945 kHz) is applied to the base of the 2nd mixer.

The High IF signal from the filter and the injection voltage from the 2nd oscillator is applied to the base of 2nd mixer Q2. The 445-kHz mixer output is applied to three tuned low IF circuits, L1, L2 and L3. These tuned circuits are required for shaping the nose of the IF waveform, and for rejecting any undesired output frequencies from the 2nd mixer.

The low IF signal is applied to the base of 1st low IF amplifier Q3. The output of Q3 is R-C coupled to the base of the 2nd low IF amplifier.

2ND LO IF AMPLIFIER AND LIMITERS (A426)

Additional amplification of the low IF signal going to the limiter stages is provided by 2nd low IF amplifier A426-Q1. This stage is metered at J442-2 through a metering network consisting of C19, CR3 and R25.

Following the 2nd low IF amplifier are three R-C coupled limiter stages (A426-Q2, -Q3 and -Q4). The 1st limiter is metered at J442-3 through metering network C20, CR4 and R26.

DISCRIMINATOR (A426)

The limiter output is applied to a Foster-Seely type discriminator, where diodes CR1 and CR2 rectify the 455-kHz signal to recover the audio. The discriminator is metered at J442-10 through metering network C16 and R23.

AUDIO - NOISE AMPLIFIER (A426)

The discriminator output is coupled through a low-pass filter (C16, C18, R21 and R22) to the base of audio-noise amplifier Q5. The filter removes any 455-kHz signal remaining in the discriminator output. Q5 operates as an emitter-follower to match the discriminator impedance to the VOLUME control, SQUELCH control, and Channel Guard input. The stage also provides power gain.

AUDIO AMPLIFIERS (A426)

Any audio present in the incoming signal is coupled from the emitter of Q5 through the VOLUME control and a de-emphasis network to the base of audio amplifier Q6. The de-emphasis network consists of C22, C23, R30 and R31.

Audio driver Q7 follows the audio amplifier. The audio output of Q7 is coupled through transformer T1 to provide phase inversion for the push-pull audio PA stage.

Q410 and Q411 operate as a push-pull Class AB audio PA stage. The PA output is coupled through audio transformer T410 to the loudspeaker. The yellow and white tertiary windings of T410 supply balanced feedback to the collector of Q7. The feedback winding minimizes distortion and prevents the pick-up of external electrical noise.

Base bias for the PA stage and the elimination of crossover distortion is

controlled by bias adjust potentiometer R43. The potentiometer is set at the factory as shown in STEP 1 of the receiver Test Procedure.

NOTE

Do not adjust bias adjust potentiometer R43 unless PA transistors Q410 and Q411 have been replaced.

Audio high and low are also present at centralized metering jack J442, and can be used as shown in STEP 1 of the receiver Test Procedure. The output stage provides 5 Watts at less than 5% distortion into a 3.5-ohm load at the receiver output terminals (3.2-ohm load at the Control Unit).

SQUELCH (A426)

Noise from the audio-noise amplifier operates the squelch circuit. With no carrier present in the receiver, this noise is coupled to the base of noise amplifier Q8 through a high-pass filter which attenuates frequencies below 3 kHz. The filter consists of C30, C31 and R45, as well as C34 and L3 in the collector circuit of Q8. The gain of Q8 is determined by the Squelch control, which varies the bias on the base of Q8. Thermistor RT2 keeps the critical squelch constant over wide variations in temperature.

The output of noise amplifier Q8 is rectified by diodes CR5 and CR6, and filtered by C36 and C37 to produce a negative DC voltage. This DC voltage is applied to the base of DC amplifier Q9, turning it off. When turned off, the collector voltage of Q9 rises to approximately 8 Volts, turning on DC amplifier Q10. When conducting, the collector voltage of Q10 drops to almost ground potential, which removes the base bias to audio amplifier Q6 and audio driver Q7, turning them off.

When the receiver is quieted by a signal (unsquelched), the noise in the receiver is reduced, turning DC amplifier Q9 on and DC amplifier Q10 off. This allows the audio stages to conduct so that sound is heard in the speaker.

Resistor R53 connects from the emitter of audio driver Q7 to the emitter of noise amplifier Q8, providing a hysteresis loop in the squelch circuit. When a weak signal opens the squelch, the signal level may be reduced by 4 to 6 dB without the squelch closing. This limits squelch "flutter" or "picket-fence" operation.

With audio driver Q7 conducting, a positive voltage through R53 helps to reduce the gain of noise amplifier Q8. This positive feedback provides a quick, positive switching action in the squelch circuit.

When the receiver squelches, audio driver Q7 turns off and its emitter potential drops to zero. This reduces the DC feedback through R53 to the emitter of noise amplifier Q8. Reducing the feedback causes Q8 to conduct harder, turning the audio stages off quickly.

Keying the transmitter removes the +10 Volts from J19, turning off DC amplifier Q9 and turning on Q10 to mute the receiver.

CHANNEL GUARD (A428/A429)

Channel Guard Board Model 4EK16A10 is a fully transistorized encoder-decoder for use in the MASTR Professional Series mobile and station combinations. The tone frequencies are controlled by plug-in tone networks that are made with precision components for excellent stability and reliability. The tone frequencies range from 71.9 to 203.5 Hz.

Encoder (A428)

Keying the transmitter removes the receiver mute +10 Volts, and forward biases feedback control diode CR5, causing it to conduct. When conducting, the diode shunts R39 which reduces the impedance of the positive feedback loop (R39, R35, and C19). This provides the necessary gain to the base of Q5 to permit oscillation.

The encoder tone is provided by selective amp-oscillator transistors Q5 and Q6 which oscillate at a frequency determined by the tone network. Negative feedback applied through the tone network to the base of Q5 prevents any gain in the stage except at the desired encode frequency.

Starting network R45, C21, C22 and CR6 provide an extremely fast starting time for the encoder tone. Keying the transmitter removes the receiver mute +10 Volts, causing a pulse to be applied to the base of Q6 to quickly start the oscillator. Thermistor-resistor combination R32 and RT1 provides temperature compensation for the oscillator output. Limiter diodes CR3 and CR4 keep the tone amplitude constant.

Emitter-follower Q7 follows the oscillator circuit. The encoder tone is taken from the emitter of Q7 and applied to an active low-pass filter (G101) on the transmitter.

Decoder (A428)

The decoder function is designed to eliminate all calls that are not tone coded for the Channel Guard frequency. As long as the CHANNEL GUARD-OFF switch on the control unit is left in the CHANNEL GUARD position, all signals are locked out except those from

transmitters that are continuously tone coded for positive identification by the receiver.

Placing the CHANNEL GUARD-OFF switch in the OFF position instantly disables the Channel Guard operation so that all calls on the channel can be heard. When the hook-switch option is used, lifting the microphone from its hanger disables the Channel Guard Circuit.

Audio, tone and noise are taken from the emitter of the receiver audio-noise amplifier A426-Q5 and is fed through A428-J1 to four tone amplifier and bandpass filter circuits. The filters remove the audio and high-frequency noise from the signal, and the tone amplifiers provide sufficient gain to insure clipping by limiter diodes CR1 and CR2. The clipping action eliminates variation in the squelch performance due to changes in tone deviation. The signal is then applied to selective amplifiers Q5 and Q6 which amplify only the tone determined by the tone network.

The output of the selective amplifier is applied through emitter-follower Q7 to the high gain, broad-band tone amplifiers Q8 and Q9. The output of Q9 is rectified by detector diodes CR7 and CR8, and the resulting negative DC voltage controls the squelch gate. Q8 is normally biased for low gain. Then the tone is detected by CR7 and CR8, feedback is provided through R54 to quickly change the bias on Q8 for full gain. This ensures a more positive "unsquelching" action.

Squelch gate diode CR9 is normally forward biased by a positive DC voltage (approximately 1.5 Volts) fed through R58. The forward bias causes CR9 to conduct, feeding a DC voltage to the base of DC amplifier A426-Q10 in the receiver. This removes the bias on the receiver audio stages and hold them off.

When the proper tone is applied to the decoder, the negative DC voltage from the detector diodes back-biases squelch gate diode CR9 and cuts off the positive bias to the receiver DC amplifier A426-Q10. However, the receiver noise squelch circuit continues to operate until a carrier quiets the receiver.

Placing the CHANNEL GUARD - OFF switch in the OFF position (or removing the microphone from its hookswitch) removes the ground to the base of the decoder DC switch (Q10), causing it to conduct. This back-biases

squelch control diode CR9 and cuts off the positive bias to the receiver DC amplifier (A426-Q10). The receiver noise squelch circuit continues to operate until a carrier quiets the receiver.

A tone rejection filter connected in parallel with A426-J2 (in the receiver) bypasses any incoming tone to ground. This attenuates the tone level reaching the receiver audio circuits. The filter is composed of C26, C27, C28, C29, L1 and R59.

An optional tone reject filter (A429) that is identical to the filter described above is available for use in two-way radios with transmitter Channel Guard only.

MAINTENANCE

DISASSEMBLY

To service the receiver from the top--

1. Pull locking handle down and pull radio about one inch out of mounting frame. (see Figure 3).
2. Pry up cover at rear of receiver.
3. Slide cover back and lift off.

To service the receiver from the bottom--

1. Pull locking handle down. Pull radio out of mounting frame. (See Figure 4).
2. Remove screws in bottom cover. Pry up cover at back of receiver.
3. Slide cover back and lift off.

To remove the receiver from the system frame--

1. Loosen the two Phillips-head retaining screws in front casting (see Figure 3), and pull casting away from system frame.
2. Remove the four screws in the back cover.
3. Remove the two screws holding the receiver at each end of the system frame.
4. Disconnect the antenna jack and the 20-pin connector from the front of the receiver, and slide the unit out of the system frame.

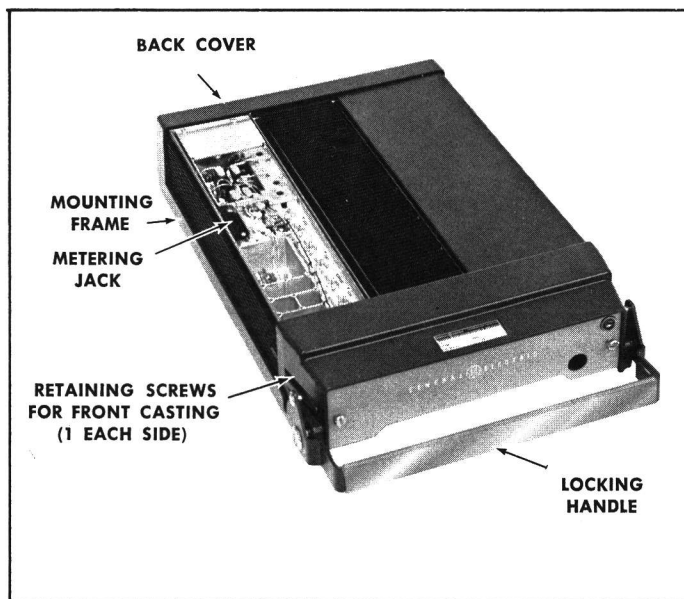


Figure 3 - Removing Top Cover

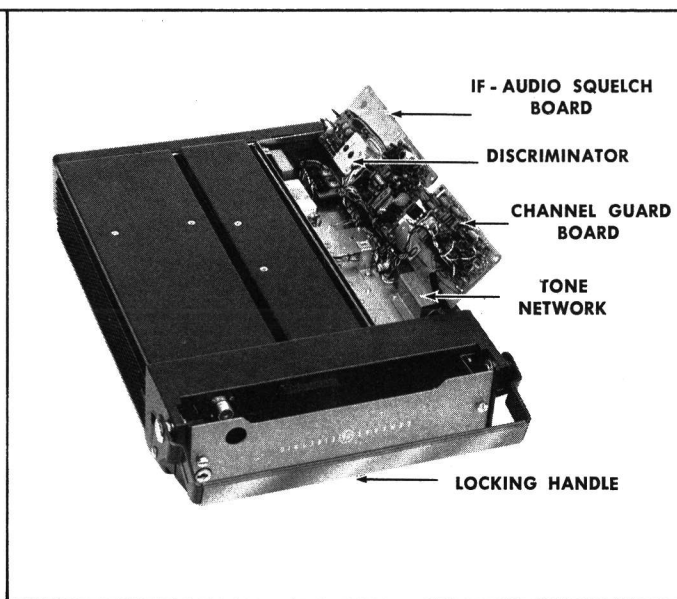


Figure 4 - Removing Bottom Cover

COMPLETE RECEIVER ALIGNMENT

EQUIPMENT REQUIRED

- GE Test Set Models 4EX3A10, 4EX8K11, station test meter panel, or 20,000 ohms-per-volt multimeter.
- A 450 to 460 kHz source (GE Test Set Model 4EX7A10), and 406-470 MHz signal source. Connect a one-inch piece of insulated wire no larger than .065 inch to generator output probe.

PRELIMINARY CHECKS AND ADJUSTMENTS

- Connect Test Set to receiver centralized metering jack J442, and set meter sensitivity switch to the TEST 1 or 1-volt position.
- For a large change in frequency or a badly mis-aligned receiver, set crystal trimmer C9 on 1st OSC/MULT board (ER-42-E only) to mid-capacity. In multi-frequency receivers, set C10, C11 or C12 to mid-capacity as required.
- In multi-frequency receivers where the maximum frequency spacing is less than 500 kHz, align the unit on channel F1. If the frequency spacing is greater than 500 kHz, align the receiver on the center frequency.
- With Test Set in position J, check for regulated +10 volts. If using Multimeter, measure from C425 to C426.
- If using Multimeter, connect the positive lead to J442-16 (ground).
- Disable the Channel Guard.

ALIGNMENT PROCEDURE

STEP	METERING POSITION		TUNING CONTROL	METER READING	PROCEDURE
	GE Test Set or Meter Panel	Multimeter - at J442			
1.	A (DISC)	Pin 10	L1 and L2 (on IF-AUDIO SQUELCH board)	Zero	Remove three screws and swing open the IF-AUDIO & SQUELCH board. Adjust L1 (disc primary) 1/2 turn counterclockwise from the bottom of coil. Next, apply a 455-kHz signal to J2 and J4 and adjust L2 (disc secondary) for zero meter reading.
2.	A (DISC)	Pin 10		See Procedure	Alternately apply a 450-kHz and 460-kHz signal and check for readings of at least 0.3 volt, but not more than 0.5 volt on GE Test Set. Both readings must be within .05 volt. Do not attempt to balance reading any closer than 0.05 volt.
OSCILLATOR AND MULTIPLIERS					
3.	D (MULT-1)	Pin 4	L5 (1st OSC/MULT) and L1 (2nd MULT)	See Procedure	Tune L5 for maximum meter reading. Then tune L1 for minimum meter reading.
4.	G (MULT-1)	Pin 4	L5 (1st OSC/MULT) and L1 and L2 (2nd MULT)	Maximum	Tune L5, L1 and L2 for maximum meter reading. If two peaks occur while tuning L1 and L2, use the peak with the slug nearest the top of the coil.
5.	G (MULT-2)	Pin 4	C423	See Procedure	Adjust C423 for a small dip in meter reading.
6.	A (DISC)	Pin 10		Zero	Apply an on-frequency signal into Hole 411. Adjust the signal generator for discriminator zero.
7.	B (2nd IF AMP)	Pin 2	C423 and C424	Maximum	Apply an on-frequency signal as above. Tune C423 and C424 for maximum meter reading, keeping signal below saturation.
RF SELECTIVITY					
8.	B (2nd IF AMP)	Pin 2	L3 (1st Mixer)	Maximum	Apply an on-frequency signal in the Hole shown below, keeping the signal below saturation. Tune C415 thru C418 for maximum meter reading as shown below: <div>Insert Generator Probe In: Peak 1. Hole 411 C418 thru C417 2. Hole 410 C415, C416 thru C417</div>
9.	B (2nd IF AMP)	Pin 2	C415 thru C418	Maximum	Apply an on-frequency signal in the Hole shown below, keeping the signal below saturation. Tune C415 thru C418 for maximum meter reading, keeping signal below saturation.
10.	B (2nd IF AMP)	Pin 2	C414 thru C418, L3 (on 1st Mixer) and C410, and C411 (on UHS receivers)	See Procedure	Apply an on-frequency signal to the receiver antenna jack. Tune C410, and C411 on UHS receivers for maximum meter reading. On all receivers, tune C414 for maximum meter reading, and tune C415 thru C418 and L3 for maximum quieting.
2ND MIXER & HI IF					
The 2nd mixer, and high IF circuits have been aligned at the factory and will normally require no further adjustment. If adjustment is necessary use the procedure outlined in STEPS 11, 12 and 13.					
NOTE Refer to DATAFILE BULLETIN 1000-6 IF Alignment of Two-Way Radio FM Receivers for helpful suggestions on how to determine when IF alignment is required.					
11.	B (2nd IF AMP)	Pin 2	L3, L2, L1, T2 (2nd Mixer) and T1 (HI IF AMP)	Maximum	Apply on-frequency, unmodulated signal and tune L3, L2, L1, T2 (2nd mixer) and T1 (HI IF AMP) for maximum meter reading, keeping signal below saturation.
12.			L3, L2, L1, T2 (2nd Mixer) and T1 (HI IF AMP)		Connect scope, signal generator, and detector as shown in Figure 7. Set signal generator level for 50-50 μ v and modulate with 10 kHz at 20 Hz. With detector at the collector of Q3 (2nd mixer board output), tune for double trace as shown on scope pattern.
13.	A (DISC)	Pin 10		See Procedure	Check to see that discriminator idling voltage is within $\pm .06$ volt of zero with no signal applied. Check to see that modulation acceptance bandwidth is between ± 7.5 and 9 kHz.
FREQUENCY ADJUSTMENT					
14.	Refer to the appropriate adjustment procedure for the ICOM or Standard Oscillator.				

FRONT END ALIGNMENT

EQUIPMENT REQUIRED

- GE Test Set Model 4EX3A10, 4EX8K11 station test meter panel or 20,000 ohms-per-volt multimeter.
- A 406-470 MHz signal source. Connect a one-inch piece of insulated wire no larger than 0.065 inch to generator output probe.

PRELIMINARY CHECKS AND ADJUSTMENTS

- Connect Test Set to receiver centralized metering jack J442 and set meter sensitivity switch to the TEST 1 (or 1-volt position on 4EX8K11).
- With Test Set in position J, check for regulated +10 volts. If using Multimeter, measure from C425 to C426.
- If using Multimeter, connect the positive lead to J442-16 (ground).
- Disable the Channel Guard.

ALIGNMENT PROCEDURE

METERING POSITION		TUNING CONTROL	METER READING	PROCEDURE
STEP	GE Test Set or Meter Pane			
OSCILLATOR AND MULTIPLIERS				
1.	D (MULT-1)	Pin 4	L5 (1st OSC/MULT) and L1 (2nd MULT)	See Procedure Tune L5 for maximum meter reading. Then Tune L1 for minimum meter reading.
2.	G (MULT-2)	Pin 4	L5 (1st OSC/MULT) and L1 and L2 (2nd MULT)	Maximum Tune L5, L1 and L2 for maximum meter reading. If two peaks occur while tuning L1 and L2, use the peak with the slug nearest the top of the coil.
3.	G (MULT-2)	Pin 4	C423	See Procedure Adjust C423 for a small dip in meter reading.
4.	A (DISC)	Pin 10		Zero Apply on on-frequency signal into Hole 411. Adjust the signal generator for discriminator zero.
5.	B (2nd IF AMP)	Pin 2	C423 and C424	Maximum Apply an on-frequency signal as above. Tune C423 and C424 for maximum meter reading, keeping signal below saturation.
RF SELECTIVITY				
6.	B (2nd IF AMP)	Pin 2	L3, C415-C418	Maximum Apply an on-frequency signal in Hole 411 and tune L3 and C415 thru C418 for maximum meter reading, keeping the signal below saturation. If two peaks occur when tuning L3, use the peak with the slug nearest the bottom of the coil.
7.	B (2nd IF AMP)	Pin 2	C414 thru C418, L3 (on 1st Mixer) and C410, and C411 (on UHS receivers)	See Procedure Apply on on-frequency signal to the receiver antenna jack. Tune C410, and C411 on UHS receivers for maximum meter reading. On all receivers, tune C414 for maximum meter reading, and then tune C415 thru C418 and L3 for maximum quieting.
FREQUENCY ADJUSTMENT				
8.	Refer to the appropriate adjustment procedure for the ICOM or Standard Oscillator.			

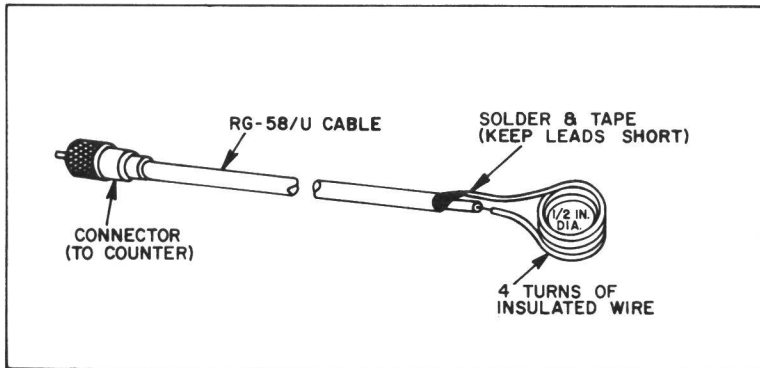


Figure 5 - Coaxial Cable and Test Loop

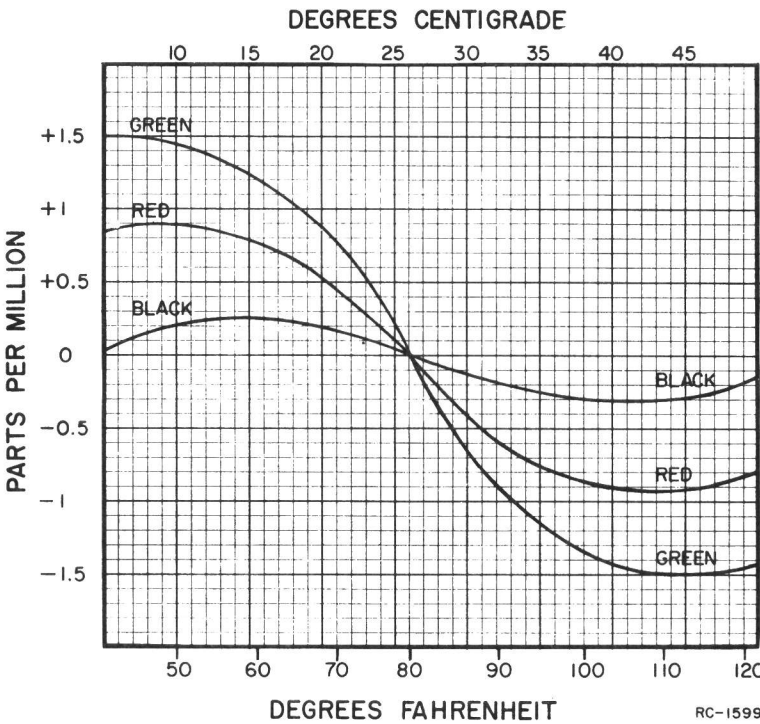


Figure 6 - ICOM Correction Curves

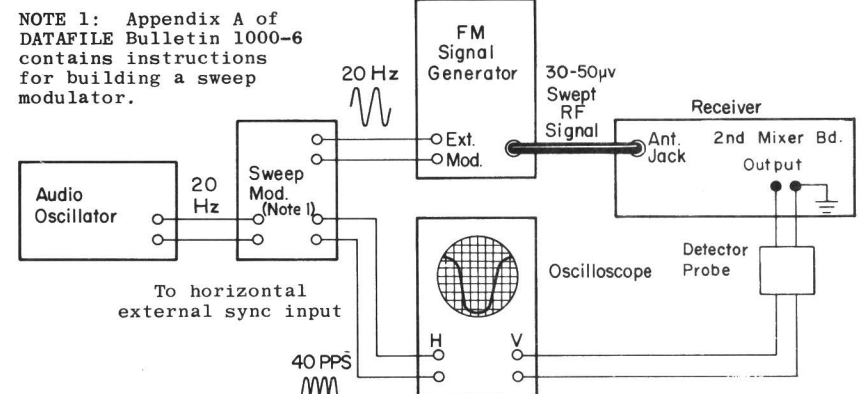
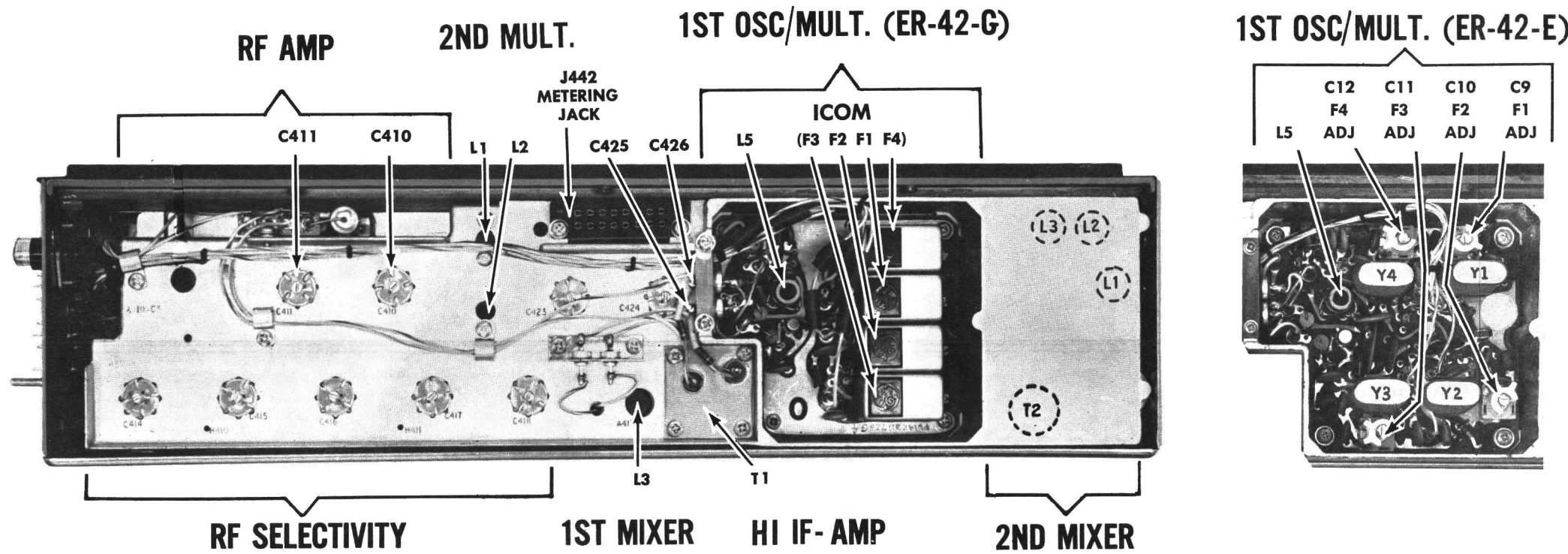


Figure 7 - Test Setup for 20-Hz Double-Trace Sweep Alignment

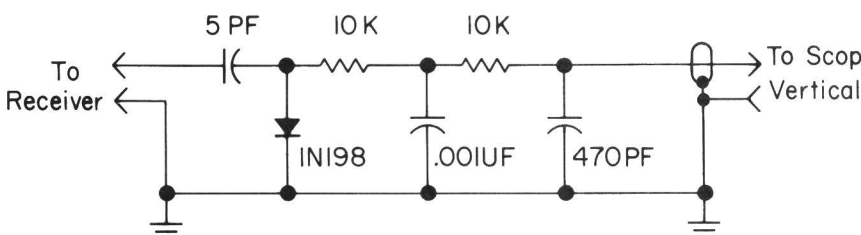


Figure 8 - Detector Probe for Sweep Alignment

FREQUENCY ADJUSTMENT LBI-3999

STANDARD OSCILLATOR

METERING POSITION	TUNING CONTROL	METER READING	PROCEDURE
4EX3A10	Multi-meter - at J442		
A (Disc)	Pin 10	Zero	Apply an on-frequency signal to the antenna jack. Tune C9 for zero discriminator reading. In multi-frequency units, tune C10, C11 or C12 as required. NOTE For proper frequency control of the receiver, it is recommended that all frequency adjustments be made when the equipment is at a temperature of approximately 75°F. In no case should frequency adjustments be made when the equipment is outside the temperature range of 50° to 90°F.

ICOM MODULE

Due to the high stability of the ICOM module, it is not recommended that zero discriminator be used as the indication for setting the oscillator frequency. Instead, measure the ICOM frequency as described in the following procedure.

EQUIPMENT REQUIRED:

- Frequency Counter capable of measuring the 70-80 MHz frequency range. (The counter should have an accuracy of 0.4 part-per-million.)
- Coaxial cable with test loop as described in Figure 5.
- Mercury thermometer.

PROCEDURE:

- Check the ICOM temperature by taping the mercury thermometer to the side of the ICOM.
- Connect the frequency counter to L5 (on the 1st Osc/Mult) using the 4-turn test loop and cable shown in Figure 5.
- If the ICOM temperature is 80°F ($\pm 4^\circ$ F) or 26.5°C ($\pm 2^\circ$ C), the frequency indication on the counter should be 4 times the frequency stenciled on the ICOM case. Adjust the ICOM trimmer (if necessary) to obtain this frequency.
- If the temperature is not within the 80°F ($\pm 4^\circ$ F) or 26.5°C ($\pm 2^\circ$ C) range, use the correction curves of Figure 6 for setting the ICOM frequency as follows:
 - Check the color dot beneath the GE emblem and select the matching curve to determine the correction factor in parts-per-million (PPM).
 - Multiply the frequency stenciled on the ICOM by 4 and then multiply this figure by the correction factor (from Figure 6) observing the sign (\pm) given to the correction factor.
 - The frequency measured at L5 should be 4 times the ICOM frequency \pm the correction factor. Adjust the ICOM trimmer (if required) to obtain this frequency.

FOR EXAMPLE	
ICOM Frequency	18.233333 MHz
ICOM Color Dot	Green
Ambient Temperature	35°C (95°F)
Correction Factor	-1.15 PPM
(From Figure 6)	
Multiply ICOM Frequency by 4:	
(18.233333 MHz x 4 = 72.933332 MHz)	
Multiply preceding figure by correction factor:	
(72.933 MHz x -1.15 PPM = -83.87 hertz (or -84 hertz))	
Set the frequency measured at L5 for 72.933248 MHz:	
72.933332 MHz	
- .000084 MHz	
72.933248 MHz	

ALIGNMENT PROCEDURE

406-470 MHz MASTR RECEIVER
MODELS 4ER42E10-33 & 4ER42G10-33

TEST PROCEDURES

These Test Procedures are designed to help you to service a receiver that is operating---but not properly. The problems encountered could be low power, poor sensitivity, distortion, limiter not operating properly, and low gain. By following the sequence of test steps starting with Step 1, the defect can be quickly localized. Once

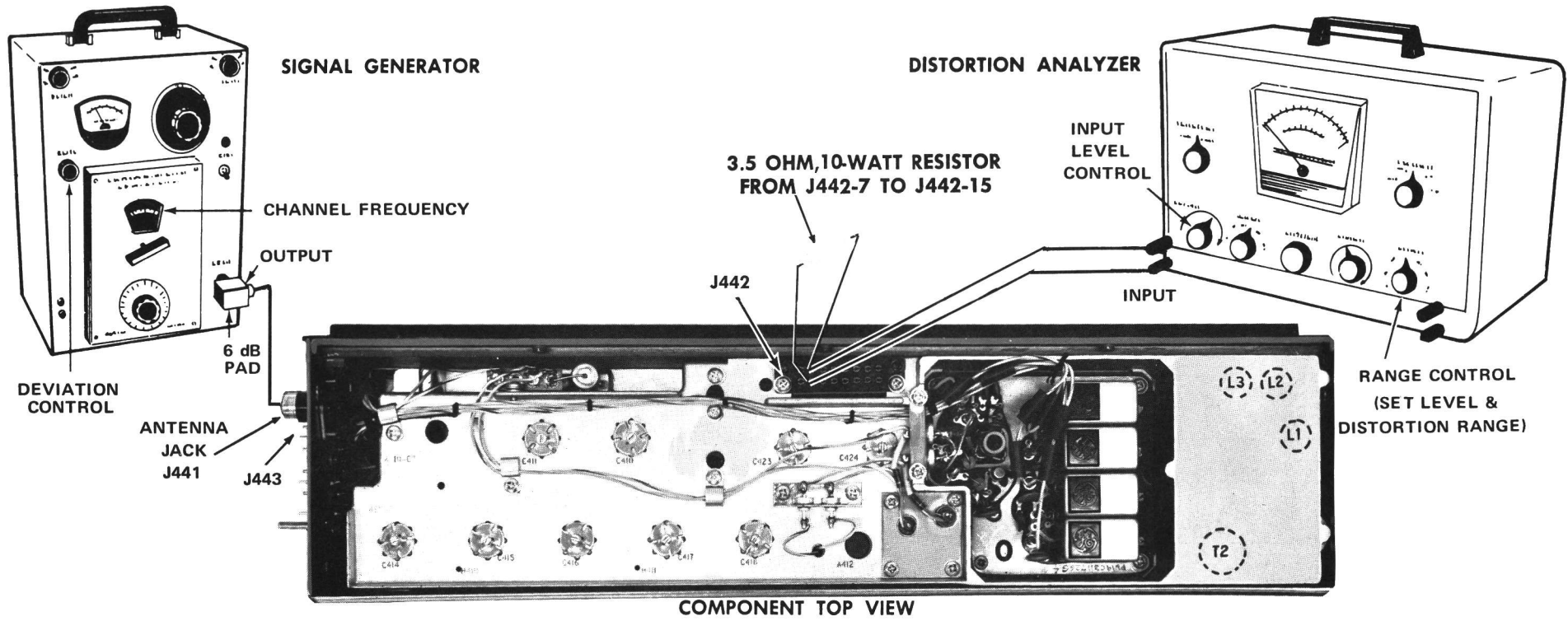
the defective stage is pin-pointed, refer to the "Service Check" listed to correct the problem. Additional corrective measures are included in the Troubleshooting Procedure. Before starting with the Receiver Test Procedures, be sure the receiver is tuned and aligned to the proper operating frequency.

TEST EQUIPMENT REQUIRED

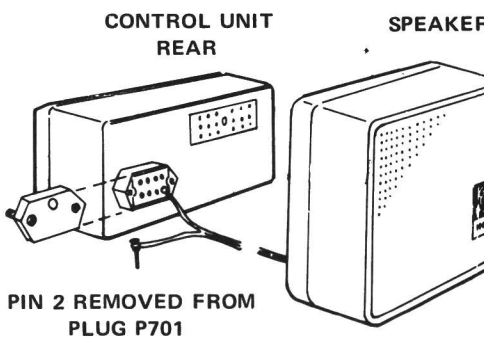
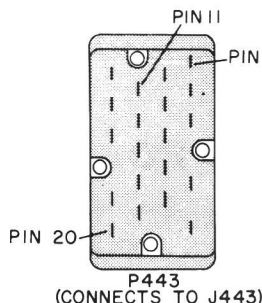
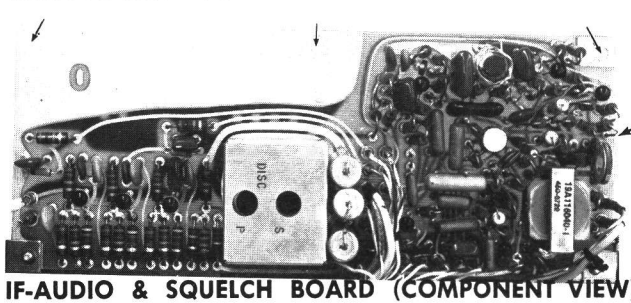
- Distortion Analyzer similar to: Heath IM-12
- Signal Generator similar to: Measurements M-560
- 6-dB attenuation pad, and 3.5-ohm, 10-watt resistor

PRELIMINARY ADJUSTMENTS

1. Connect the test equipment to the receiver as shown for all steps of the receiver Test Procedure.
2. Turn the SQUELCH control fully clockwise for all steps of the Test Procedure.
3. Turn on all of the equipment and let it warm up for 20 minutes.



REMOVE THREE SCREWS AND SWING BOARD OPEN-



STEP 1
AUDIO POWER OUTPUT
AND DISTORTION

TEST PROCEDURE

Measure Audio Power Output as follows:

- A. Apply a 1,000-microvolt, on-frequency test signal modulated by 1,000 hertz with ± 3.0 kHz deviation to antenna jack J441.
- B. With Five-Watt Speaker:

Disconnect speaker lead pin from J701-2 (on rear of Control Unit).

Connect a 3.5-ohm load resistor from J442-15 to J442-7. Connect the Distortion Analyzer input across the resistor as shown.

OR

With Handset:

Lift the handset off of the hookswitch. Connect the Distortion Analyzer input from J442-15 to J442-7.

- C. Adjust the VOLUME control for five-watt output (4.18 VRMS using the Distortion Analyzer as a VTVM).
- D. Make distortion measurements according to manufacturer's instructions. Reading should be less than 5%. If the receiver sensitivity is to be measured, leave all controls and equipment as they are.

SERVICE CHECK

If the distortion is more than 5%, or maximum audio output is less than five watts, make the following checks:

- E. Battery and regulator voltage---low voltage will cause distortion. (Refer to Receiver Schematic Diagram for voltages.)
- F. P.A. Bias Adjust (R43) -- Turn the SQUELCH control fully counterclockwise.

Then connect a milliammeter in series with the +12 volt lead at P443-11. With no signal in, adjust R43 for a reading of approximately 20 milliamps. This adjustment should not be necessary unless an output transistor has been replaced.

- G. Audio Gain (Refer to Receiver Troubleshooting Procedure).
- H. Discriminator Alignment (Refer to Receiver Alignment on reverse side of page).

STEP 2
USABLE SENSITIVITY
(12-dB SINAD)

If STEP 1 checks out properly, measure the receiver sensitivity as follows:

- A. Apply a 1000-microvolt, on-frequency signal modulated by 1000 Hz with 3.0-kHz deviation to J441.
- B. Place the RANGE switch on the Distortion Analyzer in the 200 to 2000-Hz distortion range position (1000-Hz filter in the circuit). Tune the filter for minimum reading or null on the lowest possible scale (100%, 30%, etc.)
- C. Place the RANGE switch to the SET LEVEL position (filter out of the circuit) and adjust the input LEVEL control for a +2 dB reading on a mid range (30%).
- D. While reducing the signal generator output, switch the RANGE control from SET LEVEL to the distortion range until a 12-dB difference (+2 dB to -10 dB) is obtained between the SET LEVEL and distortion range positions (filter out and filter in).
- E. The 12-dB difference (Signal plus Noise and Distortion to noise plus distortion ratio) is the "usable" sensitivity level. The sensitivity should be less than rated 12 dB SINAD specification with an audio output of at least 2.5 watts (2.9 volts RMS across the 3.5-ohm receiver load using the Distortion Analyzer as a VTVM).

- F. Leave all controls as they are and all equipment connected if the Modulation Acceptance Bandwidth test is to be performed.

SERVICE CHECK

If the sensitivity level is more than rated 12 dB SINAD, check the alignment of the RF stages as directed in the Alignment Procedure, and make the gain measurements as shown on the Troubleshooting Procedure.

STEP 3
MODULATION ACCEPTANCE
BANDWIDTH (IF BANDWIDTH)

If STEPS 1 and 2 check out properly, measure the bandwidth as follows:

- A. Set the Signal Generator output for twice the microvolt reading obtained in the 12-dB SINAD measurement.
- B. Set the RANGE control on the Distortion Analyzer in the SET LEVEL position (1000-Hz filter out of the circuit), and adjust the input LEVEL control for a +2 dB reading on the 30% range.
- C. While increasing the deviation of the Signal Generator, switch the RANGE control from SET LEVEL to distortion range until a 12-dB difference is obtained between the SET LEVEL and distortion range readings (from +2 dB to -10 dB).
- D. The deviation control reading for the 12-dB difference is the Modulation Acceptance Bandwidth of the receiver. If should be more than ± 7.5 kHz (but less than ± 9.5 kHz).

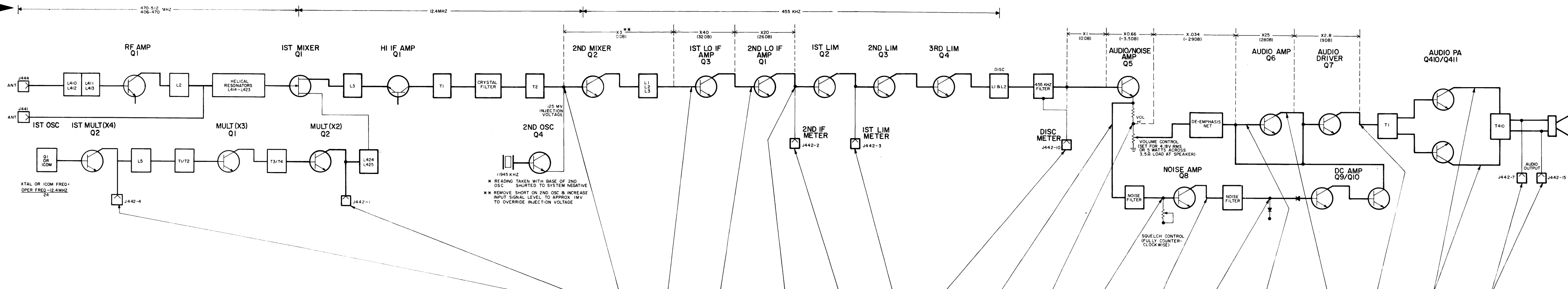
SERVICE CHECK

If the Modulation Acceptance Bandwidth test does not indicate the proper width, make gain measurements as shown on the Receiver Troubleshooting Procedure.

Metering Position	Reading with No Signal in	Reading with 1 μ v unmodulated input
A Disc idling	Less than ± 0.05 VDC	
B 2nd IF	.05 VDC	0.2 VDC
C 1st Lim	0.6 VDC	0.8 VDC
D Mult 1	1.0 VDC	
G Mult 2	0.3 VDC	
J Regulated +10 Volts	10 VDC	

SYMPTOM	PROCEDURE
NO SUPPLY VOLTAGE	<ul style="list-style-type: none"> ● Check power connections and continuity of supply leads, and check fuse in power supply. If fuse is blown, check receiver for short circuits.
NO REGULATED 10-VOLTS	<ul style="list-style-type: none"> ● Check the 12-volt supply. Then check regulator circuit (See Troubleshooting Procedure for Power Supply).
LOW 1ST LIM READING	<ul style="list-style-type: none"> ● Check supply voltages and then check oscillator reading at J442-4 & 5 as shown in STEP 2A. ● Make SIMPLIFIED VTVM GAIN CHECKS from 2nd Mixer through 1st Limiter stages as shown in STEP 2A.
LOW OSCILLATOR/MULTIPLIER READINGS	<ul style="list-style-type: none"> ● Check alignment of Oscillator (Refer to Front End Alignment Procedure). ● Check voltage readings of 1st Oscillator/Multiplier Q1/Q2. ● Check crystal Y1.
LOW RECEIVER SENSITIVITY	<ul style="list-style-type: none"> ● Check Front End Alignment (Refer to Receiver Alignment Procedure). ● Check antenna connections, cable and relay. ● Check 1st and 2nd Oscillator injection voltage. ● Check voltage readings of RF Amp, 1st Mixer and HI IF Amp. ● Make SIMPLIFIED GAIN CHECKS (STEP 2A).
LOW AUDIO	<ul style="list-style-type: none"> ● Check Audio PA (Q410 & Q411) voltage readings on schematic diagram. ● Make simplified gain and waveform checks of audio and squelch stages (Steps 2A and 2B). ● Make unsquelched voltage readings in Audio section (Refer to Receiver Schematic Diagram). ● Check voltage readings on Channel Guard board.
HIGH DISTORTION AT LOW AUDIO LEVELS (50 MW)	<ul style="list-style-type: none"> ● Set PA bias adjust R43 as specified under Service checks in STEP 1 of TEST PROCEDURES.
IMPROPER SQUELCH OPERATION	<ul style="list-style-type: none"> ● Check voltage readings of Squelch circuit (Refer to Receiver Schematic Diagram). ● Make gain and waveform checks of audio and squelch stages (Steps 2A and 2B).
DISCRIMINATOR IDLING TOO FAR OFF ZERO	<ul style="list-style-type: none"> ● See if discriminator zero is in center of IF bandpass.

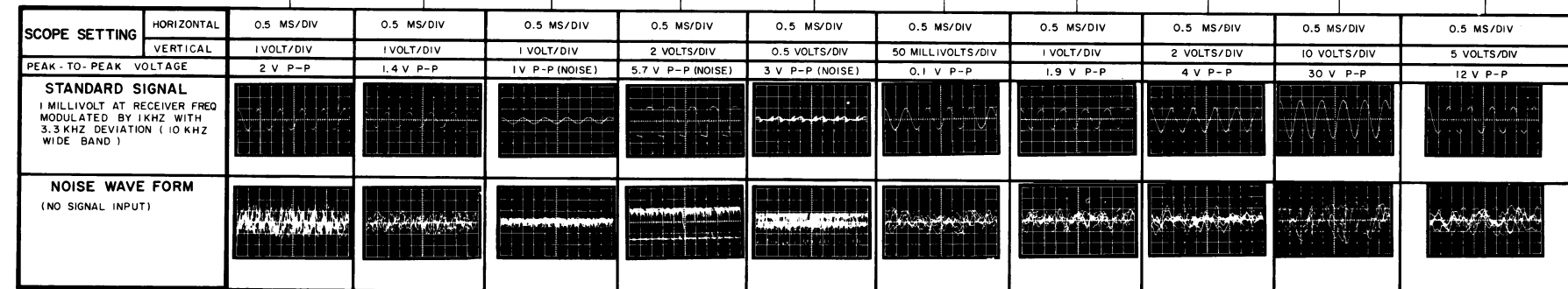
4. Check results with typical voltage ratios shown on diagram.



1. Set VOLUME control for 4.18 volts across 3.5-ohm load. If this cannot be obtained, set to approx. 70% of max. rotation.
2. Set SQUELCH control fully counterclockwise.
3. Receiver should be properly aligned.
4. Connect VTVM between system negative and points indicated by arrow (except for 1st MULT which references chassis ground).

[illegible]

1. Set VOLUME control for 4.18 volts across 3.5-ohm load. If this cannot be obtained, set to approx 70% of max. rotation.
2. Set SQUELCH control fully counterclockwise.
3. Receiver should be properly aligned.
4. Connect oscilloscope between system negative and points indicated by arrow.



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PARTS LIST		
LB14021K		
406-470 MHz RECEIVERS 4R4A2E10-33, 4R4A2010-33		
SYMBOL	GE PART NO.	DESCRIPTION
A410* and A411*		RF AMPLIFIER 19C320697G1
----- CAPACITORS -----		
C1	5496218P45	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef 0 PPM.
C3	5493392P105	Ceramic, stand-off: 220 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type SS5D.
C4	5493392P5	Ceramic, feed-thru: 220 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type FASC.
----- TERMINALS -----		
E1 and E2	19B209055P8	Terminal, feed-thru: sim to Electrical Industries ABAS40WS.
E3	19B209055P1	Terminal, feed-thru: sim to Electrical Industries ABAS-40W-RR.
E4	19B209055P8	Terminal, feed-thru: sim to Electrical Industries ABAS40WS.
----- TRANSISTORS -----		
Q1	19A116859P1	Silicon, NPN; sim to Type 2N5032 or 2N3570.
----- RESISTORS -----		
R1	3R152P10J	Composition: 10K ohms ±5%, 1/4 w.
R2	3R152P27J	Composition: 2.7K ohms ±5%, 1/4 w.
R3	3R152P821J	Composition: 820 ohms ±5%, 1/4 w.
R4	3R152P301J	Composition: 390 ohms ±5%, 1/4 w.
A410* and A411*		In 19B500881G3 REV G-M; In 19B500881G4 REV G-M; 19C317950G1
----- CAPACITORS -----		
C1*	19A116114P43	Ceramic: 27 pf ±10%, 100 VDCW; temp coef 0 PPM.
C2	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.
C3	5493392P5	Ceramic, stand-off: 220 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type SS5D.
C4 thru C6	5493392P107	Ceramic, stand-off: 1000 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type SS5D.
L1 and L2	19B209420P1	Coil, RF: 0.10 µh ±5%, 0.08 ohms DC res max; sim to Jeffers 4416-J.
L3 thru L5	19A116632P1	Toroidal core.
----- INDUCTORS -----		
Q1	19A116154P1	N Channel, field effect.
----- RESISTORS -----		
R1 and R2	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
----- INDUCTORS -----		
L1	19A127430G1	Choke.

SYMBOL	GE PART NO.	DESCRIPTION
A410* and A411*		In REV F and earlier: RF AMPLIFIER A410 19C317975G1 (406-420 MHz) A411 19C317975G2 (450-470 MHz)
----- CAPACITORS -----		
C1	5493392P107	Ceramic, stand-off: 1000 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type SS5D.
C2	7484398P3	Silver mica: 250 pf ±10%, 500 VDCW; sim to Underwood Type 21R7.
C3	5493392P7	Ceramic, feed-thru: 1000 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type FASC.
C4	5493392P107	Ceramic, stand-off: 1000 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type SS5D.
C5	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.
C6	5491601P124	Phenolic: 1.8 pf ±5%, 500 VDCW.
C7	7484389P1	Variable 1.5-7 pf, temp coef 0 PPM; sim to Erie Style 503.
C8	5491601P122	Phenolic: 1.2 pf ±5%, 500 VDCW.
----- TERMINALS -----		
E1	19B209055P1	Terminal: sim to Electrical Industries ABAS-40W-RR.
----- INDUCTORS -----		
L1	19B209420P1	Coil, RF: 0.10 µh ±5%, 0.08 ohms DC res max; sim to Jeffers 4416-J.
L2	19A127429P1	Coil.
L3	19A127429P2	Coil.
----- TRANSISTORS -----		
Q1	19A116154P1	N Channel, field effect.
----- RESISTORS -----		
R1 and R2	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
R3	3R152P470K	Composition: 47 ohms ±10%, 1/4 w.
A412		FIRST MIXER ASSEMBLY 19C317974G1
----- CAPACITORS -----		
C1	5496218P312	Ceramic disc: 18 pf ±10%, 500 VDCW, temp coef -150 PPM.
C2		(Part of L3).
C3*	5496218P344	Ceramic disc: 15 pf ±5%, 500 VDCW, temp coef -80 PPM.
C4	5496218P249	In 19B500881G1 of REV L and earlier: In 19B500881G2 of REV M and earlier: In 19B500881G3 of REV P and earlier: In 19B500881G4 of REV R and earlier:
C5	5493392P107	Ceramic, stand-off: 1000 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type SS5D.
C6	19A116080P1	Polyester: 0.01 µf ±20%, 50 VDCW.
C7	5493392P107	Ceramic, stand-off: 1000 pf ±100% -0%, 500 VDCW; sim to Allen-Bradley Type SS5D.
C8		(Part of L3).
----- TERMINALS -----		
E1 and E2	19B209055P8	Terminal, feed-thru: sim to Electrical Industries ABAS40WS.
----- INDUCTORS -----		
L1	19A127430G1	Choke.

SYMBOL	GE PART NO.	DESCRIPTION
L2		(Part of L3).
L3	19B216440G1	Coil assembly, includes:
C2	5496218P249	Ceramic disc: 27 pf ±5%, 500 VDCW, temp coef -80 PPM.
C8*	19A116114P12	Ceramic: 3.3 pf ±5%, 100 VDCW. Added to 19B500881G1, G3 by REV J, G4 by REV K.
L2	19B209420P113	Coil, RF: 1 µh ±10%, 0.74 ohms DC res max; sim to Jeffers 4426-6.
	5491798P8	Tuning slug.
----- TRANSISTORS -----		
Q1*	19A116960P1	N Type, field effect; sim to Type 2N4416.
		In 19B500881G1 of REV M and earlier: In 19B500881G2 of REV N and earlier: In 19B500881G3 of REV P and earlier: In 19B500881G4 of REV R and earlier:
	19A116154P1	N Channel, field effect.
----- RESISTORS -----		
R1	3R152P302J	Composition: 3000 ohms ±5%, 1/4 w.
R2 and R3	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
A413 and A414		MULTIPLIER BOARD ASSEMBLY A413 19B213360G1 A414 19B213360G2
----- CAPACITORS -----		
C1	19A116655P12	Ceramic disc: 330 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C2		(Part of T1).
C3		(Part of T2).
C4	5496203P149	Ceramic disc: 220 pf ±10%, 500 VDCW, temp coef -3300 PPM.
C5		(Part of T3).
C6		(Part of T4).
C7		(Part of T4).
C8*	5494481P107	Ceramic disc: 470 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap. Deleted by REV E.
C10	5496203P149	Ceramic disc: 220 pf ±10%, 500 VDCW, temp coef -3300 PPM.
C11	5496218P245	Ceramic disc: 18 pf ±5%, 500 VDCW, temp coef -80 PPM.
C12	5494481P107	Ceramic disc: 470 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.
C13	19A116655P13	Ceramic disc: 470 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.
C14	5496218P548	Ceramic disc: 24 pf ±5%, 500 VDCW, temp coef -330 PPM.
C15*	5494481P7	Ceramic disc: 470 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap. Added by REV C.
----- INDUCTORS -----		
L1		(Part of T1 and T2).
L2		(Part of T3 and T4).
L3	19B209420P1	Coil, RF: 0.10 µh ±5%, 0.08 ohms DC res max; sim to Jeffers 4416-J.
L4		(Part of T1).
----- TRANSISTORS -----		
Q1*	19A115329P2	Silicon, NPN.
		Earlier than REV C:
	19A116059P1	Silicon, NPN.
	19A115991P1	Silicon, NPN.
Q2		
----- CAPACITORS -----		
	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.

SYMBOL	GE PART NO.	DESCRIPTION
----- RESISTORS -----		
R1	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
R2	3R152P181J	Composition: 180 ohms ±5%, 1/4 w.
R3	3R152P100K	Composition: 10 ohms ±10%, 1/4 w.
R4	3R152P471K	Composition: 470 ohms ±10%, 1/4 w.
R5	3R152P480J	Composition: 68 ohms ±5%, 1/4 w.
R6	3R152P273K	Composition: 27K ohms ±10%, 1/4 w.
R7*	3R152P100K	Composition: 10 ohms ±10%, 1/4 w. Added by REV C.
T1 and T2		COIL ASSEMBLY T1 19B216373G1 T2 19B216373G2
----- CAPACITORS -----		
C2	5496218P350	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -150 PPM.
C3	5496218P248	Ceramic disc: 24 pf ±5%, 500 VDCW, temp coef -80 PPM.
----- INDUCTORS -----		
L1	19B216373P5	Coil.
L4	19B209420P1	Coil, RF: 0.10 µh ±5%, 0.08 ohms DC res max; sim to Jeffers 4416-J.
	19B209674P26	Tuning slug.
T3 and T4		COIL ASSEMBLY T3 19B216374G1 T4 19B216374G2
----- CAPACITORS -----		
C5*	5496218P237	Ceramic disc: 6.0 pf ±0.25 pf, 500 VDCW, temp coef -80 PPM.
	5496218P439	Ceramic disc: 8 pf ±0.25 pf, 500 VDCW, temp coef -220 PPM.
C6*	5496218P237	Ceramic disc: 6.0 pf ±0.25 pf, 500 VDCW, temp coef -80 PPM.
	5496218P436	Ceramic disc: 5 pf ±0.25 pf, 500 VDCW, temp coef -220 PPM.
	5496218P437	Ceramic disc: 6 pf ±0.25 pf, 500 VDCW, temp coef -220 PPM.
C7*	5496218P746	Ceramic disc: 20 pf ±5%, 500 VDCW, temp coef -750 PPM.
	5496218P750	Ceramic disc: 30 pf ±5%, 500 VDCW, temp coef -750 PPM.
C8*	5496218P246	Ceramic disc: 20 pf ±5%, 500 VDCW, temp coef -80 PPM.
	5496218P748	In REV A thru G: Ceramic disc: 24 pf ±5%, 500 VDCW, temp coef -750 PPM.
	5496218P749	Earlier than REV A: Ceramic disc: 27 pf ±5%, 500 VDCW, temp coef -750 PPM.
L2	19B216374P5	Coil.
	19B209674P26	Tuning slug.
A415 thru A420		FIRST OSCILLATOR ASSEMBLY A415 19B204419G19 A416 19B204419G20 A417 19B204419G21 A418 19B204419G22 A419 19B204419G23 A420 19B204419G24
C1 thru C4	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.

SYMBOL	GE PART NO.	DESCRIPTION
C5 thru C8	5496219P751	Ceramic disc: 33 pf ±5%, 500 VDCW, temp coef -750 PPM.
C9 thru C13	5491271P106	Variable, subminiature: approx 2.1-12.7 pf, 750 v peak; sim to EF Johnson 189.
C13 thru C16	5496219P40	Ceramic disc: 9 pf ±0.25 pf, 500 VDCW, temp coef 0 PPM.
C17 thru C20	19C300685P93	Ceramic disc: 5 pf ±0.1 pf, 500 VDCW, temp coef 0 PPM.
C23	5494481P114	Ceramic disc: 2000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C26	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C28	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C31	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C38	5491601P123	Phenolic: 1.5 pf ±5%, 500 VDCW; sim to Quality Components Type MC.
C39	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C40		(Part of T7).
C41		(Part of T8).
C42	5491601P130	Phenolic: 3.3 pf ±5%, 500 VDCW; sim to Quality Components Type MC.
C43	5496219P53	Ceramic disc: 39 pf ±5%, 500 VDCW, temp coef 0 PPM.
C44	5490008P135	Silver mica: 220 pf ±10%, 500 VDCW; sim to Electro Motive Type DM-15.
C45	5490008P35	Silver mica: 220 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C46	5496219P563	Ceramic disc: 100 pf ±5%, 500 VDCW, temp coef -330 PPM.
C47	5496219P767	Ceramic disc: 150 pf ±5%, 500 VDCW, temp coef -750 PPM.
----- DIODES AND RECTIFIERS -----		
CW1 thru CW4	19A115603P1	Silicon.
CW6	19A115250P1	Silicon.
----- JACKS AND RECEPTACLES -----		
J1 thru J6	4033513P4	Contact, electrical: sim to Bead Chain L93-3.
J15 and J16	4033513P4	Contact, electrical: sim to Bead Chain L93-3.
----- INDUCTORS -----		
L2 and L3	7488079P16	Choke, RF: 10 µh ±10% ind at 640 ma, 0.6 ohm DC res; sim to Jeffers 4421-7K.
L5		(Part of T7 and T8).
----- TRANSISTORS -----		
Q1 and Q2	19A115330P1	Silicon, NPN.
R1 thru R4	3R152P562J	Composition: 5600 ohms ±5%, 1/4 w.
R5 thru R8	3R152P104K	Composition: 0.1 megohm ±10%, 1/4 w.
R9	3R152P153J	Composition: 15,000 ohms ±5%, 1/4 w.
R10	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
----- CAPACITORS -----		
	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.

SYMBOL	GE PART NO.	DESCRIPTION
R11 and R12	3R152P102J	Composition: 1K ohms ±5%, 1/4 w.
R13	3R152P151J	Composition: 150 ohms ±5%, 1/4 w.
R14	3R152P103J	Composition: 10K ohms ±5%, 1/4 w.
R15	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
R17 and R18	3R152P103K	Composition: 10K ohms ±10%, 1/4 w.
R20	3R152P270K	Composition: 27 ohms ±10%, 1/4 w.
RT5 thru RT8	19B209284P7	Disc: 62 ohms res nominal at 25°C, color code violet.
RT9	19B209284P8	Disc: 94S ohms res nominal at 25°C, color code gray.
T7 and T8		COIL ASSEMBLY T7 19B2044850G1 T8 19B2044850G2
----- CAPACITORS -----		
C40	5496218P253	Ceramic disc: 39 pf ±5%, 500 VDCW, temp coef -80 PPM.
C41	5496218P251	Ceramic disc: 33 pf ±5%, 500 VDCW, temp coef -80 PPM.
L5	19A121728P1	Coil.
	19B209674P26	Tuning slug.
----- SOCKETS -----		
XY1 thru XY4		Refer to Mechanical Parts (MC1823).
----- CRYSTALS -----		
		NOTE: When reordering give GE Part No. and specify exact freq needed.
CW1 thru CW4	19A115603P1	Silicon.
Y1 thru Y4	19B206576P6	Quartz: freq range 15175.000 to 17925.000 KHz, temp range -30°C to +85°C. (400-450 MHz)
Y1 thru Y4	19B206576P7	Quartz: freq range 17925.001 to 20685.000 KHz, temp range -30°C to +85°C. (450-470 MHz)
A421		IF AMPLIFIER ASSEMBLY 19B216356G1
C1	19A116655P19	Ceramic disc: 1000 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.
C2*	7489162P21	Silver mica: 56 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C3	5490008P21	In 19B500881G1, G3 of REV H and earlier: In 19B500881G2, G4 of REV J and earlier: Silver mica: 56 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C4	5494481P11	Ceramic disc: 1000 pf ±20%, 1000 VDCW; sim to RMC Type JF Discap.
C5 and C6	19A116080P5	Polyester: 0.047 µf ±20%, 50 VDCW.
C7 and C8	19A116080P5	Polyester: 0.01 µf ±20%, 50 VDCW.
C9	5490008P25	Silver mica: 82 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C10	5490008P19	Silver mica: 47 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C11	5496219P656	Ceramic disc: 13 pf ±5%, 500 VDCW, temp coef 0 PPM.
C12	5494481P108	Ceramic disc: 470 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C13	19A115680P107	Electrolytic: 100 µf ±10% -10%, 15 VDCW; sim to Mallory Type TTX.
C14 and C15	19A115680P104	Electrolytic: 50 µf ±10% -10%, 25 VDCW; sim to Mallory Type TTX.
C16	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C17	19A116080P7	Polyester: 0.1 µf ±20%, 50 VDCW.
C18	5494481P108	Ceramic disc: 470 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.

SYMBOL	GE PART NO.	DESCRIPTION
----- RESISTORS -----		
R1	3R152P301J	Composition: 300 ohms ±5%, 1/4 w.
R2	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
R3*	3R152P152J	Composition: 1.5K ohms ±5%, 1/4 w.
		In 19B500881G1, G3 of REV K and earlier: In 19B500881G2, G4 of REV L and earlier:
	3R152P302J	Composition: 3K ohms ±5%, 1/4 w.
R4	3R152P682J	Composition: 6.8K ohms ±5%, 1/4 w.
R5	3R152P101K	Composition: 100 ohms ±10%, 1/4 w.
R6	3R152P301J	Composition: 300 ohms ±5%, 1/4 w.
----- TRANSFORMERS -----		
T1	19B216372G1	Coil assembly. Includes:
	5491798P7	Tuning slug.
A422		CRYSTAL FILTER ASSEMBLY 19B204610G8
----- FILTERS -----		
FL7	19C304358G1	Bandpass filter.
----- RESISTORS -----		
R10	3R152P512J	Composition: 5.1K ohms ±5%, 1/4 w.
R11	3R152P332K	Composition: 3.3K ohms ±10%, 1/4 w.
A424		SECOND MIXER ASSEMBLY 19B216119G3
----- CAPACITORS -----		
C2	19A116080P7	Polyester: 0.1 µf ±20%, 50 VDCW.
C3	5494481P112	Ceramic disc: 1000 pf ±10%, 1000 VDCW; sim to RMC Type JF Discap.
C7 and C8	19A116080P5	Polyester: 0.047 µf ±20%, 50 VDCW.
C9	5496219P369	Ceramic disc: 180 pf ±5%, 500 VDCW, temp coef -150 PPM.
C10	19A116080P7	Polyester: 0.1 µf ±20%, 50 VDCW.
C12	5496219P369	Ceramic disc: 180 pf ±5%, 500 VDCW, temp coef -150 PPM.
C14	19A116656P220J2	Ceramic disc: 220 pf ±5%, 500 VDCW, temp coef -220 PPM.
C15	7491395P109	Ceramic disc: 1000 pf ±10%, 500 VDCW; sim to RMC Type JL.
C16	19A116080P5	Polyester: 0.047 µf ±20%, 50 VDCW.
C17	19A116080P1	Polyester: 0.01 µf ±20%, 50 VDCW.
C18	5490008P25	Silver mica: 82 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C19	5490008P19	Silver mica: 47 pf ±5%, 500 VDCW; sim to Electro Motive Type DM-15.
C20	5490008P1	Silver mica: 5 pf ±0.5%, 500 VDCW; sim to Electro Motive Type DM-15.
C23		(Part of T2).
C24 and C25	5496219P43	Ceramic disc: 13 pf ±5%, 500 VDCW, temp coef 0 PPM.
----- JACKS AND RECEPTACLES -----		
J1	4033513P4	Contact, electrical: sim to Bead Chain L93-3.
----- INDUCTORS -----		
L1	19C311181G3	Coil assembly.
L2 and L3	19A115711P1	Transformer, freq: 455 KHz; sim to Automatic Mfg EX12670.
----- PLUGS -----		
P1	4029840P2	Contact, electrical: sim to Amp 42827-2.
P2	4029840P1	Contact, electrical: sim to Amp 41854.

MODELS WITH DISCRETE CIRCUIT OSCILLATOR	MODELS WITH ICOM OSCILLATOR	NO. OF	FREQ. RANGE	CHANNEL	U. S. S. RECEIVER
			406-420+LO	GUARD	A410/A411
			450-470+HI		PRESENT
4ER42E10	4ER42G10	1	LO		
4ER42E11	4ER42G11	1	HI		
4ER42E12		2	LO		
4ER42E13		2	HI		
4ER42E14	4ER42G14	4	LO		
4ER42E15	4ER42G15	4	HI		
4ER42E16	4ER42G16	1	LO	X	
4ER42E17	4ER42G17	1	HI	X	
4ER42E18		2	LO	X	
4ER42E19		2	HI	X	
4ER42E20	4ER42G20	4	LO	X	
4ER42E21	4ER42G21	4	HI	X	
4ER42E22	4ER42G22	1	LO		X
4ER42E23	4ER42G23	1	HI		X
4ER42E24		2	LO	X	
4ER42E25		2	HI	X	
4ER42E26	4ER42G26	4	LO	X	
4ER42E27	4ER42G27	4	HI	X	
4ER42E28	4ER42G28	1	LO	X	X
4ER42E29	4ER42G29	1	HI	X	X
4ER42E30		2	LO	X	X
4ER42E31		2	HI	X	X
4ER42E32	4ER42G32	4	LO	X	X
4ER42E33	4ER42G33	4	HI	X	X

IN ORDER TO RETAIN RATED EQUIPMENT PERFORMANCE, REPLACEMENT OF ANY SERVICE PART SHOULD BE MADE ONLY WITH A COMPONENT HAVING THE SPECIFICATIONS SHOWN ON THE PARTS LIST FOR THAT PART.

ALL RESISTORS ARE 1/2 WATT UNLESS OTHERWISE SPECIFIED AND RESISTOR VALUES IN OHMS UNLESS FOLLOWED BY K=1000 OHMS OR M=1,000,000 OHMS. CAPACITOR VALUES IN PICOFARADS (EQUAL TO MICRO/MICROFARADS) UNLESS FOLLOWED BY M= MICROFARADS. INDUCTANCE VALUES IN MICROHENRYS UNLESS FOLLOWED BY MH= MILLIHENRYS OR H=HENRYS.

VOLTAGE READINGS

VOLTAGE READINGS ARE TYPICAL READINGS MEASURED TO SYSTEM NEGATIVE (J442-B) WITH TEST SET MODEL 4EX3A10 OR A 2Q,000 OHM PER-VOLT METER.
S=NO SIGNAL IN WITH SQUELCH CONTROL FULLY COUNTERCLOCKWISE (MAXIMUM SQUELCH)
US=SQUELCH CONTROL FULLY CLOCKWISE WITH A ONE MILLIVOLT MODULATED SIGNAL (UNSQUELCHED) AND 5 WATT AUDIO OUTPUT.

NOTE:

TO CHECK FOR PROPER OPERATION OF 1ST MIXER A412, MEASURE CURRENT 10V CIRCUIT (W-R LEAD), CURRENT WITH FIRST OSC XTAL REMOVED SHOULD BE 0.6 TO 0.8 MA. CURRENT WITH FIRST OSC OPERATING PROPERLY, SHOULD BE 1.2 TO 1.6 MA.

● THESE ARE ONLY PARTS PRESENT ON A429.

▲ LOW SPLIT 406-420 MHZ

▲ HIGH SPLIT 450-470 MHZ

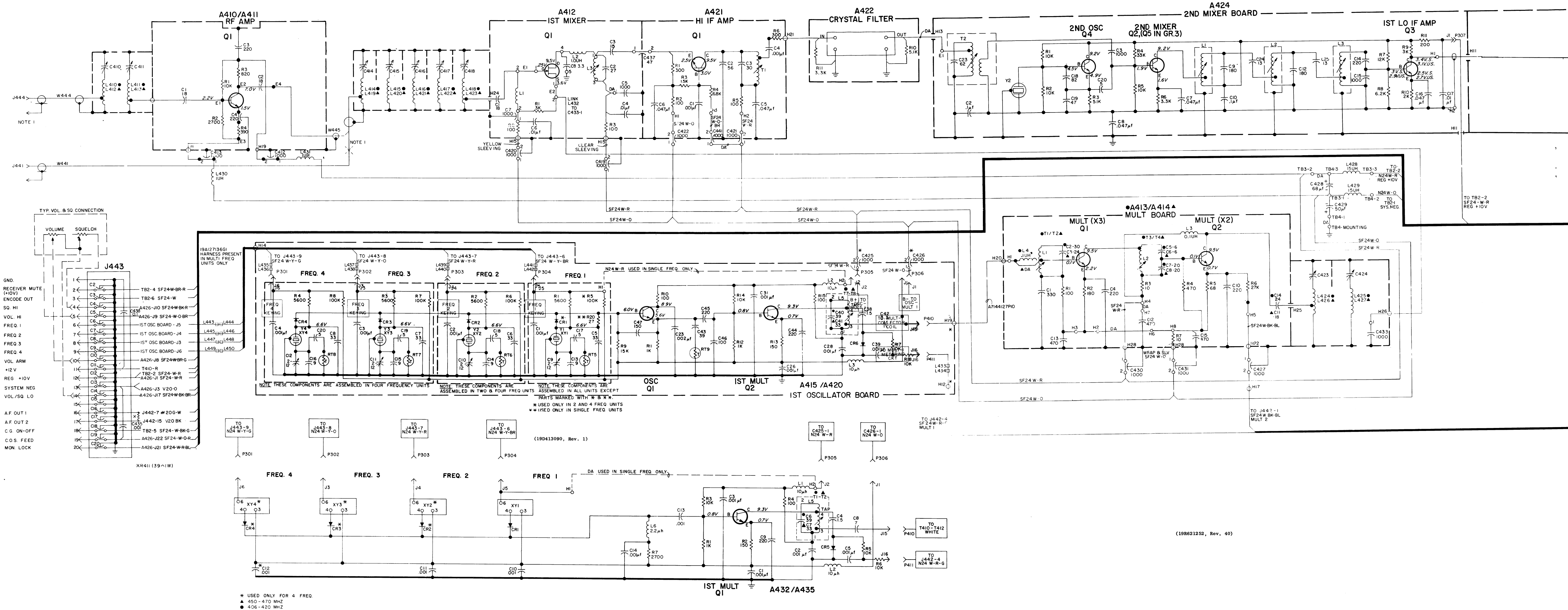
* LEADS TO BE TERMINATED AS SHORT AS POSSIBLE

■ VALUE OF A428-R47 IS DETERMINED BY TEST (SEE TEST SPEC 19A127182)

	REV
PL19E5008B1G1	N
PL19E5008B1G2	R
PL19E5008B1G3	A
PL19E5008B1G4	T
A424 PL19B216119G3	A
A426 PL19B413129G3	R
A428 4EK16A10	A
A429 PL19C311797G2	

SCHEMATIC DIAGRAM

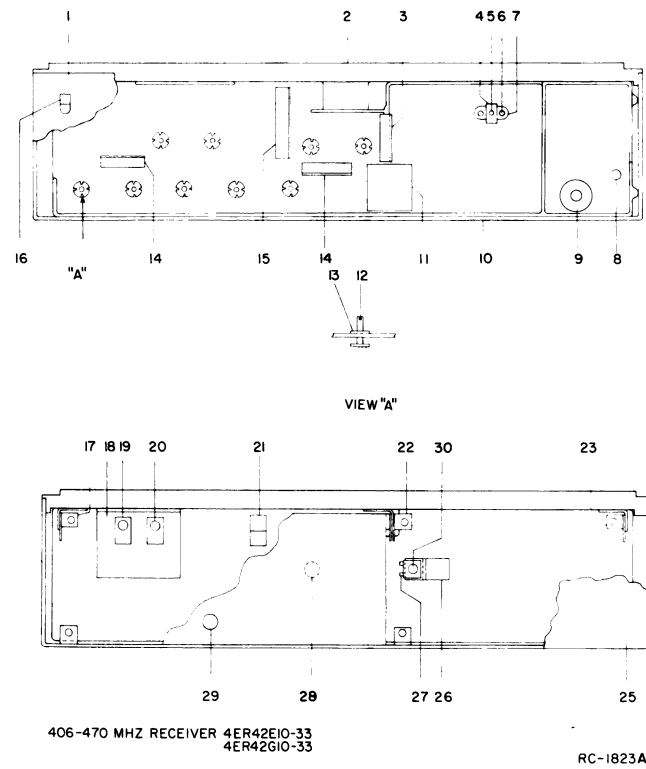
406—470 MHz RECEIVER
MODELS 4ER42E10-33 & 4ER42G10-33





14

SYMBOL	GE PART NO.	DESCRIPTION	SYMBOL	GE PART NO.	DESCRIPTION
P325	4029840P1	Contact, electrical: sim to Amp 41854.	3	19A121723P1	Support. (Mounts C425 and C426)
P326	4029840P2	Contact, electrical: sim to Amp 42827-2.	4	4033089P1	Clip, spring tension. (Part of XY1-XY4).
P327	4029840P1	Contact, electrical: sim to Amp 41854.	5	19B200525P9	Rivet. (Part of XY1-XY4).
P328 thru P335	4029840P2	Contact, electrical: sim to Amp 42827-2.	6	19A115793P1	Contact, electrical: sim to Malco 2700. (Part of XY1-XY4).
P410 and P411	4029840P2	Contact, electrical: sim to Amp 42827-2.	7	4039307P1	Crystal socket. (Part of XY1-XY4).
Q410* and Q411*	19A116741P1	Silicon, NPN. In 19E500881G1, G3 of REV B-K: In 19E500881G2, G4 of REV B-L:	8	4035306P40	Fiber washer. (Used with Y2 on A424).
	19A116203P2	Silicon, NPN.	9	4034252P5	Can. (Used with T1 on A424).
	19A115948P1	Earlier than REV B: Silicon, NPN.	10	19C303389G1	Chassis.
		----- RESISTORS -----	11	19A121722P1	Plate.
R410	19A116278P444	Metal film: 0.28 megohm $\pm 2\%$, 1/2 w.	12	4036765G4	Screw: 6-32. (Part of C410, C411, C414-C418, C423 and C424).
R411*	3R78P390K	Composition: 39 ohms $\pm 10\%$, 1 w. Added by REV B.	13	7137968P8	Nut, stamped: thd size No. 6-32; sim to Palnut T0632005. (Part of C410, C411, C414-C418, C423 and C424).
		----- TRANSFORMERS -----	14	19A121724P1	Support. (Mounts C419 and C420).
T410	19A116041P2	Audio freq: 300 to 4000 Hz, Pri: 1.00 ohm $\pm 15\%$ DC res. Sec 1: 0.23 ohm $\pm 10\%$ DC res. Sec 2: 10.5 ohms $\pm 15\%$ DC res.	15	19A127372P1	Support. (Mounts C427, C430 and C431).
		----- TERMINAL BOARDS -----	16	7145451P1	(Not Used).
TB1	7487424P2	Miniature, phen: 1 terminal.	17	19B204583G3	Hinge.
TB2	7487424P26	Miniature, phen: 6 terminals.	18	19B216727P1	Support. (Used with Q410 and Q411).
TB3 and TB4	7487424P24	Miniature, phen: 3 terminals.	19	19A116023P2	Plate, insulated. (Used with Q410 and Q411).
		----- CABLES -----	20	19A115222P3	Insulator, bushing. (Used with Q410 and Q411).
W441	19B205634G3	Coaxial cable: 50 ohm, approx 5 inches long. Includes (J441) 19B209122P3 connector.	21	4029851P6	Clip, loop: nylon, sim to Weckesser S/16-4-128.
W444	19B205634G7	Coaxial cable: 50 ohm, approx 7 inches long. Includes (J444) 19B209122P4 connector.	22	19B204583G1	Hinge.
W445	19A122550G1	RF: 50 ohm imp, approx 4 inches long.	23	19B204583G2	Hinge.
		HARNESSE ASSEMBLY 19E500881G9 (Includes C435, C436, C438-C440, J442, J443, L433, L434, P307-P313, P315-P317, P319, P320, P322-P327, P411, R410, R411, T410, TB2)	24	19A121676P1	Guide pin.
		MULTI-FREQUENCY MODIFICATION KIT 19A127096G1 and G2	25	19C303495G3	Top cover. (Station, except Repeaters and VM).
P301 thru P304	4029840P2	Harness assembly. Contact, electrical: sim to Amp 42827-2. (Part of 19A127136G1 Harness assembly).	26	19C303676G2	Top cover. (Station, Repeater and VM only).
L435 thru L440	19A115700P2	Bead, ferrite. (Part of 19A127136G1 Harness assembly).	27	19C303385G2	Top cover. (Mobile).
L443 thru L450	19A115700P2	Bead, ferrite.	28	19A121297P2	Angle.
		MECHANICAL PARTS (SEE RC-1823)	29	7160861P4	Nut, sheet spring: sim to Tinnerman C6452-82-67. (Used to secure cover).
1	19C303495G4	Bottom cover. (Station)	30	4036555P1	Insulator, disc. (Used with Q7 on A426).
	19C303385G1	Bottom cover. (Mobile)		4035267P2	Button, plug.
2	19C317344P3	Heat sink.		N115P1508C13	Screw, flathead, self tap: No. 8 x 1/2.



PRODUCTION CHANGES

Changes in the equipment to improve performance or to simplify circuits are identified by a "Revision Letter", which is stamped on the unit includes all previous revisions. Refer to the Parts List for description of parts affected by these revisions.

CHANNEL GUARD ENCODER/DECODER MODEL 4EK16A10

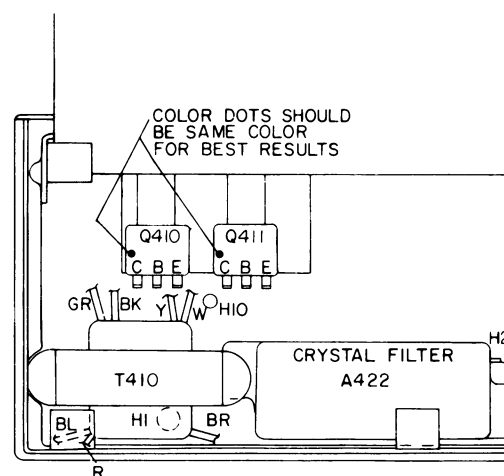
Rev. A - To obtain correct output level. Changed R8.

CHASSIS & RF ASSEMBLY 19E500881-G1 thru -G4

Rev. A - To facilitate tuning of low IF and improve critical squelch. Added C439 and C440. Changed C6 & C8 on A413/A414.

Rev. B - To incorporate new PA transistors. Changed Q410 and Q411. Added R411.

Outline Diagram Was:



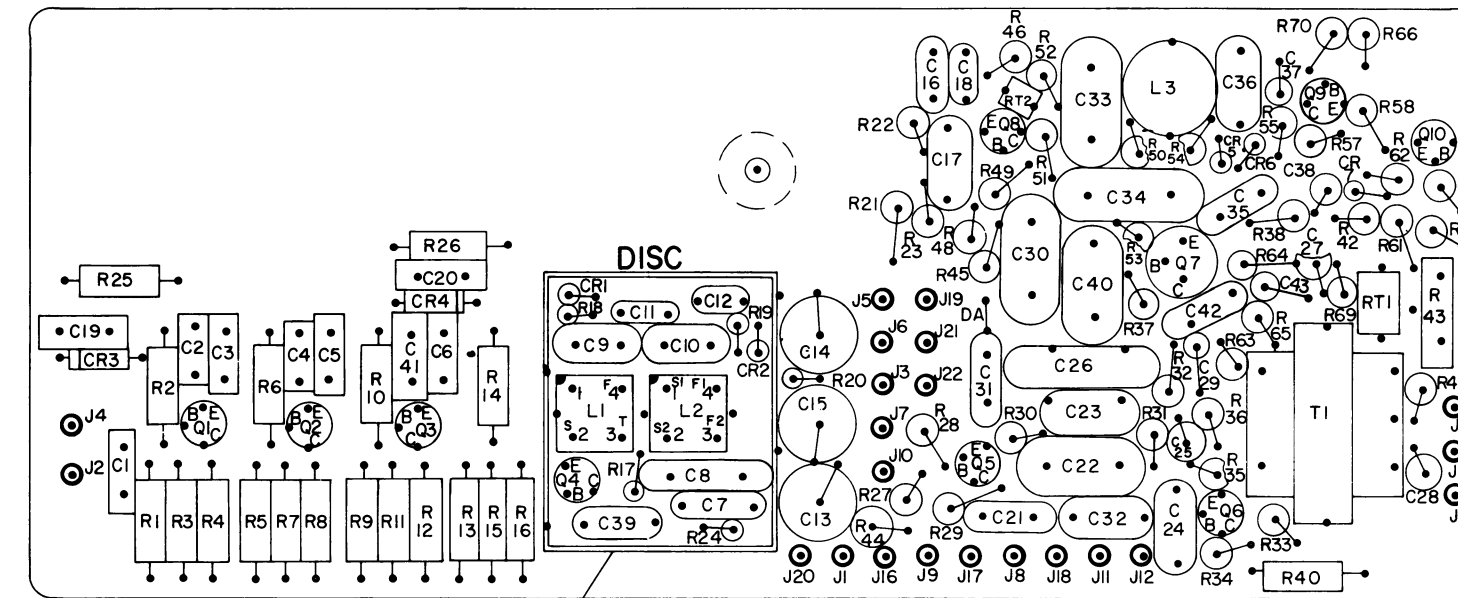
Rev. C - To incorporate a new multiplier transistor and decouple supply voltage. Changed Q1. Added C15 and R7.

IF AUDIO & SQUELCH BOARD A426 (19D413129-G3)

Rev. A - To make IF Audio & Squelch board compatible with new PA transistors and to improve squelch operation. Deleted C24, C28, C29, C42, C43, R32, R37, R63 and R65. Added C49-C54, CR8, R75-R79 and RT3. Changed C21, C26, C37, C38, C40, R33, R38, R39, R41 R42, R48, R53 and R62.

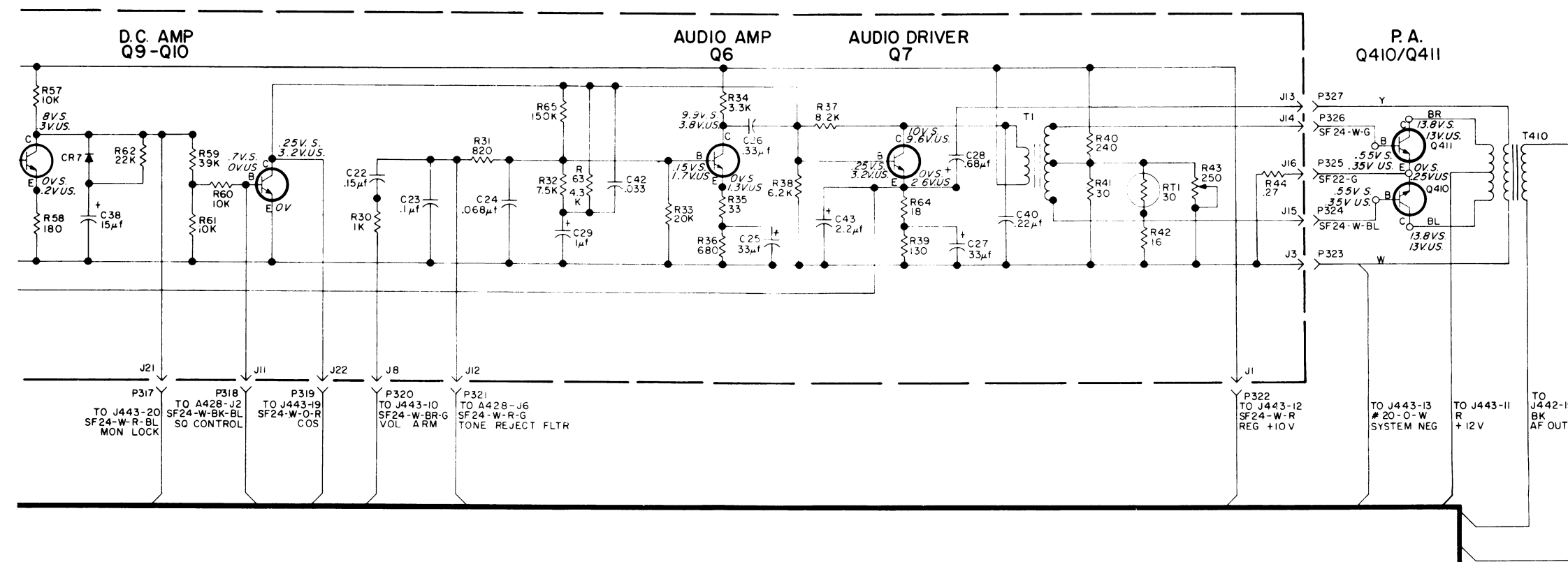
Outline Diagram Was:

IF-AUDIO & SQUELCH BOARD A426



Schematic Diagram Was:

IF AUDIO & SQUELCH BOARD A426



PRODUCTION CHANGES

406-470 MHz MASTR RECEIVER
MODELS 4ER42E10-33 & 4ER42G10-33

CHANNEL GUARD ENCODER/DECODER MODEL 4EK16A10

- Rev. B - To increase stop-band attenuation. Changed R8.
- Rev. C - To optimize frequency response. Changed C29.

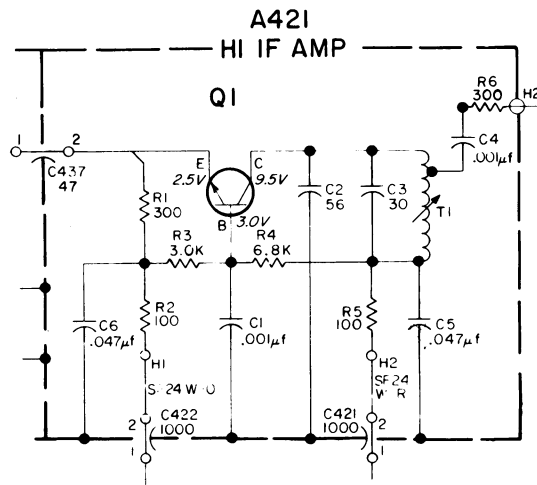
TONE REJECT FILTER 19C311797-G2

- Rev. A - To optimize frequency response. Changed C29.

CHASSIS & RF ASSEMBLY 19E500881-G1 thru -G4

- Rev. D - To eliminate squelch opening thump in receivers with Channel Guard. Removed white-orange wire between J443-13 and TB2-1. Added a white-orange wire between P312 (on J17 on IF audio and squelch board) and TB2-1.
- Rev. E - To stabilize the tripler stage. Removed C9 on A413/A414.
- Rev. F - To improve sensitivity when used with dual front-end. Added C441. Changed DC feed point of R4 to C441-2. Jumpered C441-1 to C421-1.

SCHEMATIC DIAGRAM WAS:

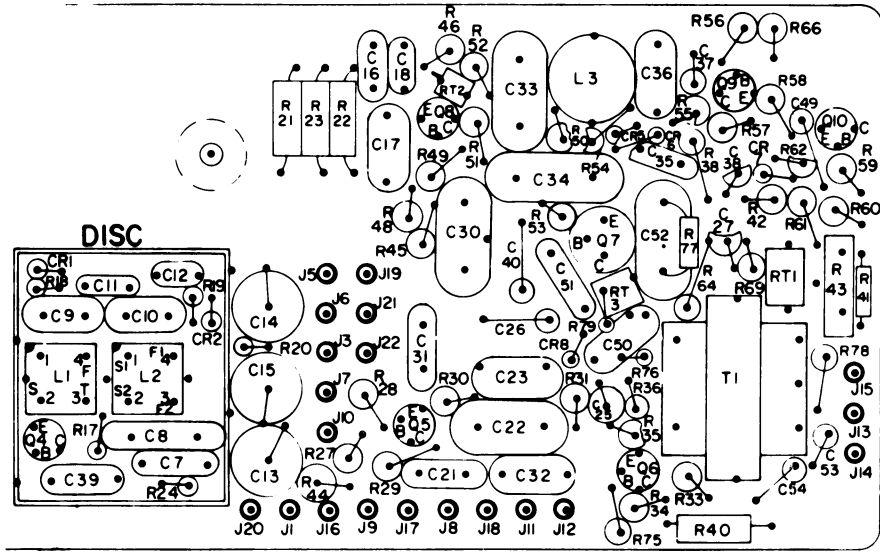


IF AUDIO & SQUELCH BOARD A426 (19D413129-G3)

- Rev. B - To control more closely the squelch control rotation. Changed R48.
- Rev. C - To eliminate barely audible squelch switching transients and to reduce receiver squelch tail. Deleted C38, C49, CR7, CR8, R62, R75 and R76. Added C55, R80, R81, and R82. Changed C27, C36, R53, R64 and R77.

OUTLINE DIAGRAM WAS:

IF-AUDIO & SQUELCH BOARD



SCHEMATIC DIAGRAM WAS:

IF AUDIO & SQUELCH BOARD A426 (19D413129-G3)

- Rev. D - To improve receiver frequency response. Changed R30 and R78.

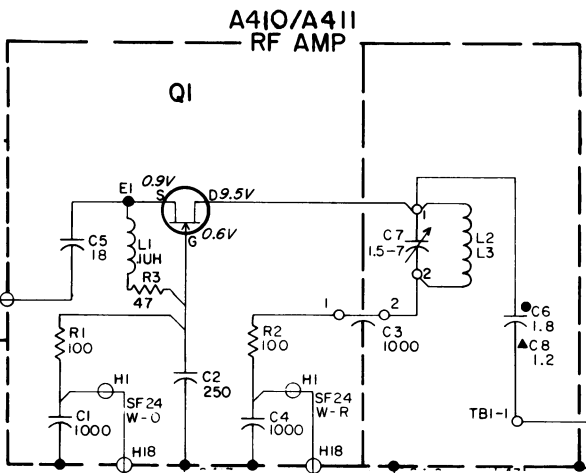
- REV. D - Channel Guard Encoder/Decoder A428 (Model 4EK16A10)
- REV. B - Tone Reject Filter A429 (19C311797-G2)

- To prevent excessive roll-off at 300 Hertz. Changed R59.

CHASSIS & RF ASSEMBLY 19E500881-G1 THRU -G4

- REV. G - To stabilize the R.F. Amplifier and to improve the band-end tuning of the multiplier assembly. Changed the R.F. amplifier board. Changed C5, C7 and C8 on the multiplier assembly.

Schematic Diagram was:



CHASSIS & RF ASSEMBLY 19E500881-G2 and G4

- REV. H - To improve band-end tuning. Changed C6 and C8.

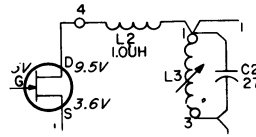
- REV. J - To remove unnecessary protection. Deleted CR1.

CHASSIS & RF ASSEMBLY 19E500881-G1 and G3

- REV. H - To remove unnecessary protection. Deleted CR1.

- REV. J - To prevent oscillations in the high IF amplifier and mixer. Changed C2 on the IF amplifier assembly 19B216356G1 & G2. Added C8 to First Mixer assembly 19C311974G1 as part of L3.

SCHEMATIC WAS:



- REV. K - To incorporate a new transistor. Changed Q410 and Q411.

CHASSIS & RF ASSEMBLY 19E500881-G2 and G4

- REV. L - To incorporate a new transistor. Changed Q410 and Q411.

- REV. M - To improve intermodulation performance. Changed Q1 and R3.

CHASSIS & RF ASSEMBLY 19E500881-G1 and G3

- REV. L - To improve intermodulation performance. Changed Q1 and R3.

IF AUDIO & SQUELCH BOARD A426 (19D413129-G3)

- REV. J - To increase PA bias current. Changed R40.

IF AUDIO & SQUELCH BOARD A426 (19D413129-G3)

- REV. E - To improve critical squelch action. Deleted R53 and added R84.
- REV. F - To compensate for vendor change. Changed C26.
- REV. G - To incorporate silicon diodes. Changed CR3 and CR4.
- REV. H - To insure squelch action at -30° C. Changed Q10.

IF AUDIO & SQUELCH BOARD A426 (19D413129-G3)

- REV. K - To improve stability of audio output with no load. Added R85

- REV. L - To improve frequency response. Deleted R85 and changed C40

OSCILLATOR/MULTIPLIER BOARD A432 Through A435 (19C311726G1-G4)

- REV. A - To improve Selectivity. Changed C8 and C14. Added L6.
- REV. B - To incorporate a new transistor. Changed Q1.

CHASSIS & RF ASSEMBLY (19E500881-G3)

- REV. M - To increase gain of RF amplifier. Changed C1.

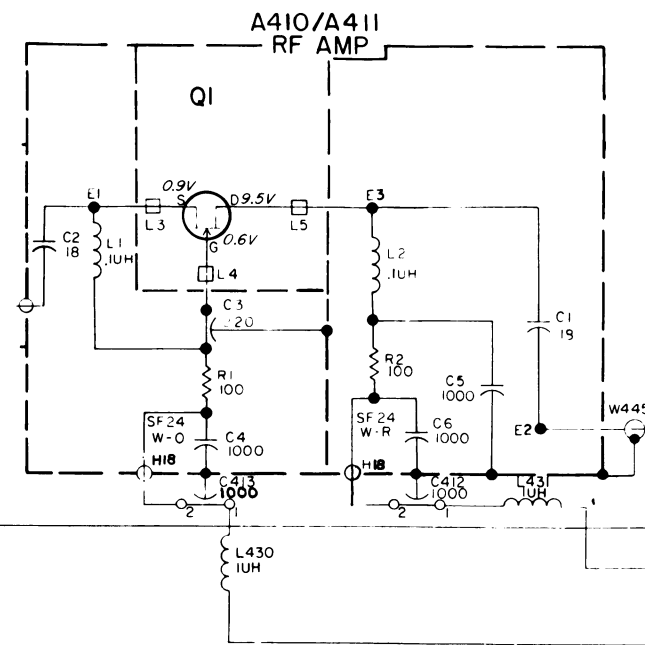
CHASSIS & RF ASSEMBLY (19E500881-G4)

- REV. N - To increase gain of RF Amplifier. Changed C1.

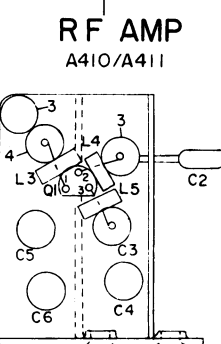
REV. N - CHASSIS & RF ASSEMBLY (19E500881-G3)

- REV. P - CHASSIS & RF ASSEMBLY (19E500881-G4)
- To incorporate improved design. Replaced existing RF amplifier assembly A410/A411 (19C317950G1) with a new RF Amplifier assembly (19C320697G1).

SCHEMATIC DIAGRAM WAS:



OUTLINE DIAGRAM WAS:



- REV. M - CHASSIS & RF ASSEMBLY (19E500881G1)
- REV. N - CHASSIS & RF ASSEMBLY (19E500881G2)
- REV. P - CHASSIS & RF ASSEMBLY (19E500881G3)
- REV. R - CHASSIS & RF ASSEMBLY (19E500881G4)

- To improve Sensitivity. Changed C3.

IF AUDIO & SQUELCH BOARD A426 (19D413129G3)

- REV. M - To improve audio quality. Changed R80.

- REV. N - To improve frequency response. Changed C26.

- REV. P - To improve stability. Changed Q5.

- REV. R - To improve critical squelch operation. Deleted C37, added C56 and changed R84.

- REV. N - Chassis & RF Assembly (19E500881G1)
- REV. P - Chassis & RF Assembly (19E500881G2)
- REV. R - Chassis & RF Assembly (19E500881G3)
- REV. S - Chassis & RF Assembly (19E500881G4)

- To incorporate new transistor. Changed Q1.

- REV. R - Chassis & RF Assembly (19E500881G2)
- REV. T - Chassis & RF Assembly (19E500881G4)

- To improve operation. Changed L427.

2nd Mixer Board A424 (19B216119G3)

- REV. A - To incorporate new transistor and improve stability. Deleted Q2 and added Q5.