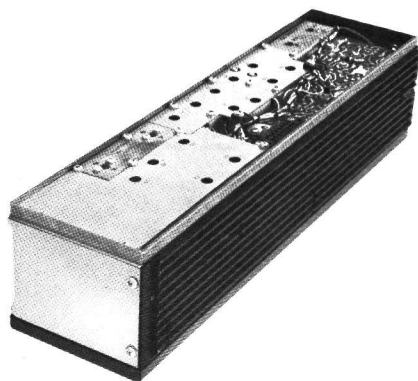


MASTR

Progress Line

25-50 MHz RECEIVER MODELS 4ER39C68-85 (WITH NOISE BLANKER)



SPECIFICATIONS *

FCC Filing Designation

Frequency Range

Audio Output

Sensitivity

12-dB SINAD (EIA Method)
20-dB Quieting Method

Selectivity

EIA Two-Signal Method
20-dB Quieting Method

Spurious Response

First Oscillator Stability

Modulation Acceptance

Squelch Sensitivity

Critical Squelch
Maximum Squelch

Intermodulation (EIA)

Maximum Frequency Separation

Frequency Response

ER-39-C

25—50 MHz

5 watts at less than 5% distortion

0.25 μ V
0.35 μ V

-85 dB (adjacent channel, 20 kHz channels)
-100 dB at ± 15 kHz

-100 dB

$\pm 0.0005\%$ (-30°C to $+60^{\circ}\text{C}$)

± 7 kHz (narrow-band)

0.15 μ V
Greater than 20 dB quieting (less than 1.5 μ V)

-65 dB

0.4%

+1 and -8 dB of a standard 6-dB per octave
de-emphasis curve from 300 to 3000 Hz (1000-Hz
reference)

*These specifications are intended primarily for the use of the serviceman. Refer to the appropriate Specification Sheet for the complete specifications.

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WARNING

No one should be permitted to handle any portion of the equipment that is supplied with high voltage; or to connect any external apparatus to the units while the units are supplied with power.

KEEP AWAY FROM LIVE CIRCUITS

DESCRIPTION

General Electric MASTR Progress Line Receiver Type ER-39-C is a double conversion, superheterodyne FM receiver designed for operation on the 25-50 megahertz band.

The receiver is of single-unit construction and is completely housed in a copper-plated aluminum casting for maximum shielding and rigidity. The top compartment of the casting contains the RF, oscillator, converter, and 1st low IF amplifier, and noise blanker. The bottom portion of the casting contains the audio-squelch board and the optional Channel Guard board.

CIRCUIT ANALYSIS

The MASTR Progress Line Receiver is completely transistorized, using silicon transistors throughout for added reliability. Input leads to the receiver are individually

filtered by the 20-pin feed-through by-pass connector J443. A regulated +10 volts is used for all receiver stages except the audio PA stage which operates from the 12-volt system supply.

Centralized metering jack J442 is provided for use with General Electric Test Set Model 4EX3A10 or 4EX8K11 for ease of alignment and servicing. The Test Set meters the noise blanker, multiplier, and limiter stages as well as the discriminator, and regulated 10 volts.

RF AMPLIFIERS (A341 & A344)

1st RF Amplifier (A341) consists of two high-Q helical resonators and an RF amplifier stage (Q2). The RF signal from the antenna is coupled by RF cable W441 to a tap on L341/L343/L345. The tap is positioned to insure the proper impedance match to the antenna. RF energy is coupled through the two coils by an opening in the shield wall to the base of 1st RF Amplifier

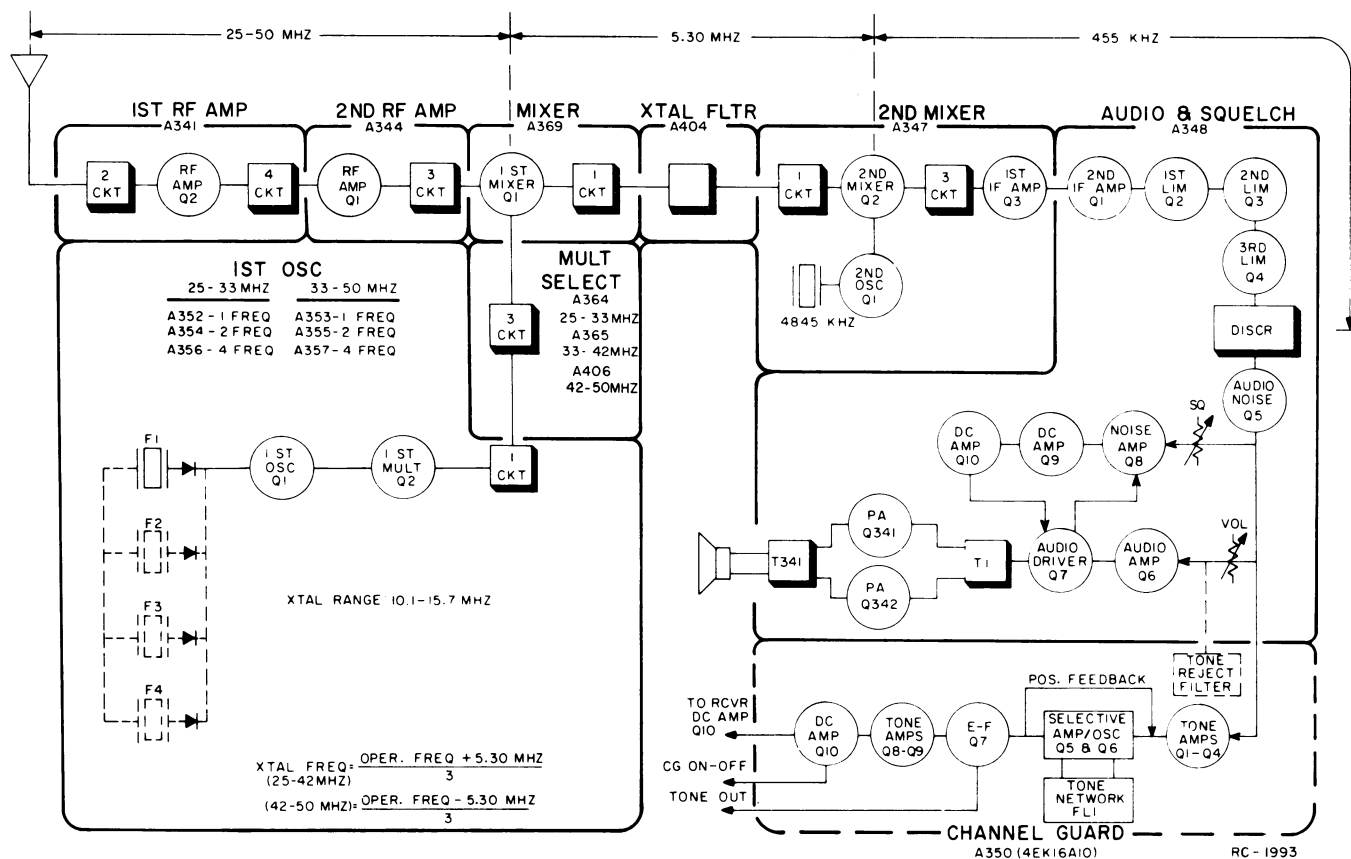


Figure 1 - Receiver Block Diagram

Q1. The coils are tuned to the incoming frequency by air trimmer capacitors C341 and C342.

The 1st RF amplifier uses a Field-Effect Transistor (FET) as the active device. The FET may be considered a semiconductor current path (or channel) whose resistance is varied by a voltage applied between the "gate" and "source" terminals. Lead identification for the FET is shown in Figure 2). The FET has voltage-controlled characteristics, and may be compared to a vacuum tube in operation (see Figure 2).

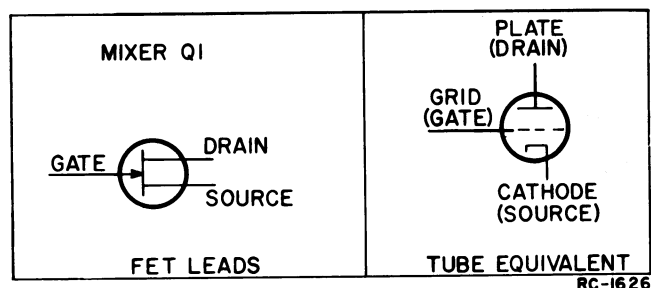


Figure 2 - FET Nomenclature

RF from the antenna is applied to the "source" terminal of FET Q1. Q1 operates as a grounded-gate amplifier. This method of operation provides a low impedance input to the amplifier. The amplified output is taken from the "drain" terminal and coupled through three tuned circuits to the 1st mixer.

The output of A341-Q1 is taken from the drain and is coupled through two or four tuned circuits to the base of 2nd RF Amplifier A344-Q1.

The output of the 2nd RF Amplifier is coupled through three tuned circuits to the base of 1st Mixer A369-Q1.

1ST OSCILLATOR AND MULTIPLIER (A352-A357)

The receiver 1st oscillator operates in a transistorized Colpitts oscillator circuit. The oscillator crystal operates in a fundamental mode at a frequency of approximately 10 to 15 megahertz. The crystal is cut to provide temperature compensation at the high end of the temperature range and is thermistor compensated at low temperatures. This provides $\pm 0.0005\%$ frequency stability as soon as the receiver is energized — without the warm-up time required by crystal ovens or warmers.

In single frequency receivers, bias for the oscillator is obtained by a jumper from H1 to H2 on the oscillator board.

In multi-frequency receivers, a diode is connected in series with the crystal,

and up to three additional crystal circuits can be added. The 10-volt jumper is removed and the proper frequency is selected by switching the desired crystal circuit to +10 volts by means of a frequency selector switch on the control unit.

Switching the +10 volts to the crystal circuit forward biases the diode and reduces its impedance. This applies the crystal frequency to the base of oscillator transistor Q1. Feedback for the oscillator is developed across C21/C22. The output is coupled to the base of 1st multiplier Q2.

The output of the 1st multiplier (multiplier Q2) is transformer-coupled (T3/T4) to multiplier selectivity assembly A364/A365. The multiplier tank is tuned to three times the crystal frequency. The stage is metered at centralized metering jack J442-4 through metering network CRL, R1, C5 and C6.

MULTIPLIER SELECTIVITY (A364/A365/A404)

Following the 1st multiplier tank (T3/T4) are two additional L-C tuned circuits (L1, L2 and L3). Capacitor C34/C35/C36 couples the multiplier selectivity output to the base of the first mixer.

1ST MIXER (A345) AND CRYSTAL FILTER (A404)

The 1st mixer uses a Field-Effect Transistor (FET) as the active device (Figure 2). The FET has several advantages over a conventional transistor, including a high input impedance, high power gain, and an output that is relatively free of harmonics (low in intermodulation products).

In 1st mixer A345, RF from the 1st RF amplifier and injection voltage from the multiplier selectivity assembly are applied to the gate of Q1. The mixer output is taken from the drain with the output tuned to the 5.3 MHz high IF frequency.

A highly selective crystal filter (A404) following the 1st mixer provides the major selectivity for the receiver. The output of the filter is fed through impedance matching transformer A347-T1 to the base of the 2nd mixer.

2ND OSCILLATOR, 2ND MIXER AND 1ST LO IF AMPLIFIER (A347)

A347-Q1 operates in a Colpitts oscillator circuit, with feedback supplied through C4. The oscillator low-side injection voltage (4845 kHz) is applied to the base of the 2nd mixer.

The High IF signal from the filter and the injection voltage from the 2nd oscillator is applied to the base of 2nd mixer Q2. The 455 kHz mixer output is applied to three tuned low IF circuits, L1, L2 and L3. These tuned circuits are required for shaping the

nose of the IF waveform, and for rejecting any undesired output frequencies from the 2nd mixer.

The low IF signal is applied to the base of 1st low IF amplifier A347-Q3. The output of A347-Q3 is R-C coupled to the base of the 2nd low IF amplifier.

2ND LO IF AMPLIFIER AND LIMITERS (A348)

Additional amplification of the low IF signal going to the limiter stages is provided by 2nd low IF amplifier A318-Q1. This stage is metered at J442-2 through a metering network consisting of C19, CR3 and R25.

Following the 2nd low IF amplifier are three R-C coupled limiter stages (A348-Q2, Q3 and Q4). The 1st limiter is metered at J442-3 through metering network C20, CR4 and R26.

DISCRIMINATOR (A348)

The limiter output is applied to a Foster-Seely type discriminator, where diodes CR1 and CR2 rectify the 455-kHz signal to recover the audio. The discriminator is metered at J442-10 through metering network C16 and R23.

AUDIO - NOISE AMPLIFIER (A348)

The discriminator output is coupled through a low-pass filter (C16, C18, R21 and R22) to the base of audio-noise amplifier Q5. The filter removes any 455-kHz signal remaining in the discriminator output. Q5 operates as an emitter-follower to match the discriminator impedance to the VOLUME control, SQUELCH control, and Channel Guard input. The stage also provides power gain.

AUDIO AMPLIFIERS (A348)

Any audio present in the incoming signal is coupled from the emitter of Q5 through the VOLUME control and a de-emphasis network to the base of audio amplifier Q6. The de-emphasis network consists of C22, C23, R30 and R31.

Audio driver Q7 follows the audio amplifier. The audio output of Q7 is coupled through transformer T1 to provide phase inversion for the push-pull audio PA stage.

Q341 and Q342 operate as a push-pull, class AB audio PA stage. The PA output is coupled through audio transformer T341 to the loudspeaker. The yellow and white tertiary windings of T341 supply balanced feedback to the collector of Q7. The feedback winding minimizes distortion and prevents the pick-up of external electrical noise.

The PA stage provides a 5-watt output at less than 5% distortion into a 3.5-ohm load at the receiver output terminals (3.2-ohms at the Control Unit). Base bias for the PA stage and the elimination of cross-over distortion is controlled by bias adjust potentiometer R43. The potentiometer is set at the factory as shown in STEP 1 of the receiver Test Procedure.

NOTE

Do not adjust bias adjust potentiometer R43 unless PA transistors Q341 and Q342 have been replaced.

Audio high and low are also present at centralized metering jack J442, and can be used as shown in STEP 1 of the Test Procedure.

SQUELCH (A348)

Noise from the audio-noise amplifier operates the squelch circuit. With no carrier present in the receiver, this noise is coupled to the base of noise amplifier Q8 through a high-pass filter which attenuates frequencies below 3 kHz. The filter consists of C30, C31 and R45, as well as C34 and L3 in the collector circuit of Q8. The gain of Q8 is determined by the Squelch control, which varies the bias on the base of Q8. Thermistor RT2 keeps the critical squelch constant over wide variations in temperature.

The output of noise amplifier Q8 is rectified by diodes CR5 and CR6, and filtered by C36 and C37 to produce a negative DC voltage. This DC voltage is applied to the base of DC amplifier Q9, turning it off. When turned off, the collector voltage of Q9 rises to approximately 8 volts, turning on DC amplifier Q10. When conducting, the collector voltage of Q10 drops to almost ground potential, which removes the base bias to audio amplifier Q6 and audio driver Q7, turning them off.

When the receiver is quieted by a signal (unsquelched), the noise in the receiver is reduced, turning DC amplifier Q9 on and DC amplifier Q10 off. This allows the audio stages to conduct so that sound is heard in the speaker. A network composed of C38, CR7 and R62 slows down the switching action of Q10, preventing an obnoxious "thump" from being heard in the speaker.

Resistor R53 connects from the emitter of audio driver Q7 to the emitter of noise amplifier Q8, providing a hysteresis loop in the squelch circuit. When a weak signal opens the squelch, the signal level may be reduced by 4 to 6 dB without the squelch closing. This limits squelch "flutter" or "picket-fence" operation.

With audio driver Q7 conducting, a positive voltage through R53 helps to reduce the gain of noise amplifier Q8. This positive feedback provides a quick, positive switching action in the squelch circuit. When the receiver squelches, audio driver Q7 turns off and its emitter potential drops to zero. This reduces the DC feedback through R53 to the emitter of noise amplifier Q8. Reducing the feedback causes Q8 to conduct harder, turning the audio stages off quickly.

Keying the transmitter removes the +10 volts from J19, turning off DC amplifier Q9 and turning on Q10 to mute the receiver.

NOISE BLANKER (A370/A372 - Figure 3)

An RF signal and noise pulse from the antenna is fed simultaneously to the Noise Blanker 1st RF Amplifier and the receiver 1st RF amplifier sections. The signal and noise is transformer coupled through T1/T2/T3 to the base of the first of two RF amplifier stages. The amplifier stages (Q1, Q2) raise the level of the noise pulse which is coupled through T10/T11/T12 and L10 to the base of the pulse detector Q3. A metering network consisting of R22, C21, and C17 permits the blanker to be metered at centralized metering jack J442-11.

Base bias for the pulse detector is established by R9 and CR1. CR1 is normally conducting, which keeps Q3 in a barely conducting state. A noise pulse applied to the base of Q3 causes it to conduct heavily. This results in a negative pulse at the out-

put (collector) of Q3. Following Q3 is a low-pass RF filter consisting of C18, C22 and L5.

The output of the filter is fed to the base of pulse amplifier Q4. This stage is biased by CR3, R12 and R13 so that it is just conducting. The negative-going pulse from the pulse detector cuts CR3 off, which biases Q4 on, and a positive pulse appears at the output of pulse amplifier Q4.

Q5 and Q6 form part of the one-shot multivibrator circuit. Bias voltage through R17 keeps Q5 normally turned on. The positive voltage at the collector of Q5 keeps Q6 turned off. The positive-going pulse from the pulse amplifier (Q4) is fed to the base of Q5, cutting the stage off. As Q5 cuts off, Q6 is turned on; and the output is an 8-volt, 12 to 18 microsecond positive-going blanking pulse. The positive blanking pulse is fed to the emitter of 2nd RF Amplifier A344-Q1 and coil L2. The pulse cuts off Q1 and shunts L2 for the duration of the noise pulse.

The positive blanking pulse to the emitter of the 2nd RF amplifier A344-Q1 is controlled by the RF Level Shut-Off Switch A376. The output of the 1st Mixer is fed through a low-pass filter network in the RF level switch circuit to the base of the high IF level amplifier Q1. When the antenna signal input level is approximately 500-5000 microvolts, the high IF level output of Q1 is sufficient to turn level ON level-sensitive switch Q2. The output of Q2 is filtered through C7, C8, L2 and then turns ON the Noise Blanker (A370/A372)

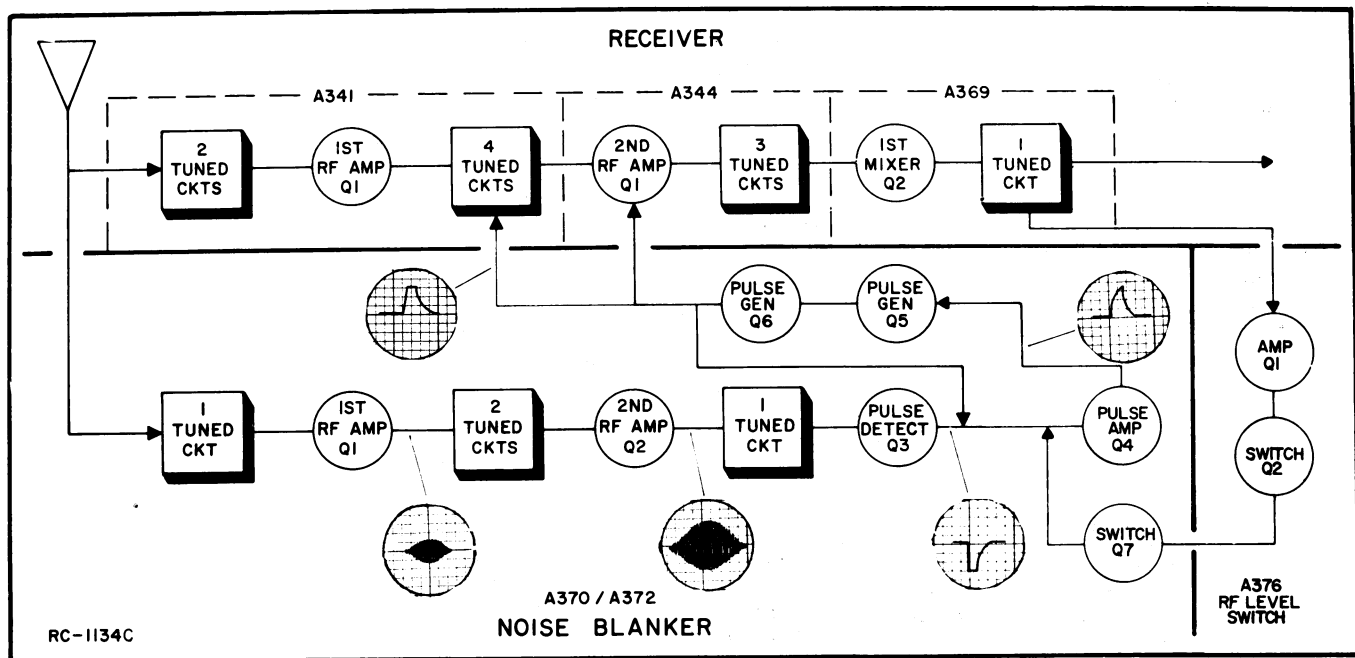


Figure 3 - Noise Blanker Block Diagram

switch Q7. The conduction of Q7 changes the bias to the 1st Pulse Amplifier Q4 and shorts the blanking pulse to ground.

The high IF output level (amplified by Q1) is not sufficient to turn Q2 ON when the antenna signal input is below the 500 to 5000 microvolt range. As a result, Q7 does not turn ON, and the positive blanking pulse is fed to the emitter of the 2nd RF Amplifier A344-Q1.

The blanking width is determined by R17 and C27. Diode CR6 keeps the output pulse a square wave. CR5 prevents oscillation at temperature extremes.

At the same time that the blanking pulse is applied to the receiver, samples of the pulse are fed to automatic repetition rate switch C30, C24, CR4, R13, R14 and R20. The pulse sample is coupled through C30 and is rectified by CR4. The rectified voltage charges C24 which then discharges through R13 and R14 to reverse bias CR3 and turn off pulse amplifier Q4. The components (C23, C24, R13 and R14) are selected so that the output pulses cannot blank the receiver continuously and prevent the desired signal from being heard.

The circuit time constant disables the blanking function whenever sinusoidal intermodulation signals produce beat frequencies of two kHz or higher. However, continuous impulse noise will not disable the blanker until a repetition rate of approximately 10 to 20 kHz is exceeded. The higher impulse noise repetition rate is provided by C23 which bypasses CR3 with the negative-going impulse noise. This turns on Q4 and allows the blanker to function.

As the noise signal from the antenna is applied to the Noise Blanker, the RF signal is applied to the receiver RF amplifier (A341). The six tuned circuits in the receiver front end provide a time delay for the RF signal, which enables the blanking pulse from the noise blanker to cut off the RF amplifier in the receiver before the noise pulse can get there.

The blanker may be disabled by shorting across the yellow dot on the noise blanker printed wiring board. Refer to the Noise Blanker Troubleshooting Procedure (as listed in the Table of Contents) for a complete performance check.

CHANNEL GUARD

Channel Guard Board Model 4EK16A10 is a fully transistorized encoder-decoder for use with MASTR Professional Series mobile and station combinations. The tone frequencies are controlled by plug-in tone networks that are made with precision components for excellent stability and reliability. The tone frequencies range from 71.9 to 203.5 Hz.

Encoder (A350)

Keying the transmitter removes the receiver mute +10 volts, and forward biases feedback control diode CR5, causing it to conduct. When conducting, the diode shunts R39, R35 and C19. This provides the necessary gain to the base of Q5 to permit oscillation.

The encoder tone is provided by selective amp-oscillator transistors Q5 and Q6 which oscillate at a frequency determined by the tone network. Negative feedback applied through the tone network to the base of Q5 prevents any gain in the stage except at the desired encode frequency.

Starting network R45, C21, C22 and CR6 provide an extremely fast starting time for the encoder tone. Keying the transmitter removes the receiver mute +10 volts, causing a pulse to be applied to the base of Q6 to quickly start the oscillator. Thermistor-resistor combination R32 and RT1 provides temperature compensation for the oscillator output. Limiter diodes CR3 and CR4 keep the tone amplitude constant.

Emitter-follower Q7 follows the oscillator circuit. The encoder tone is taken from the emitter of Q7 and applied to the transmitter.

Decoder (A350)

The decoder function is designed to eliminate all calls that are not tone coded for the Channel Guard frequency. As long as the CHANNEL GUARD-OFF switch on the control unit is left in the CHANNEL GUARD position, all signals are locked out except those from transmitters that are continuously tone coded for positive identification by the receiver.

Placing the CHANNEL GUARD-OFF switch in the OFF position instantly disables the Channel Guard operation so that all calls on the channel can be heard. When the hook-switch option is used, lifting the microphone from its hanger disables the Channel Guard Circuit.

Audio, tone and noise are taken from the emitter of the receiver audio-noise amplifier A348-Q5 and is fed through A350-J1 to four tone amplifier and bandpass filter circuits. The filters remove the audio and high-frequency noise from the signal, and the tone amplifiers provide sufficient gain to insure clipping by limiter diodes CR1 and CR2. The clipping action eliminates variation in the squelch performance due to changes in tone deviation. The signal is then applied to selective amplifiers Q5 and Q6 which amplify only the tone determined by the tone network.

The output of the selective amplifier is applied through emitter-follower Q7 to

the high gain, broad-band tone amplifiers Q8 and Q9. The output of Q9 is rectified by detector diodes CR7 and CR8, and the resulting negative DC voltage controls the squelch gate. Q8 is normally biased for low gain. When the tone is detected by CR7 and CR8, feedback is provided through R54 to quickly change the bias on Q8 for full gain. This ensures a more positive "un-squelching" action.

Squelch gate diode CR9 is normally forward biased by a positive DC voltage (approximately 1.5 volts) fed through R58. The forward bias causes CR9 to conduct, feeding a DC voltage to the base of DC amplifier A348-Q10 in the receiver. This removes the bias on the receiver audio stages and holds them off.

When the proper tone is applied to the decoder, the negative DC voltage from the detector diodes back-biases squelch gate diode CR9 and cuts off the positive bias to the receiver DC amplifier A348-Q10. However, the receiver noise squelch circuit continues to operate until a carrier quiets the receiver.

Placing the CHANNEL GUARD - OFF switch in the OFF position (or removing the microphone from its hookswitch) removes the ground to the base of the decoder DC switch (Q10), causing it to conduct. This back-biases squelch control diode CR9 and cuts off the positive bias to the receiver DC amplifier (A348-Q10). The receiver noise squelch circuit continues to operate until a carrier quiets the receiver.

A tone rejection filter connected in parallel with A348-J12 (in the receiver) bypasses any incoming tone to ground. This attenuates the tone level reaching the receiver audio circuits. The filter is composed of C26, C27, C28, C29, L1 and R59.

An optional tone reject filter (A402) that is identical to the filter described

above is available for use in two-way radios with transmitter Channel Guard only.

MAINTENANCE

DISASSEMBLY

To service the receiver from the top--

1. Pull locking handle down and pull radio about one inch out of mounting frame.
2. Pry up cover at rear of receiver.
3. Slide cover back and lift off.

To remove the receiver from the system frame--

1. Loosen the two Phillips-head retaining screws in front casting (see Figure 4), and pull casting away from system frame.
2. Remove the four screws in the back cover.
3. Remove the two screws holding the receiver at each end of the system frame.
4. Disconnect the antenna jack and the 20-pin connector from the front of the receiver, and slide the unit out of the system frame.

To service the receiver from the bottom--

1. Pull locking handle down. Pull radio out of mounting frame.
2. Remove screws in bottom cover. Pry up cover at back of receiver.
3. Slide cover back and lift off.

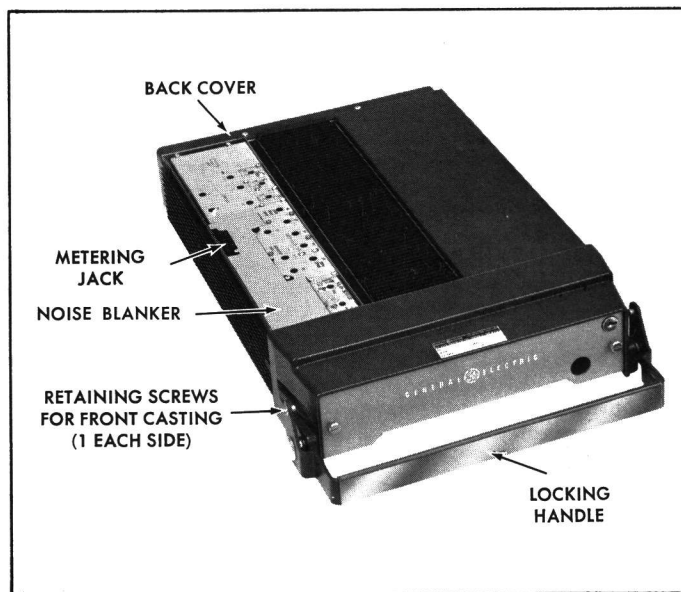


Figure 4 - Removing Top Cover

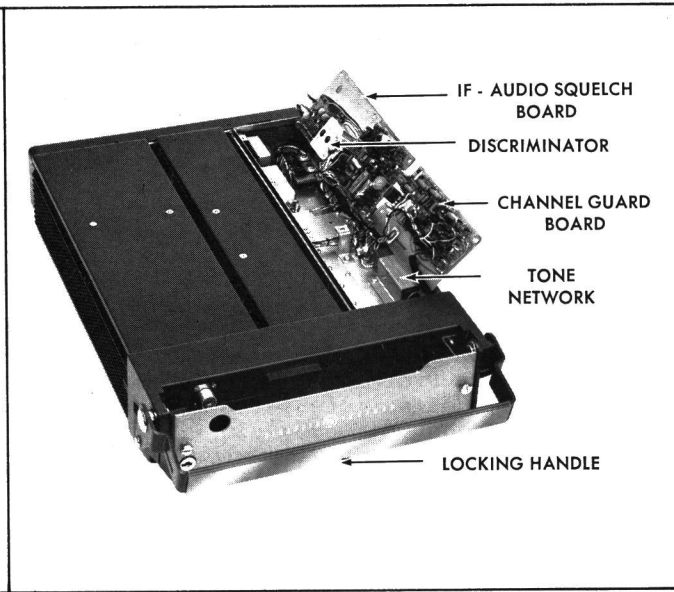


Figure 5 - Removing Bottom Cover

TEST PROCEDURES

These Test Procedures are designed to help you to service a receiver that is operating---but not properly. The problems encountered could be low power, poor sensitivity, distortion, limiter not operating properly, and low gain. By following the sequence of test steps starting with Step 1, the defect can be quickly localized. Once

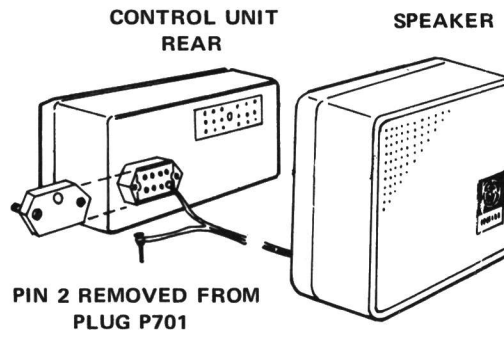
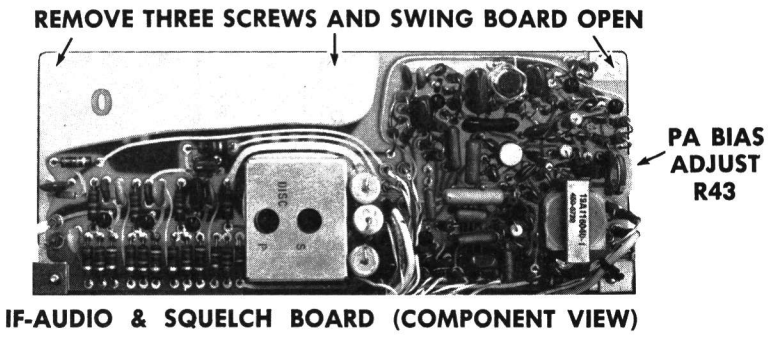
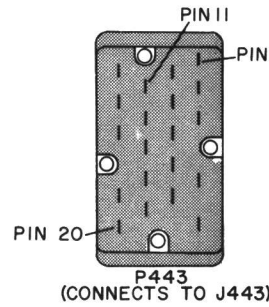
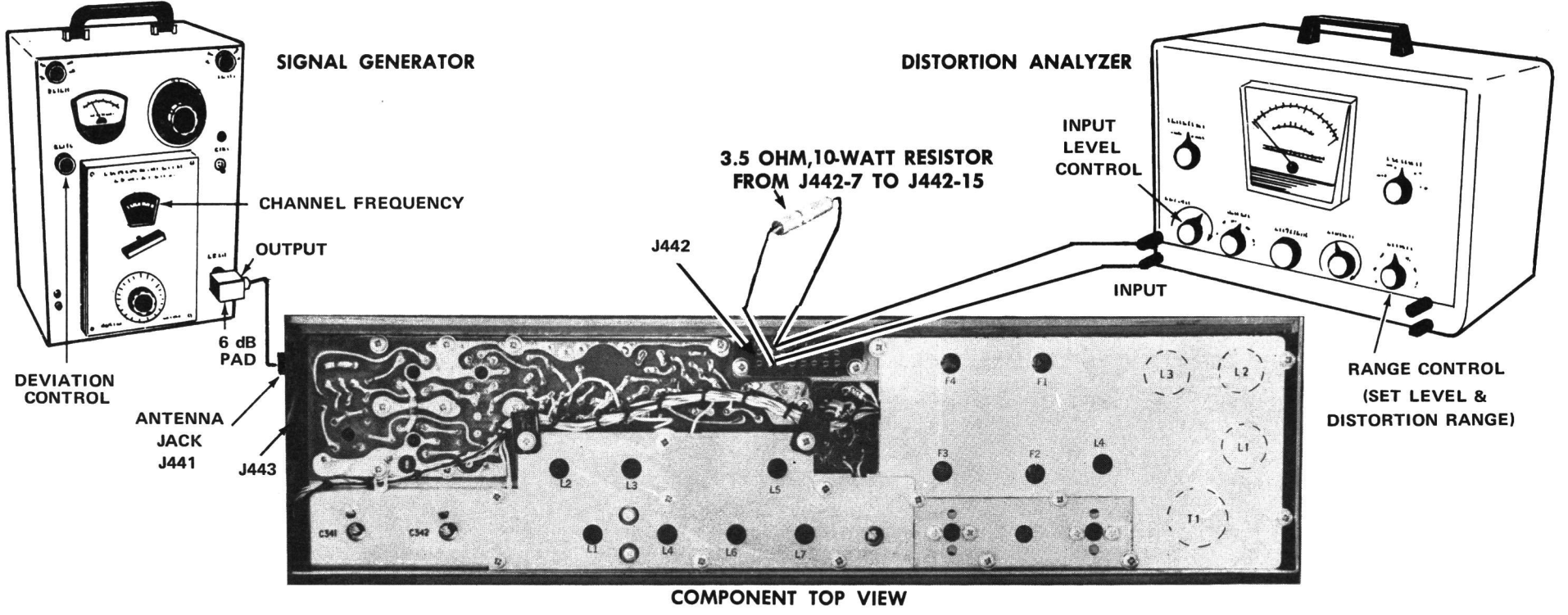
the defective stage is pin-pointed, refer to the "Service Check" listed to correct the problem. Additional corrective measures are included in the Troubleshooting Procedure. Before starting with the Receiver Test Procedures, be sure the receiver is tuned and aligned to the proper operating frequency.

TEST EQUIPMENT REQUIRED

- Distortion Analyzer similar to: Heath IM-12
- Signal Generator similar to: Measurements M-560
- 6-dB attenuation pad, and 3.5-ohm, 10-watt resistor

PRELIMINARY ADJUSTMENTS

1. Connect the test equipment to the receiver as shown for all steps of the receiver Test Procedure.
2. Turn the SQUELCH control fully clockwise for all steps of the Test Procedure.
3. Turn on all of the equipment and let it warm up for 20 minutes.



STEP 1
AUDIO POWER OUTPUT
AND DISTORTION

TEST PROCEDURE

Measure Audio Power Output as follows:

- A. Apply a 1,000-microvolt, on-frequency test signal modulated by 1,000 hertz with ± 3.0 kHz deviation to antenna jack J441.

- B. With Five-Watt Speaker:

Disconnect speaker lead pin from J701-2 (on rear of Control Unit).

Connect a 3.5-ohm load resistor from J442-15 to J442-7. Connect the Distortion Analyzer input across the resistor as shown.

OR

With Handset:

Lift the handset off of the hookswitch. Connect the Distortion Analyzer input from J442-15 to J442-7.

- C. Adjust the VOLUME control for five-watt output (4.18 VRMS using the Distortion Analyzer as a VTVM).

- D. Make distortion measurements according to manufacturer's instructions. Reading should be less than 5%. If the receiver sensitivity is to be measured, leave all controls and equipment as they are.

SERVICE CHECK

If the distortion is more than 5%, or maximum audio output is less than five watts, make the following checks:

- E. Battery and regulator voltage---low voltage will cause distortion. (Refer to Receiver Schematic Diagram for voltages.)

- F. P.A. Bias Adjust (R43) -- Turn the SQUELCH control fully counterclockwise.

Then connect a milliammeter in series with the +12 volt lead at P443-11. With no signal in, adjust R43 for a reading of approximately 20 milliamps. This adjustment should not be necessary unless an output transistor has been replaced.

- G. Audio Gain (Refer to Receiver Troubleshooting Procedure).

- H. Discriminator Alignment (Refer to Receiver Alignment on reverse side of page).

STEP 2
USABLE SENSITIVITY
(12-dB SINAD)

If STEP 1 checks out properly, measure the receiver sensitivity as follows:

- A. Apply a 1000-microvolt, on-frequency signal modulated by 1000 Hz with 3.0-kHz deviation to J441.

- B. Place the RANGE switch on the Distortion Analyzer in the 200 to 2000-Hz distortion range position (1000-Hz filter in the circuit). Tune the filter for minimum reading or null on the lowest possible scale (100%, 30%, etc.)

- C. Place the RANGE switch to the SET LEVEL position (filter out of the circuit) and adjust the input LEVEL control for a +2 dB reading on a mid range (30%).

- D. While reducing the signal generator output, switch the RANGE control from SET LEVEL to the distortion range until a 12-dB difference (+2 dB to -10 dB) is obtained between the SET LEVEL and distortion range positions (filter out and filter in).

- E. The 12-dB difference (Signal plus Noise and Distortion to noise plus distortion ratio) is the "usable" sensitivity level. The sensitivity should be less than 0.25 microvolts with an audio output of at least 2.5 watts (2.9 volts RMS across the 3.5-ohm receiver load using the Distortion Analyzer as a VTVM).

- F. Leave all controls as they are and all equipment connected if the Modulation Acceptance Bandwidth test is to be performed.

SERVICE CHECK

If the sensitivity level is more than 0.25 microvolts, check the alignment of the RF stages as directed in the Alignment Procedure, and make the gain measurements as shown on the Troubleshooting Procedure.

STEP 3
MODULATION ACCEPTANCE
BANDWIDTH (IF BANDWIDTH)

If STEPS 1 and 2 check out properly, measure the bandwidth as follows:

- A. Set the Signal Generator output for twice the microvolt reading obtained in the 12-dB SINAD measurement.

- B. Set the RANGE control on the Distortion Analyzer in the SET LEVEL position (1000-Hz filter out of the circuit), and adjust the input LEVEL control for a +2 dB reading on the 30% range.

- C. While increasing the deviation of the Signal Generator, switch the RANGE control from SET LEVEL to distortion range until a 12-dB difference is obtained between the SET LEVEL and distortion range readings (from +2 dB to -10 dB).

- D. The deviation control reading for the 12-dB difference is the Modulation Acceptance Bandwidth of the receiver. It should be more than ± 7 kHz (but less than ± 9 kHz).

SERVICE CHECK

If the Modulation Acceptance Bandwidth test does not indicate the proper width, make gain measurements as shown on the Receiver Troubleshooting Procedure.

TROUBLESHOOTING PROCEDURE

LBI-4124

Before starting the Noise Blanker troubleshooting procedure, make sure the receiver is operating properly. Align the Noise Blanker as described on the ALIGNMENT PROCEDURE Sheet. Then make the following Troubleshooting checks:

STEP 1—PERFORMANCE CHECK

Equipment Required:

- RF Signal Generator coupled through a 6 dB pad.
- Pulse Generator with repetition rate and level controls (similar to General Electric Model 4EX4A10)
- AC VTVM

Procedure:

1. Connect Pulse Generator and RF Signal Generator to receiver antenna jack through a T-connector and connect VTVM to receiver output as shown in Figure 1.

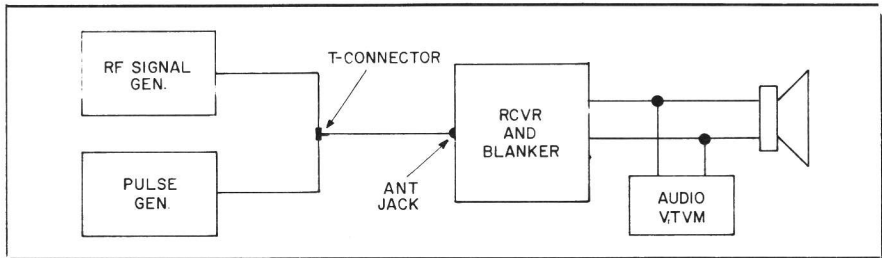


Figure 1 - Equipment Connection Diagram

RC-1388

2. Apply an unmodulated RF Signal and check the 20 dB quieting sensitivity of the receiver. (Measure with Model 4EX4A10 Pulse Generator connected but turned off).
3. Disable pulse section of the noise blanker by shorting Q4 base to emitter. (A yellow dot is located between the base and emitter connections on solder side of the noise blanker board).
4. Set the pulse generator (Model 4EX4A10) repetition rate to 1500 Hz and adjust the output level control on pulse generator until receiver sensitivity is degraded as much as possible (approximately 45 dB).
5. Remove base-emitter short from Q4. The receiver sensitivity should restore to within 5 dB of 20 dB quieting level obtained in step 2 above.

STEP 2—QUICK CHECKS

Equipment Required:

- Audio Voltmeter (VTVM)
- Audio Oscillator (sine wave)

SYMPTOMS	PROCEDURE
No regulated 10-volts	Check the 12-volt supply. Then check regulator circuit. (Refer to troubleshooting procedure for power supply.)
No blanking	Check waveforms (STEP 3) and voltage ratios (STEP 4).
Partial or no blanking	<p>a. Check RF attenuation as follows: Connect signal generator to Antenna Jack. Adjust the output of the signal generator for 0.2 volts on the 2nd IF amplifier (position B on test set) and note the signal generator reading. Short the Q5 base to emitter pattern (identified by red ink dot) and increase the signal generator output until the same 2nd IF amplifier reading is obtained. Signal level must increase 60 dB or more.</p> <p>b. Check repetition rate switch. Connect a 6-kHz sine wave signal from audio oscillator through a 0.33-μF capacitor to point "A" located on the noise blanker board. Adjust the output of the audio oscillator for 2-volts, peak-to-peak. Observe the output of the pulse generator (on noise blanker) with an oscilloscope. The repetition rate of the pulse generator should not increase over 2 kHz or decrease under 1 kHz. (This is true for sine wave inputs like intermodulation in the blanker channel but not for strong impulse noise from antenna.)</p> <p>c. Check vehicle ignition system. Worn-out points, bad spark plugs, or breaks in ignition wiring can cause a "dirty" ignition pulse to be generated causing the blanker to operate incorrectly.</p>

STEP 4—VOLTAGE RATIO READINGS

Equipment Required:

- RF Voltmeter (similar to Boonton Model 91-CA
- or Millivac Type MV-18 C)

Procedure:

1. Apply probe to input of stage (for example, base of 1st RF Amp). Peak resonant circuit of stage being measured and take voltage reading (E₁).
2. Move probe to input of following stage (2nd RF Amp. Repeat first resonant circuit. Then peak circuit being measured and take reading (E₂).
3. Convert readings by means of the following formula.

$$\text{Voltage Ratio} = \frac{E_2}{E_1}$$

4. Check results with typical voltage ratios shown on diagram for each stage.

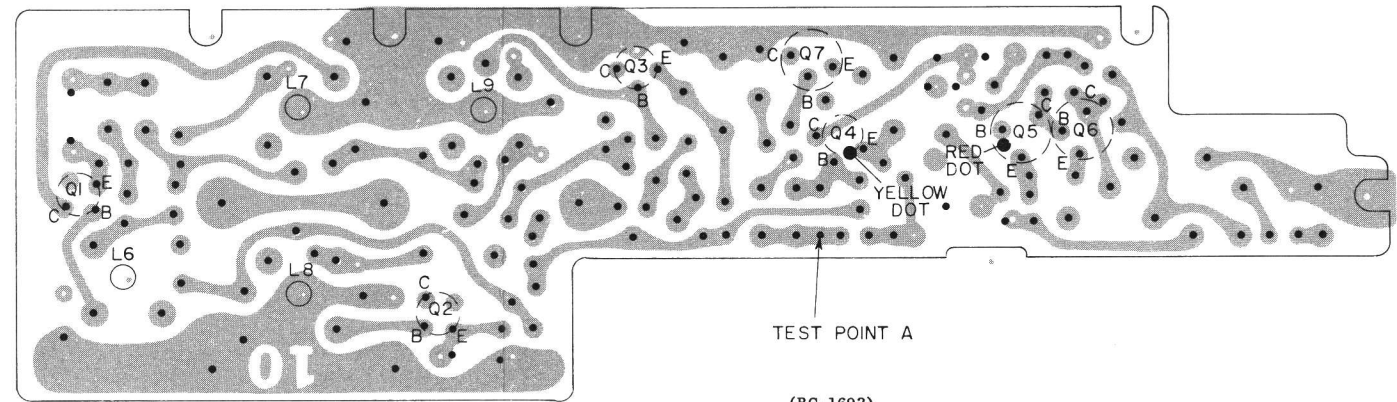
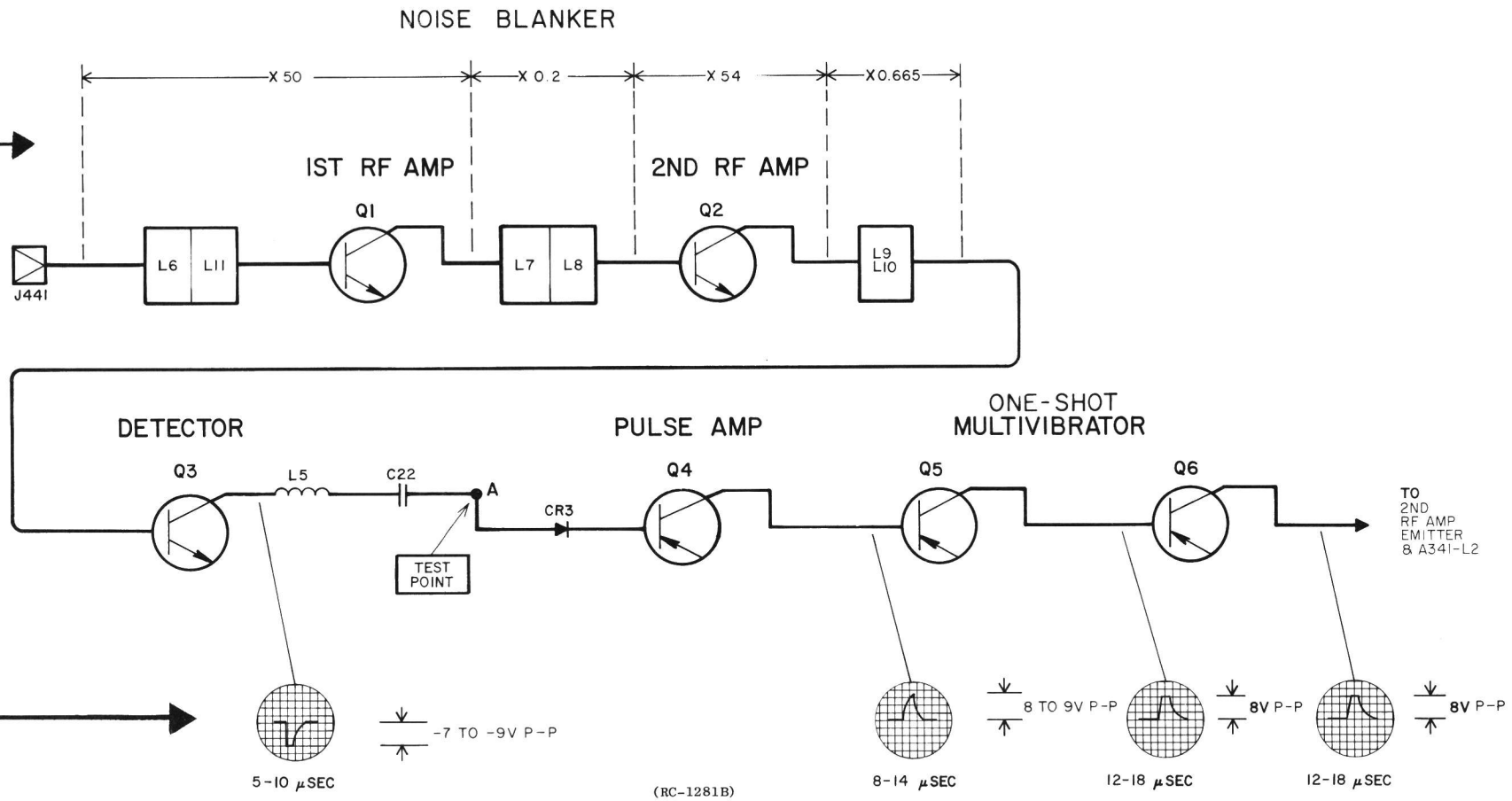
STEP 3—WAVE FORMS

Equipment Required:

- Oscilloscope
- Noise Generator

Procedure:

Adjust noise generator for maximum output level and observe waveforms on oscilloscope at the indicated points.



TEST POINT A

(RC-1693)
(19B204655, Sh. 2, Rev.10)

Denotes Solder Side

TROUBLESHOOTING PROCEDURE

NOISE BLANKER FOR 25—50 MHz RECEIVER
TYPE ER-39-C

TROUBLESHOOTING PROCEDURE

LBI4124

Before starting the Noise Blanker troubleshooting procedure, make sure the receiver is operating properly. Align the Noise Blanker as described on the ALIGNMENT PROCEDURE Sheet. Then make the following Troubleshooting checks:

STEP 1—PERFORMANCE CHECK

Equipment Required:

- RF Signal Generator coupled through a 6 dB pad.
- Pulse Generator with repetition rate and level controls (similar to General Electric Model 4EX4A10)
- AC VTVM

Procedure:

1. Connect Pulse Generator and RF Signal Generator to receiver antenna jack through a T-connector and connect VTVM to receiver output as shown in Figure 1.

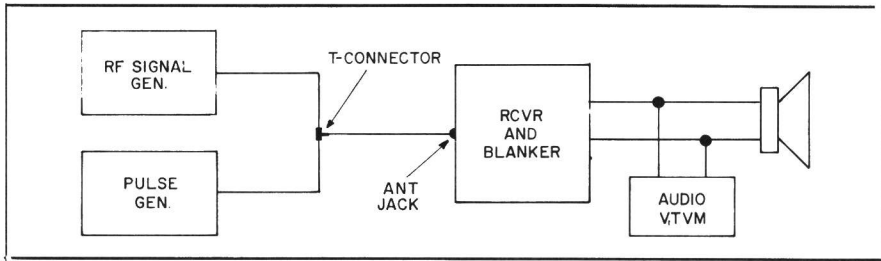


Figure 1 - Equipment Connection Diagram

RC-1388

2. Apply an unmodulated RF Signal and check the 20 dB quieting sensitivity of the receiver. (Measure with Model 4EX4A10 Pulse Generator connected but turned off).
3. Disable pulse section of the noise blanker by shorting Q4 base to emitter. (A yellow dot is located between the base and emitter connections on solder side of the noise blanker board).
4. Set the pulse generator (Model 4EX4A10) repetition rate to 1500 Hz and adjust the output level control on pulse generator until receiver sensitivity is degraded as much as possible (approximately 45 dB).
5. Remove base-emitter short from Q4. The receiver sensitivity should restore to within 5 dB of 20 dB quieting level obtained in step 2 above.

STEP 2—QUICK CHECKS

Equipment Required:

- Audio Voltmeter (VTVM)
- Audio Oscillator (sine wave)

SYMPTOMS	PROCEDURE
No regulated 10-volts	Check the 12-volt supply. Then check regulator circuit. (Refer to troubleshooting procedure for power supply.
No blanking	Check waveforms (STEP 3) and voltage ratios (STEP 4).
Partial or no blanking	<p>a. Check RF attenuation as follows: Connect signal generator to Antenna Jack. Adjust the output of the signal generator for 0.2 volts on the 2nd IF amplifier (position B on test set) and note the signal generator reading. Short the Q5 base to emitter pattern (identified by red ink dot) and increase the signal generator output until the same 2nd IF amplifier reading is obtained. Signal level must increase 60 dB or more.</p> <p>b. Check repetition rate switch. Connect a 6-kHz sine wave signal from audio oscillator through a 0.33-μF capacitor to point "A" located on the noise blanker board. Adjust the output of the audio oscillator for 2-volts, peak-to-peak. Observe the output of the pulse generator (on noise blanker) with an oscilloscope. The repetition rate of the pulse generator should not increase over 2 kHz or decrease under 1 kHz. (This is true for sine wave inputs like intermodulation in the blanker channel but not for strong impulse noise from antenna.)</p> <p>c. Check vehicle ignition system. Worn-out points, bad spark plugs, or breaks in ignition wiring can cause a "dirty" ignition pulse to be generated causing the blanker to operate incorrectly.</p>

STEP 4—VOLTAGE RATIO READINGS

Equipment Required:

- RF Voltmeter (similar to Boonton Model 91-CA or Millivac Type MV-18 C)

Procedure:

1. Apply probe to input of stage (for example, base of 1st RF Amp). Peak resonant circuit of stage being measured and take voltage reading (E_1).
2. Move probe to input of following stage (2nd RF Amp). Repeat first resonant circuit. Then peak circuit being measured and take reading (E_2).
3. Convert readings by means of the following formula.

$$\text{Voltage Ratio} = \frac{E_2}{E_1}$$

4. Check results with typical voltage ratios shown on diagram for each stage.

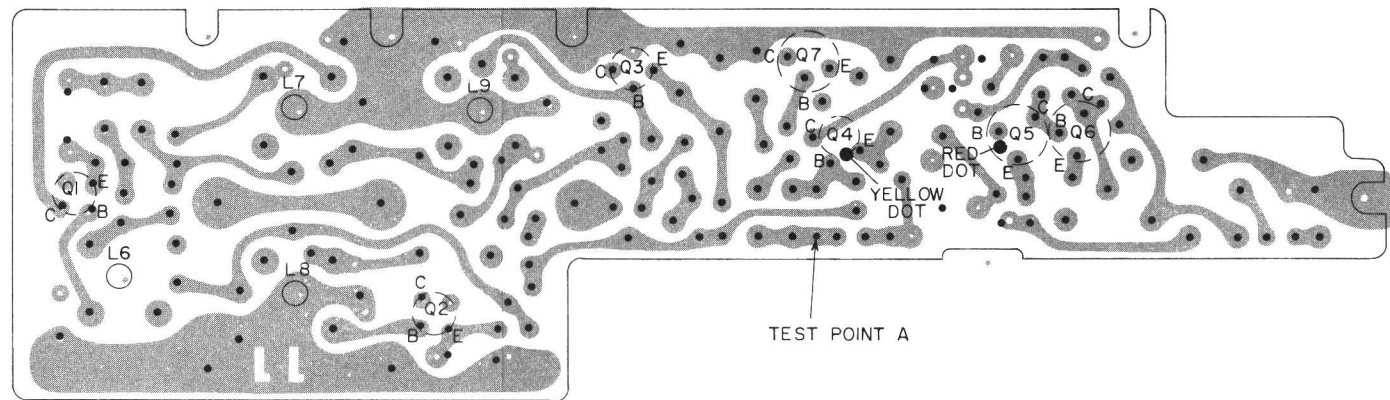
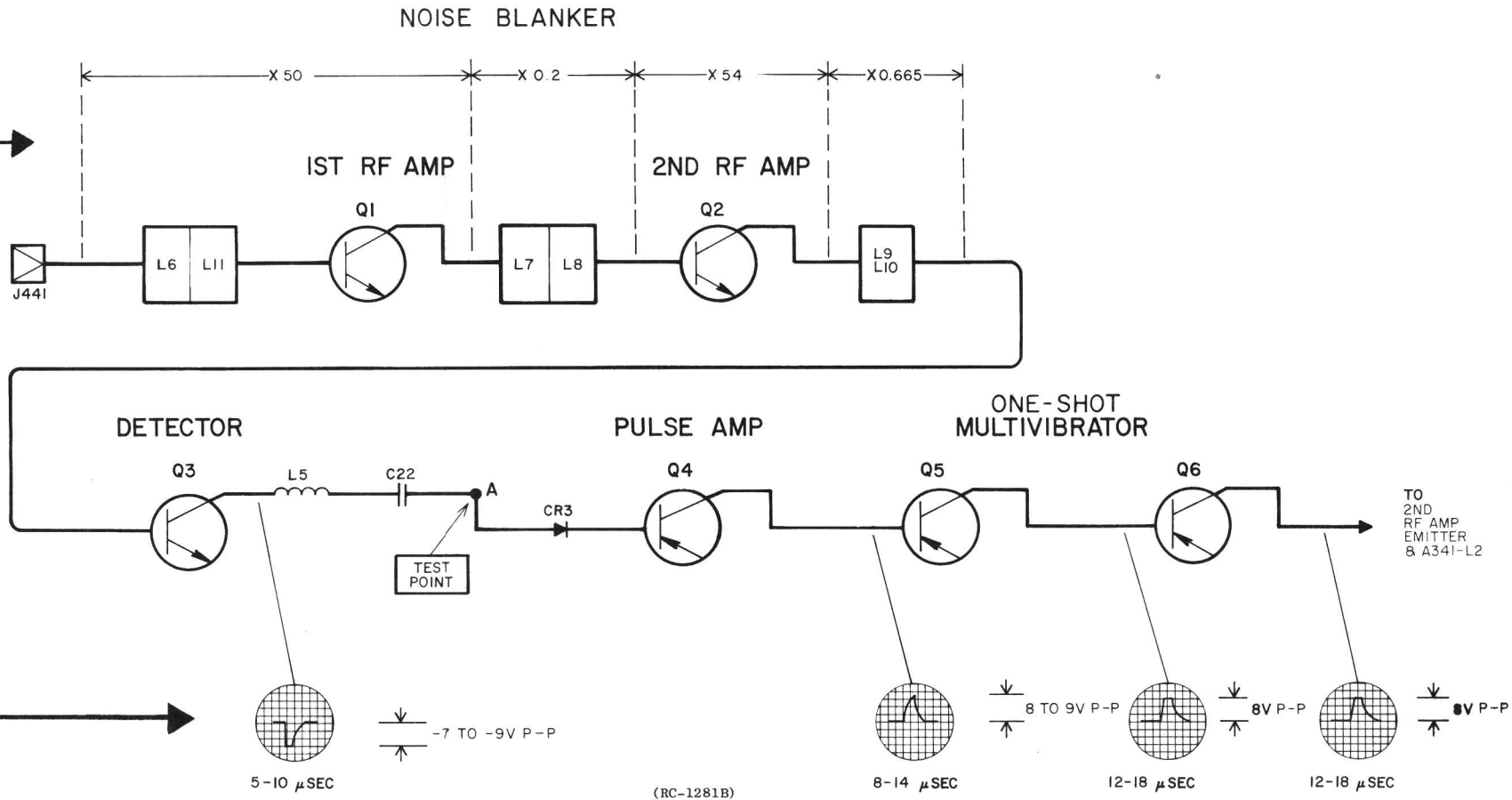
STEP 3—WAVE FORMS

Equipment Required:

- Oscilloscope
- Noise Generator

Procedure:

Adjust noise generator for maximum output level and observe waveforms on oscilloscope at the indicated points.



Denotes Solder Side

TROUBLESHOOTING PROCEDURE

NOISE BLANKER FOR 25—50 MHz RECEIVER
TYPE ER-39-C

STEP 1 - QUICK CHECKS

TEST SET CHECKS

These checks are typical voltage readings measured with GE Test Set Model 4EX3A10 in the Test 1 position, or Model 4EX8K10 or 11 in the 1-volt position.

Metering Position	Reading With No Signal In	Reading with 1 Micro-volt Unmodulated
A (Disc Idling)	Less than ±.05 VDC	
B (2nd IF)	.15 VDC	.7 VDC
C (1st Lim)	.7 VDC	0.8 VDC
D (Mult-1)	0.6 VDC	
J (Reg. +10 volts)	+10 VDC	

SYMPTOM CHECKS

SYMPTOM	PROCEDURE
NO SUPPLY VOLTAGE	● Check power connections and continuity of supply leads, and check fuse in power supply. If fuse is blown, check receiver for short circuits.
NO REGULATED 10-VOLTS	● Check the 12-volt supply. Then check regulator circuit. (See Troubleshooting Procedure for Power Supply).
LOW 1ST LIM READING	● Check supply voltages and then check oscillator reading at J442-4 & 5 as shown in STEP 2A. ● Make SIMPLIFIED VTVM GAIN CHECKS from 2nd Mixer through 1st Limiter stages as shown in STEP 2A.
LOW OSCILLATOR/MULTIPLIER READINGS	● Check alignment of Oscillator, (Refer to Front End Alignment Procedure). ● Check voltage readings of 1st Oscillator/Multiplier Q1/Q2. ● Check crystal Y1.
LOW RECEIVER SENSITIVITY	● Check Front End Alignment. (Refer to Receiver Alignment Procedure). ● Check antenna connections, cable and relay. ● Check 1st and 2nd Oscillator injection voltage. ● Check voltage readings of 1st Mixer, HI IF Amp and 2nd Mixer. ● Make SIMPLIFIED GAIN CHECKS (STEP 2A).
LOW AUDIO	● Check Audio PA (Q341 & Q342) voltage readings on schematic diagram. ● Make simplified gain and waveform checks of audio and squelch stages. (Steps 2A and 2B). ● Make unsquelched voltage readings in Audio section. (Refer to Receiver Schematic Diagram). ● Check voltage readings on Channel Guard board.
HIGH DISTORTION AT LOW AUDIO LEVELS (50 MW)	● Set PA bias adjust R43 as specified under Service Checks in STEP 1 of TEST PROCEDURES.
IMPROPER SQUELCH OPERATION	● Check voltage readings of Squelch circuit. (Refer to Receiver Schematic Diagram). ● Make gain and waveform checks of audio and squelch stages. (Steps 2A and 2B).
DISTORTION IDLING TOO FAR OFF ZERO	● See if discriminator zero is in center of IF bandpass.

STEP 3-VOLTAGE RATIO READINGS

EQUIPMENT REQUIRED:

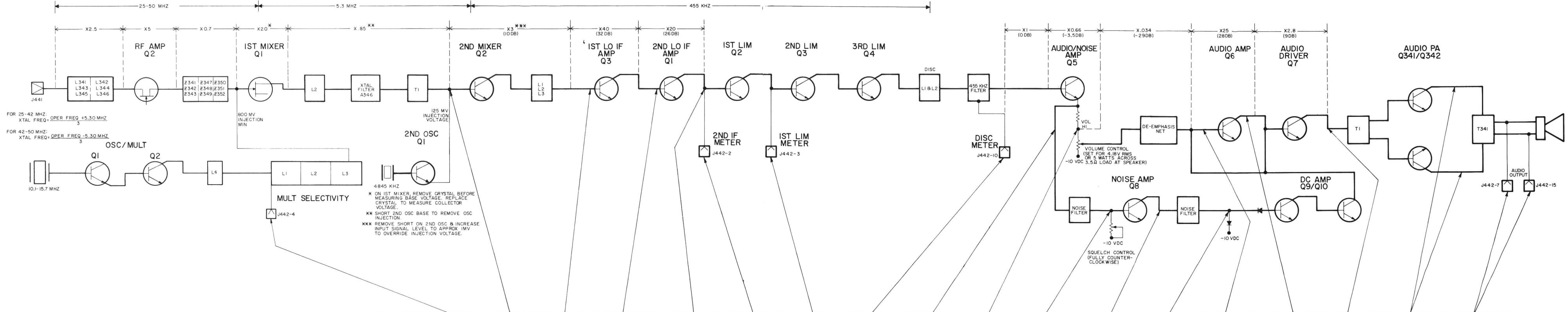
- RF Voltmeter (similar to Boonton Model 91-CA or Millivac Type MV-18 C.
- Signal on receiver frequency (below saturation). Correct frequency can be determined by zeroing the discriminator. Use 1,000 hertz signal with 3.0 kHz deviation.

PROCEDURE:

- Apply probe to input of stage (for example, base of RF amp). Peak resonant circuit of stage being measured and take voltage reading (E₁).
- Move probe to input of following stage (1st mixer*). Re-peak first resonant circuit then peak circuit being measured and take reading (E₂).
- Convert readings by means of the following formula.

$$\text{Voltage Ratio} = \frac{E_2}{E_1}$$

- Check results with typical voltage ratios shown on diagram.



STEP 2A-SIMPLIFIED VTVM GAIN CHECKS

EQUIPMENT REQUIRED:

- VTVM - AC & DC
- Signal generator (Measurements M560 to equivalent).

PRELIMINARY STEPS:

- Set VOLUME control for 4.18 volts across 3.5-ohm load. If this cannot be obtained, set to approx. 70% of max. rotation.
- Set SQUELCH control fully counterclockwise.
- Receiver should be properly aligned.
- Connect VTVM between system negative and points indicated by arrow.

SIGNAL GENERATOR INPUT AT J441. MAINTAIN SETTING AT DISCRIMINATOR ZERO.	UNMODULATED	UNMODULATED	UNMODULATED	UNMODULATED	1 MICROVOLT UNMODULATED	NO SIGNAL INPUT	STANDARD SIGNAL (1 MILLIVOLT AT RECEIVER FREQUENCY MODULATED BY 3.3 KHZ DEVIATION)	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL	STANDARD SIGNAL
PROCEDURE	INCREASE GENERATOR OUTPUT UNTIL VTVM READING ON 12 V SCALE INCREASES BY 50 MV	INCREASE SIGNAL GENERATOR OUTPUT FROM ZERO UNTIL VTVM READING DECREASES BY 5%	INCREASE SIGNAL GENERATOR OUTPUT FROM ZERO UNTIL VTVM READING DECREASES BY 5%	INCREASE SIGNAL GENERATOR OUTPUT FROM ZERO UNTIL VTVM READING DECREASES BY 5%	INCREASE SIGNAL GENERATOR OUTPUT FROM ZERO UNTIL VTVM READING DECREASES BY 5%												CONNECT VTVM OR SCOPE ACROSS 3.5Ω LOAD BETWEEN J442-7 AND J442-15 WITH SPEAKER DISCONNECTED.
READING	2.4 VDC	GENERATOR OUTPUT SHOULD BE APPROX 20 MILLIVOLTS	GENERATOR OUTPUT SHOULD BE APPROX 600 MICROVOLTS	GENERATOR OUTPUT SHOULD BE APPROX 5 MICROVOLTS	GENERATOR OUTPUT SHOULD BE APPROX 0.3 MICROVOLTS	-0.6 VDC	-2 VDC	0.8 VAC	0.75 VAC	0.55 VAC	0.15 VAC	2.3 VAC	0.05 VAC	0.5 VAC	1.4 VAC	10 VAC	4.18 VAC

STEP 2B-AUDIO & SQUELCH WAVEFORMS

EQUIPMENT REQUIRED:

- Oscilloscope.
- Signal generator (Measurements M560 to equivalent).

PRELIMINARY STEPS:

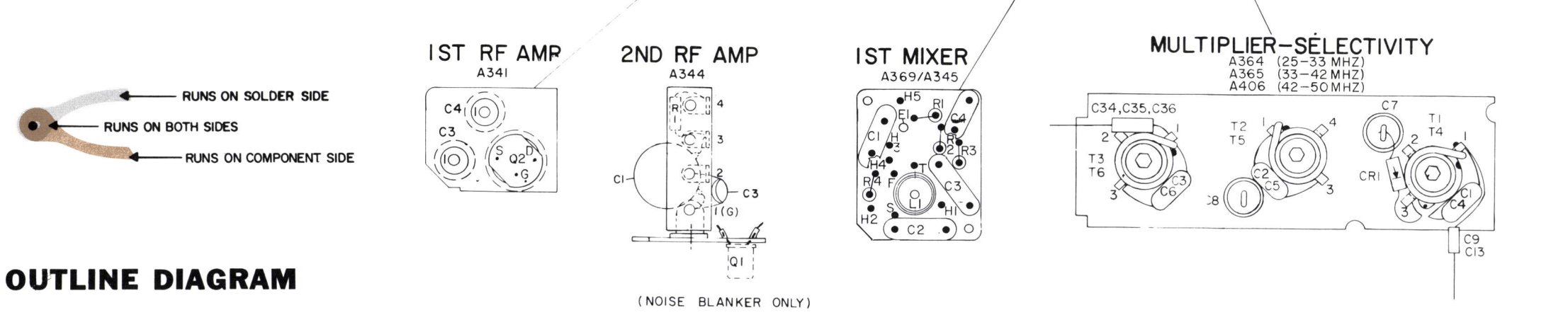
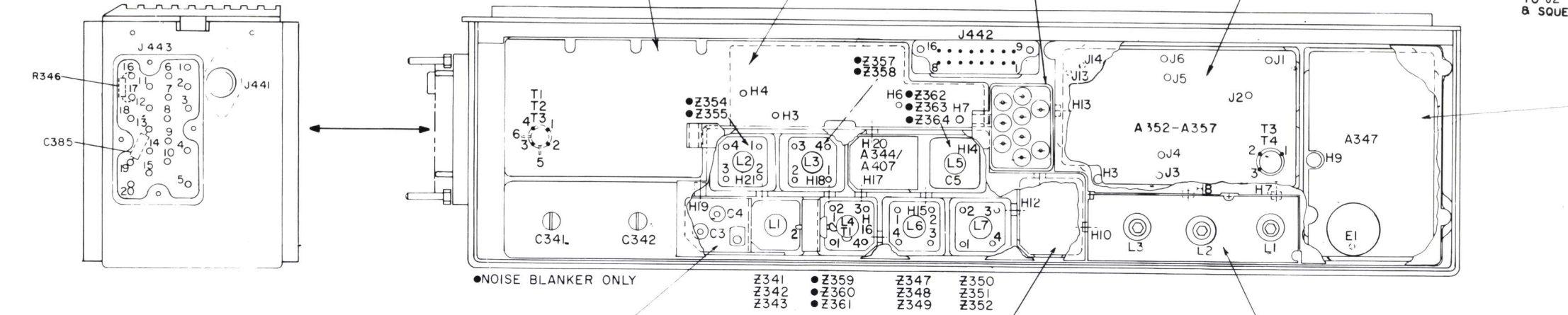
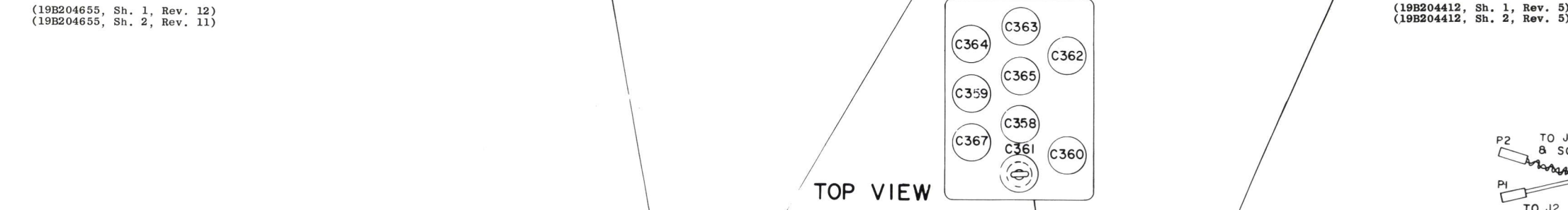
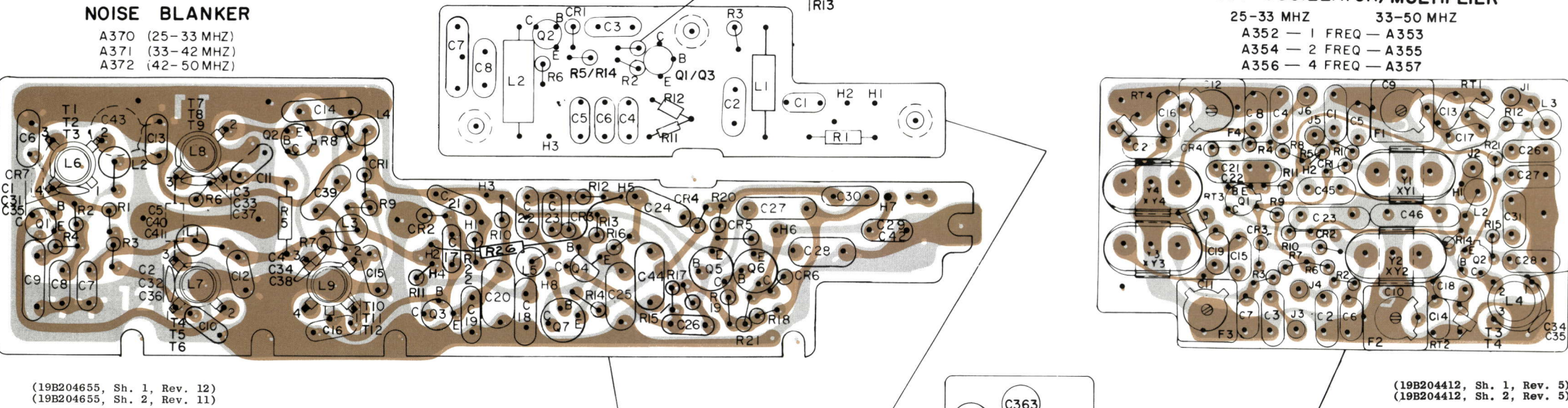
- Set VOLUME control for 4.18 volts across 3.5-ohm load. If this cannot be obtained, set to approx. 70% of max. rotation.
- Set SQUELCH control fully counterclockwise.
- Receiver should be properly aligned.
- Connect oscilloscope between system negative and points indicated by arrow.

SCOPE SETTING	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV	0.5 MS/DIV
	1 VOLT/DIV	1 VOLT/DIV	1 VOLT/DIV	2 VOLTS/DIV	0.5 VOLTS/DIV	50 MILLIVOLTS/DIV	1 VOLT/DIV	2 VOLTS/DIV	10 VOLTS/DIV	5 VOLTS/DIV							
STANDARD SIGNAL (1 MILLIVOLT AT RECEIVER FREQUENCY MODULATED BY 1 KHZ WITH 3.3 KHZ DEVIATION)																	
NOISE WAVE FORM (NO SIGNAL INPUT)																	

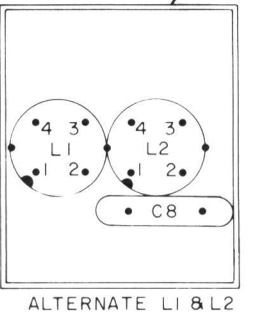
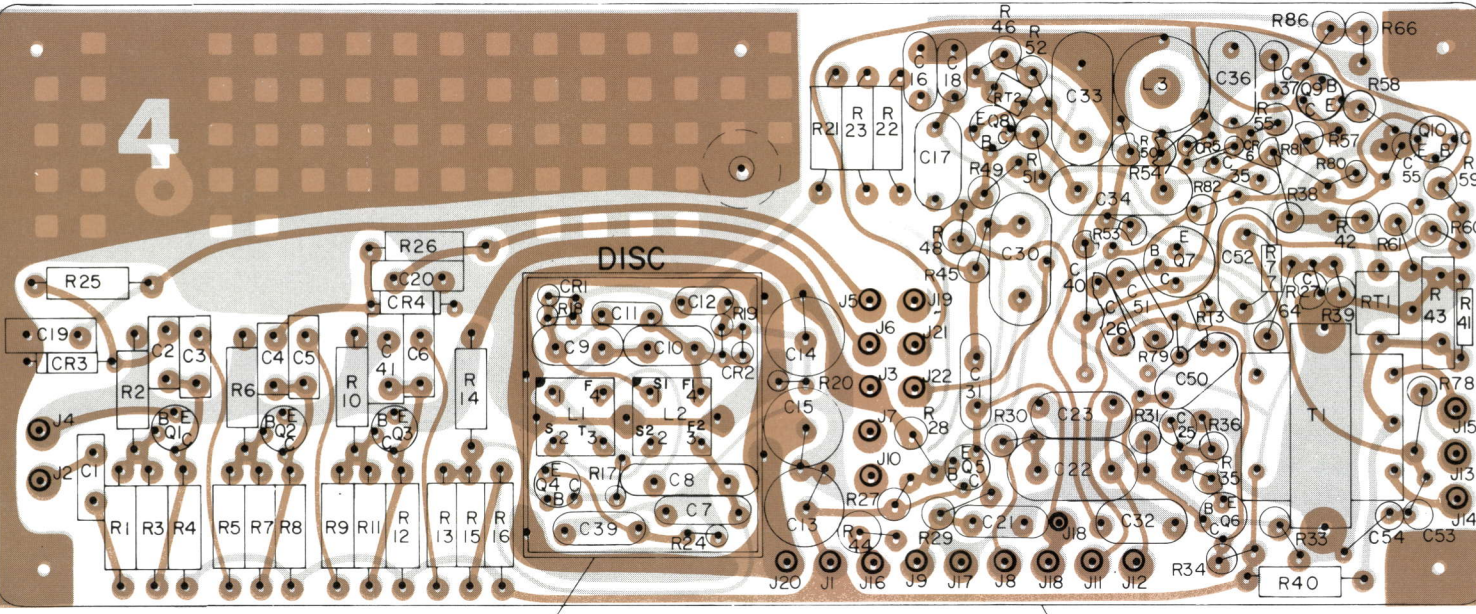
(RC-1992)

TROUBLESHOOTING PROCEDURE

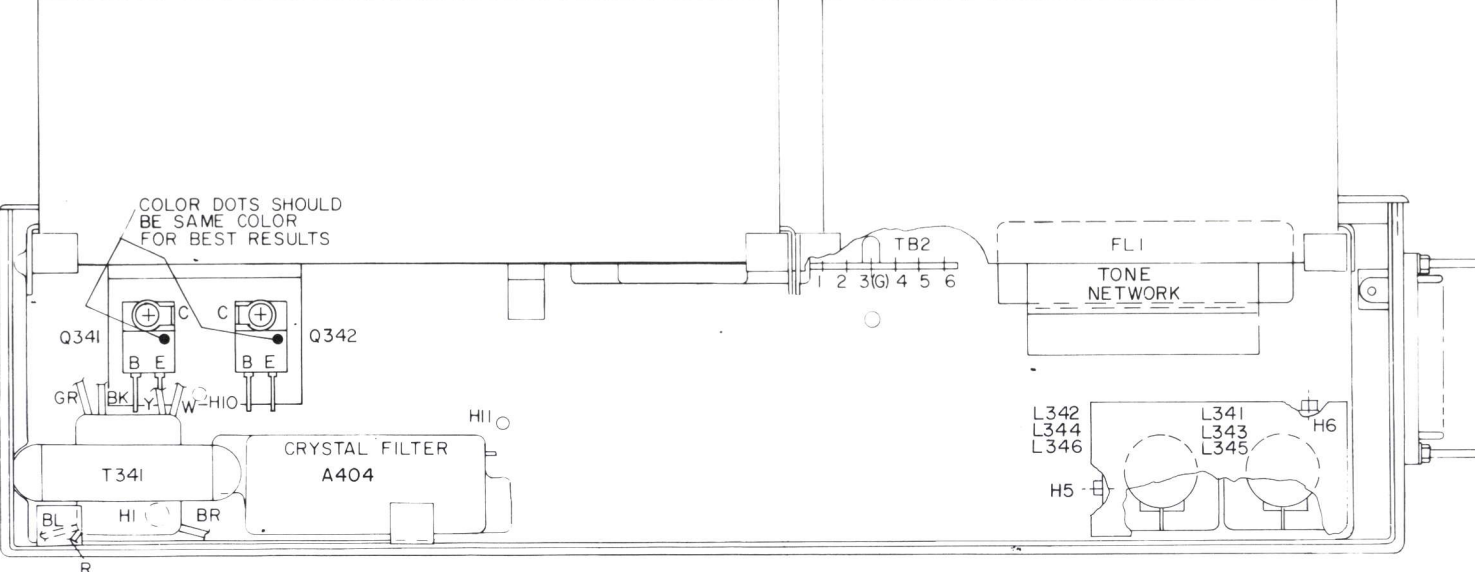
25—50 MHz, MASTR RECEIVER
MODELS 4ER39C68-85



IF-AUDIO & SQUELCH BOARD
A348



BOTTOM VIEW



[illegible]

MODEL NO.	FREQ. RANGE	NO FRE	CHAN GUARD
4ER39C68	25-33 MHz	1	
4ER39C69	33-42 MHz	1	X
4ER39C70	42-50 MHz	1	
4ER39C71	25-33 MHz	2	
4ER39C72	33-42 MHz	2	X
4ER39C73	42-50 MHz	2	
4ER39C74	25-33 MHz	4	
4ER39C75	33-42 MHz	4	X
4ER39C76	42-50 MHz	4	
4ER39C77	25-33 MHz	1	X
4ER39C78	33-42 MHz	1	X
4ER39C79	42-50 MHz	1	X
4ER39C80	25-33 MHz	2	X
4ER39C81	33-42 MHz	2	X
4ER39C82	42-50 MHz	2	X
4ER39C83	25-33 MHz	4	X
4ER39C84	33-42 MHz	4	X
4ER39C85	42-50 MHz	4	X

REV. LTR. BLOCK		REV
	PLI9E50087364	R
	PLI9E50087365	N
	PLI9E50087366	P
A347	PLI9B216119G1	A
A350	4EK16A10	D
A348	PLI9D413129G1	R
A402	PLI9C311797G2	B
	PLI9C303540G1	F
	PLI9C303540G2	F
	PLI9C303540G3	F

ALL RESISTORS ARE 1/2 WATT UNLESS OTHERWISE SPECIFIED AND RESISTOR VALUES IN OHMS UNLESS FOLLOWED BY K=1,000 OHMS OR MEG = 1,000,000 OHMS. CAPACITOR VALUES IN PICOFARADS (EQUAL TO MICROMICROFARADS) UNLESS FOLLOWED BY UF = MICROFARADS, INDUCTANCE VALUES IN MICROHENRYS UNLESS FOLLOWED BY MH = MILLIHENRYS OR H=HENRYS.

VOLTAGE READINGS

VOLTAGE READINGS ARE TYPICAL READINGS
MEASURED TO SYSTEM NEGATIVE (J442-8)
WITH TEST SET MODEL 4EX3A10 OR A
20,000 OHM-PER-VOLT METER.

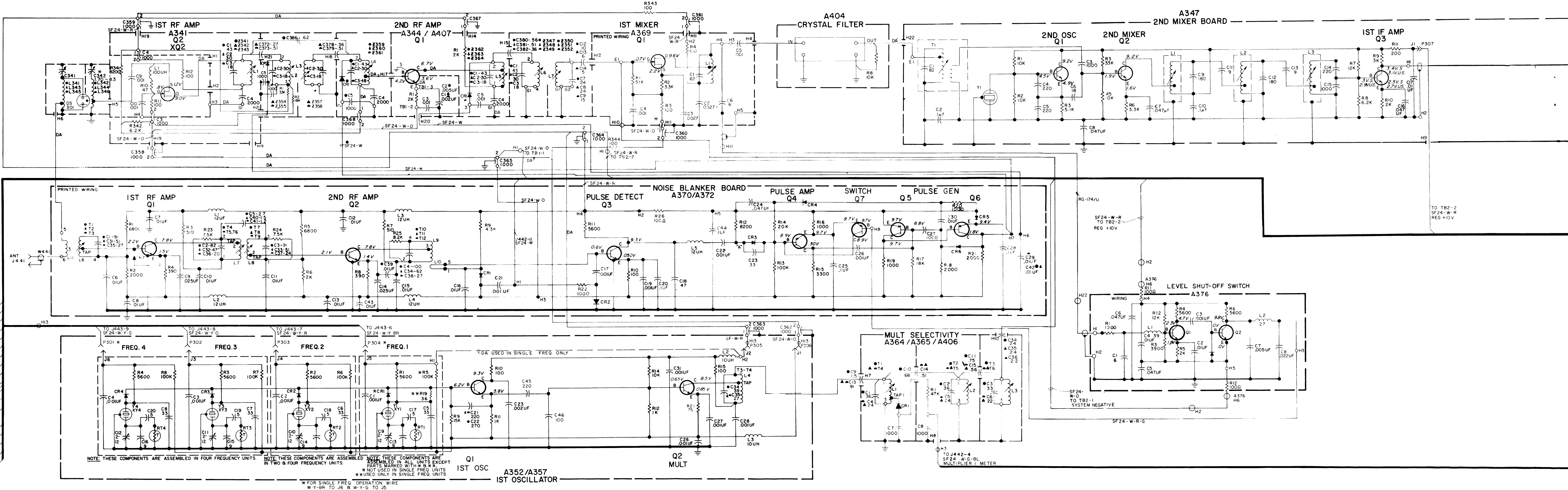
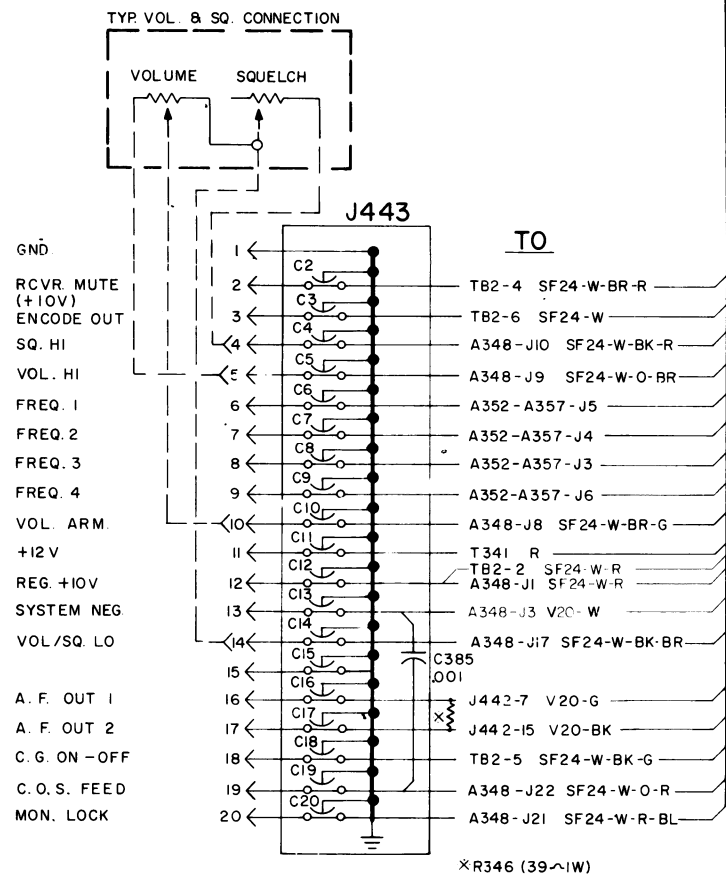
S= NO SIGNAL IN WITH SQUELCH CONTROL
FULLY COUNTERCLOCKWISE (MAXIMUM SQUELCH)

US = SQUELCH CONTROL FULLY CLOCKWISE
WITH A ONE MILLIVOLT MODULATED
SIGNAL (UNSQUELCHED) AND 5 WATT
AUDIO OUTPUT.

- LOW SPLIT 25-33 MHZ
- ▲ MID SPLIT 33-42 MHZ
- ▲ HIGH SPLIT 42-50 MHZ
- VALUE OF R47 IS DETERMINED BY TEST (SEE TEST SPEC 19A27182).
- THESE ARE ONLY PARTS PRESENT ON A402.
- * C342 1.80-8.3 IN HIGH SPLIT ONLY

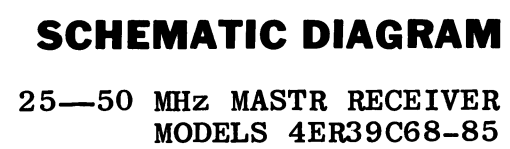
REV LTR BLOCK		REV
A352	PL19B204419G13	C
A353	PL19B204419G1C	C
A354	PL19B204419G14	A
A355	PL19B204419G17	A
A356	PL19B204419G15	A
A357	PL19B204419G18	A

IN ORDER TO RETAIN RATED EQUIPMENT PERFORMANCE, REPLACEMENT OF ANY SERVICE PART SHOULD BE MADE ONLY WITH A COMPONENT HAVING THE SPECIFICATION SHOWN ON THE PARTS LIST FOR THAT PART.



SCHEMATIC DIAGRAM

25—50 MHz MASTR RECEIVER
MODELS 4ER39C68-85



(Cont'd on Page 17)

(Cont'd from Page 16) (LBI4134)

SYMBOL	GE PART NO.	DESCRIPTION
R1*	3R152P202J	----- RESISTORS ----- Composition: 2K ohms $\pm 5\%$, 1/4 w. In REV L & earlier:
	3R152P510J	Composition: 51 ohms $\pm 5\%$, 1/4 w.
TB1	7487424P19	----- TERMINAL BOARDS ----- Miniature, phen: 3 terminals.
		CHASSIS AND RF ASSEMBLY 19E500873G4 19E500873G5 19E500873G6
C358 thru C365	5493392P7	----- CAPACITORS ----- Ceramic feed-thru: 1000 pf $\pm 100\%$ -0%, 500 VDCW; sim to Allen-Bradley Type FASC.
	5493392P7	Ceramic, feed-thru: 1000 pf $\pm 100\%$ -0%, 500 VDCW; sim to Allen Bradley Type FASC.
C367 and C368	5493392P7	
C372	5491601P107	Phenolic: 0.27 pf $\pm 5\%$, 500 VDCW.
C373	5491601P114	Phenolic: 0.51 pf $\pm 5\%$, 500 VDCW.
C378	5491601P110	Phenolic: 0.36 pf $\pm 5\%$, 500 VDCW.
C379	5491601P114	Phenolic: 0.51 pf $\pm 5\%$, 500 VDCW.
C380	5491601P115	Phenolic: 0.56 pf $\pm 5\%$, 500 VDCW.
C381	5491601P114	Phenolic: 0.51 pf $\pm 5\%$, 500 VDCW.
C382	5491601P110	Phenolic: 0.36 pf $\pm 5\%$, 500 VDCW.
C385	7774750P4	Ceramic disc: .001 μ f $\pm 100\%$ -0%, 500 VDCW.
C386	5491601P116	Phenolic: 0.62 pf $\pm 5\%$, 500 VDCW.
C387 and C388	5494481P12	Ceramic disc: 1000 pf $\pm 10\%$, 1000 VDCW; sim to RMC Type JF Discap.
CR1*	19A116062P2	----- DIODES AND RECTIFIERS ----- Thyrector. Deleted in 19E500873G4 by REV J. Deleted in 19E500873G5, G6 by REV H.
J442	19B205689G2	----- JACKS AND RECEPTACLES ----- Connector: 18 contacts rated at 5 amps min at 1000 VDC max.
J443	19C303426G1	Connector: 20 pin contacts.
L341 thru L346	19B209159P3	----- INDUCTORS ----- COIL ASSEMBLY L341 19B204820G5 L342 19B204820G6 L343 19B204820G1 L344 19B204820G2 L345 19B204820G3 L346 19B204820G4
C341		Variable, subminiature: approx 1.70-6.9 pf, 750 v peak; sim to EF Johnson 189.
C342*	19B209159P4	Variable, air, sub-miniature: 1.80-8.30 pf, 650 v peak; sim to EF Johnson 189.
19B209159P3	19B209159P3	In 19E500873G6 of REV N & earlier: Variable, air, sub-miniature: 1.70-6.9 pf, 750 v peak; sim to EF Johnson 189.
DS301	19B209067P1	----- INDICATING DEVICES ----- Lamp, glow: 0.3 ma; sim to GE NE-2T.
P301 thru P311	4029840P2	----- PLUGS ----- Contact, electrical; sim to Amp 42827-.
P312	4029840P3	Contact, electrical; sim to Amp 42101-2.
P313	4029840P2	Contact, electrical; sim to Amp 42827-2.
P315 thru P317	4029840P2	Contact, electrical; sim to Amp 42827-2.

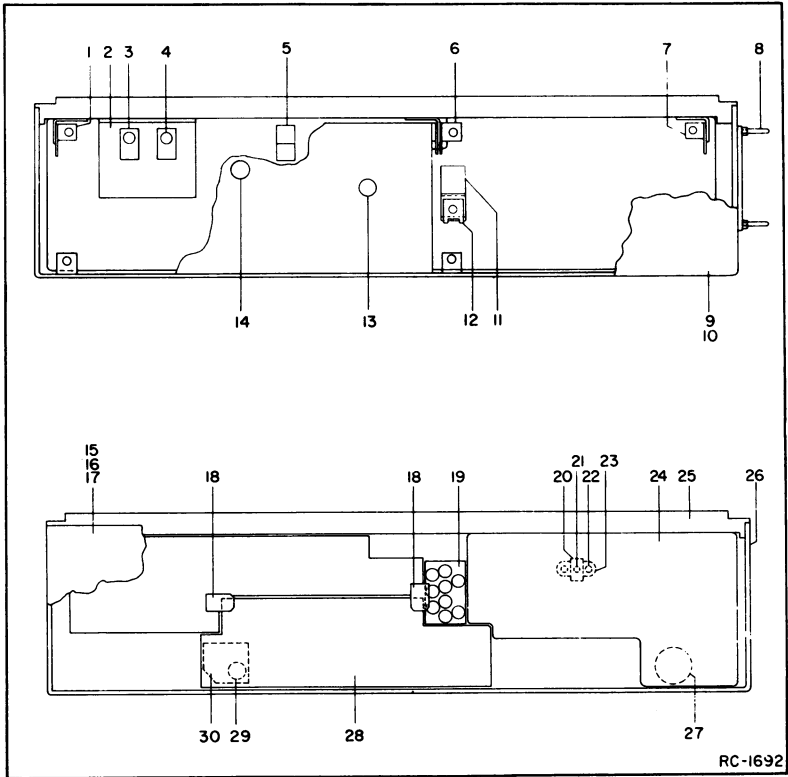
SYMBOL	GE PART NO.	DESCRIPTION
P319 and P320	4029840P2	Contact, electrical; sim to Amp 42827-2.
P322	4029840P2	Contact, electrical; sim to Amp 42827-2.
P323	4029840P1	Contact, electrical; sim to Amp 41854.
P324 thru P326	4029840P2	Contact, electrical; sim to Amp 42827-2.
P327	4029840P1	Contact, electrical; sim to Amp 41854.
Q341* and Q342*	19A116741P1	----- TRANSISTORS ----- Silicon, NPN. In 19E500873G4 of REV K & earlier: In 19E500873G5, G6 of REV J & earlier:
	19A116203P2	Silicon, NPN. ----- RESISTORS -----
R341	3R152P822K	Composition: 8.2K ohms $\pm 10\%$, 1/4 w.
R342*	3R152P622J	Composition: 6.2K ohms $\pm 5\%$, 1/4 w. In 19E500873G4 of REV M. In 19E500873G5, G6 of REV L.
	3R152P472J	Composition: 4.7K ohms $\pm 5\%$, 1/4 w. In 19E500873G4 REV L & earlier: In 19E500873G5, G6 REV K & earlier:
	3R152P222K	Composition: 2.2K ohms $\pm 10\%$, 1/4 w.
R343 and R344	3R152P101K	Composition: 100 ohms $\pm 10\%$, 1/4 w.
R345	19A116278P444	Metal film: 280K ohms $\pm 2\%$, 1/2 w.
R346	3R78P390K	Composition: 39 ohms $\pm 10\%$, 1 w. ----- TRANSFORMERS -----
T341	19A116041P2	Audio freq: 300 to 4000 Hz, ± 0.5 dB, Pri: 23.5 ohms imp, at 50 mA, Sec 1: 3.5 ohms imp at 1 KHz, Sec 2: 10.15 ± 0.10 VRMS. ----- TERMINAL BOARDS -----
TB1	7487424P26	Miniature, phen: 6 terminals. ----- CABLES -----
W441	19B205634G2	Coaxial: approx 5 inches long. ----- TUNED CIRCUITS -----
Z341 thru Z343		COIL ASSEMBLY Z341 19B204786G4 Z342 19B204786G5 Z343 19B204786G6 ----- CAPACITORS -----
C1	5496218P254	Ceramic disc: 43 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C2	5496218P250	Ceramic disc: 30 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C3	5496218P245	Ceramic disc: 18 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C4	5494481P14	Ceramic disc: 2000 pf $\pm 10\%$, 500 VDCW; sim to RMC Type JF Discap. ----- INDUCTORS -----
L1		(Part of Coil Assembly). ----- MISCELLANEOUS -----
	5491798P1	Tuning slug. (Used in Z341).
	5491798P4	Tuning slug. (Used in Z342).
	5491798P5	Tuning slug. (Used in Z343).

SYMBOL	GE PART NO.	DESCRIPTION
Z347 thru Z349		COIL ASSEMBLY Z347 19B204767G1 Z348 19B204767G2 Z349 19B204767G3
C1	5496218P254	----- CAPACITORS ----- Ceramic disc: 43 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C2	5496218P250	Ceramic disc: 30 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C3	5496218P245	Ceramic disc: 18 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
L6		----- INDUCTORS ----- (Part of Coil Assembly).
		----- MISCELLANEOUS -----
	5491798P1	Tuning slug. (Used in Z347).
	5491798P4	Tuning slug. (Used in Z348).
	5491798P5	Tuning slug. (Used in Z349).
Z350 thru Z352		COIL ASSEMBLY Z350 19B204784G8 Z351 19B204784G9 Z352 19B204784G10
C7 and C8	5496218P248	----- CAPACITORS ----- Ceramic disc: 24 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C9	5496218P244	Ceramic disc: 15 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C12	5496218P241	Ceramic disc: 10 pf ± 0.25 pf, 500 VDCW, temp coef -80 PPM.
C13	5496218P237	Ceramic disc: 6 pf ± 0.25 pf, 500 VDCW, temp coef -80 PPM.
C14	5496218P236	Ceramic disc: 5 pf ± 0.25 pf, 500 VDCW, temp coef -80 PPM.
L7		----- INDUCTORS ----- (Part of Coil Assembly).
		----- MISCELLANEOUS -----
	5491798P1	Tuning slug. (Used in Z350).
	5491798P4	Tuning slug. (Used in Z351).
	5491798P5	Tuning slug. (Used in Z352).
Z354 and Z355		COIL ASSEMBLY Z354 19B204767G4 Z355 19B204767G5
C2	5496218P250	----- CAPACITORS ----- Ceramic disc: 30 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C3	5496218P245	Ceramic disc: 18 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C4 and C5	5494481P12	Ceramic disc: 1000 pf $\pm 10\%$, 1000 VDCW; sim to RMC Type JF Discap.
CR1*	19A115250P1	----- DIODES AND RECTIFIERS ----- Silicon, fast recovery, 225 mA, 50 PIV. In 19E500873G4 of REV G & earlier: In 19E500873G5, G6 of REV F & earlier:
	7777146P3	Germanium.
L2		----- INDUCTORS ----- (Part of Coil Assembly).
R1	3R152P333K	----- RESISTORS ----- Composition: 33K ohms $\pm 10\%$, 1/4 w.

SYMBOL	GE PART NO.	DESCRIPTION
R2	3R152P183K	Composition: 18K ohms $\pm 10\%$, 1/4 w.
		----- MISCELLANEOUS -----
	5491798P5	Tuning slug. (Used in Z355).
	5491798P4	Tuning slug. (Used in Z354).
Z357 and Z358		COIL ASSEMBLY Z357 19B204783G2 Z358 19B204783G3
		----- CAPACITORS -----
C2	5496218P250	Ceramic disc: 30 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C3	5496218P245	Ceramic disc: 18 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
		----- INDUCTORS -----
L3		(Part of Coil Assembly).
		----- MISCELLANEOUS -----
	5491798P4	Tuning slug. (Used in Z357).
	5491798P5	Tuning slug. (Used in Z358).
Z359 thru Z361		COIL ASSEMBLY Z359* 19B204785G4 (In REV P) 19B204785G1 (In REV N and earlier) Z360 19B204785G2 Z361 19B204785G3
		----- CAPACITORS -----
C1	5496218P254	Ceramic disc: 43 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C2	5496218P250	Ceramic disc: 30 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C3	5496218P245	Ceramic disc: 18 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C4	5494481P14	Ceramic disc: 2000 pf $\pm 10\%$, 1000 VDCW; sim to RMC Type JF Discap.
C5	5494481P11	Ceramic disc: 1000 pf $\pm 20\%$, 1000 VDCW; sim to RMC Type JF Discap.
		----- DIODES AND RECTIFIERS -----
CR1	19A116052P1	Hot carrier: Fwd. drop .350 volts max.
		----- INDUCTORS -----
L4		(Part of Coil Assembly).
		----- MISCELLANEOUS -----
	5491798P1	Tuning slug. (Used in Z359- before REV P).
	5491798P4	Tuning slug. (Used in Z360).
	5491798P5	Tuning slug. (Used in Z361).
Z362 thru Z364		COIL ASSEMBLY Z362 19B204787G1 Z363 19B204787G2 Z364 19B204787G3
		----- CAPACITORS -----
C1	5496218P254	Ceramic disc: 43 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C2	5496218P250	Ceramic disc: 30 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C3	5496218P245	Ceramic disc: 18 pf $\pm 5\%$, 500 VDCW, temp coef -80 PPM.
C4	5494481P14	Ceramic disc: 2000 pf $\pm 10\%$, 1000 VDCW; sim to RMC Type JF Discap.
C5*	5494481P11	Ceramic disc: 1000 pf $\pm 20\%$, 1000 VDCW; sim to RMC Type JF Discap. Added to 19E500873G4 by REV M. Added to 19E500873G5, G6 by REV L.

SYMBOL	GE PART NO.	DESCRIPTION
CR1*	4038642P1	----- DIODES AND RECTIFIERS ----- Germanium. Added to 19E500873G4 by REV M. Added to 19E500873G5, G6 by REV L.
L5		----- INDUCTORS ----- (Part of Coil Assembly).
R1*	3R152P202J	----- RESISTORS ----- Composition: 2K ohms $\pm 5\%$, 1/4 w. In 19E500873G4 of REV L & earlier: In 19E500873G5, G6 of REV K & earlier:
	3R152P431J	Composition: 430 ohms $\pm 5\%$, 1/4 w.
	5491798P1	----- MISCELLANEOUS ----- Tuning slug. (Used in Z362).
	5491798P4	Tuning slug. (Used in Z363).
	5491798P5	Tuning slug. (Used in Z364).
		HARNESSE ASSEMBLY 19E500873G14 (Includes C385, C387, C388, J442, J443, P301- P304, P307-P313, P315-P317, P319, P320, P322- P327, R345, R346, T341).
		CHANNEL GUARD MODIFICATION KIT 19A127176G1 (Used with A350)
	19B216176G1	----- MISCELLANEOUS ----- Harness (Encoder/Decoder). Includes:
P314	4029840P2	Contact, electrical; sim to Amp 42827-2.
P318	4029840P2	Contact, electrical; sim to Amp 42827-2.
P321	4029840P2	Contact, electrical; sim to Amp 42827-2.
P328 thru P335	4029840P2	Contact, electrical; sim to Amp 42827-2.
		CHANNEL GUARD MODIFICATION KIT 19A127176G2 (Used with A402)
	19B216177G1	----- MISCELLANEOUS ----- Harness (Tone Reject Filter). Includes:
P321	4029840P2	Contact, electrical; sim to Amp 42827-2.
P330	4029840P2	Contact, electrical; sim to Amp 42827-2.
P332	4029840P2	Contact, electrical; sim to Amp 42827-2.
		MECHANICAL PARTS (SEE RC1692)
1	19B204583G3	Hinge.
2	19B216727P1	Support. (Used with Q341 & Q342).
3	19A116023P2	Plate, insulated. (Used with Q341 & Q342).
4	19A115222P3	Insulator, bushing. (Used with Q341 & Q342).
5	4029851P6	Clip, loop.
6	19B204583G1	Hinge.
7	19B204583G2	Hinge.
8	19A121676P1	Guide pin.
9	19C303396G4	Bottom cover. (Station)
10	19C303385G1	Bottom cover. (Mobile)
11	19A121297P1	Angle.
12	7160861P4	Nut, sheet spring: sim to Tinnerman C6452-8Z-67. (Used to secure cover).
13	4036555P1	Insulator, washer: nylon. (Used with Q7 on A348).

SYMBOL	GE PART NO.	DESCRIPTION
14	4035267P2	Button, plug. (Used with A348, A350 and A402).
15	19C303495G3	Top cover. (Station, except Repeaters and VM).
16	19C303676G2	Top cover. (Station, Repeaters and VM only).
17	19C303385P2	Top cover. (Mobile)
18	4029851P3	Clip, loop.
19	19A121383P1	Support.
20	4033089P1	Clip. (Part of XY1-XY4).
21	19B200525P9	Rivet. (Part of XY1-XY4).
22	19A115793P1	Contact. (Part of XY1-XY4).
23	4039307P1	Crystal socket. (Part of XY1-XY4).
24	19C303547P1	Cover.
25	19C317344P3	Heat sink.
26	19C303389G1	Chassis.
27	4034252P5	Can (Used with T1 on A347).
28	19B204672P1	Cover.
29	7162414P1	Retainer, transistor. (Used with Q1 on A341).
30	19B204917P1	Support.



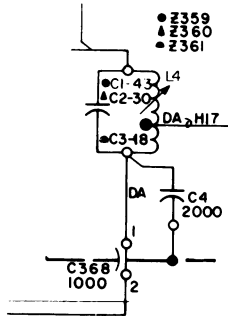
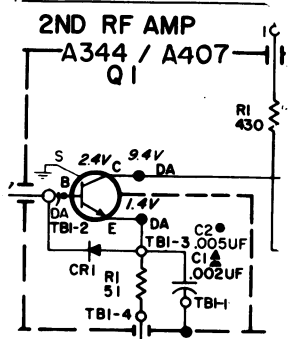
PRODUCTION CHANGES

Changes in the equipment to improve performance or to simplify circuits are identified by a "Revision Letter", which is stamped after the model number of the unit. The revision stamped on the unit includes all previous revisions. Refer to the Parts List for descriptions of parts affected by these revisions.

- REV. A - 2nd Mixer A347 (19B216119-G1)
Channel Guard Encoder/Decoder Model 4EK16A10 (19C311797-G1)
1st Osc/Mult A354 - A357 (19B204419-G14, 15, 17, 18)
- REV. C - 1st Osc/Mult A352 & A353 (19B204419-G13 - G18)
IF-Audio & Squelch A348 (19D413129-G1)
- REV. F - Chassis & RF Assembly (19E500873-G4 thru G6)
These revisions incorporated into initial shipment.
- REV. B - Channel Guard Encoder/Decoder Model 4EK16A10 (19C311797-G1)
To increase the stop-band attenuation. Changed R8.
- REV. C - Channel Guard Encoder/Decoder Model 4EK16A10 (19C311797-G1)
REV. A - Tone Reject Filter (19C311797-G2)
To optimize the frequency response. Changed C29.
- REV. D - Channel Guard Encoder/Decoder Model 4EK16A10 (19C311797-G1)
REV. B - Tone Reject Filter (19C311797-G2)
To prevent excessive roll-off at 300 Hertz. Changed R59.
- REV. D - IF-Audio & Squelch A348 (19D413129-G1)
To improve frequency response at 3000 Hertz. Changed R30 & R78
- REV. G - Chassis & RF Assembly (19E500873-G4)
To improve the blanker performance.
Added A407 and C2 to 2nd RF Amplifier.

- IF-Audio & Squelch A348 (19D413129G1)
- REV. E - To compensate for vendor change.
Changed C26.
- REV. F - To improve squelch action. Changed R53.
- REV. G - To improve operation. Changed CR3 and CR4.
- REV. H - To improve squelch action at -30°C.
Changed Q10.
- REV. H - Chassis & RF Assembly (19E500873G4)
To incorporate silicon diode. Changed CR1.
- REV. J - To eliminate unnecessary protection.
Deleted CR1.
- REV. K - To improve tuning. Deleted R14 on crystal
filter A404.
- REV. L - To incorporate new transistors.
Changed Q341 and Q342.
- REV. G - Chassis & RF Assembly (19E500873G5 & G6)
To incorporate silicon diode.
Changed CR1.
- REV. H - To eliminate unnecessary protection.
Deleted CR1.
- REV. J - To improve tuning.
Deleted R14 on crystal filter A404.
- REV. K - To incorporate new transistors.
Changed Q341 and Q342.
- REV. L - Chassis & RF Assembly (19E500873G5 & G6)
REV. M - Chassis & RF Assembly (19E500873G4)
To improve blanker performance. Changed
R342. Changed R1 and added C5 and CR1
to RF Amplifier A344. Changed R1, Deleted
CR1 and added C3 to RF Amplifier A407.
Schematic Diagram was:

SCHEMATIC DIAGRAM WAS:



- REV. D - Noise Blanker Board (19C303540G1,2 & 3)
To improve metering in positive ground
system. C21, C17, R22 & CR2.
- REV. E - Noise Blanker Board (19C303540G1,G2 & G3)
To improve blanker performance. Changed
C6 thru C16, CR3, Q4, R12 and R13.
- REV. M - Chassis & RF Assembly (19E500873G5 & G6)
REV. N - Chassis & RF Assembly (19E500873G4)
To increase RF attenuation for proper
blanking. Changed R342.
- REV. F - Noise Blanker Board (19C303540G1 & G2)
To increase RF attenuation for proper
blanking. Changed C42.
- REV. J - IF-Audio & Squelch A348 (19D413129G1)
To correct PA bias. Changed R40.
- REV. K - To improve stability of audio output with
no load. Added R85.
- REV. L - To improve frequency response at 300 Hz.
Deleted R85 and Changed C40.
- REV. M - To improve audio quality. Changed R80.
- REV. N - To improve frequency response. Changed C26.
- REV. P - To improve stability. Changed Q5.
- REV. F - Noise Blanker Board (19C303540G3)
To improve blanker restoration.
Changed C29.
- REV. P - Chassis & RF Assembly (19E500873G4)
To improve operation. Changed Z359.
- REV. R - To incorporate new transistor. Changed Q2.
- REV. N - Chassis & RF Assembly (19E500873G5 & G6)
To incorporate new transistor. Changed Q2.
- REV. P - Chassis & RF Assembly (19E500873G6)
To improve tuning range of 2nd RF stage.
Changed C342.
- REV. R - IF Audio & Squelch A348 (19D413129G1)
To improve Squelch action. Deleted R56
and added R86.

ORDERING SERVICE PARTS

Each component appearing on the schematic diagram is identified by a symbol number, to simplify locating it in the parts list. Each component is listed by symbol number, followed by its description and GE Part Number.

Service parts may be obtained from Authorized GE Communication Equipment Service Stations or through any GE Radio Communication Equipment Sales Office. When ordering a part, be sure to give:

1. GE Part Number for component
2. Description of part
3. Model number of equipment
4. Revision letter stamped on unit

These instructions do not purport to cover all details or variations in equipment nor to provide for every possible contingency to be met in connection with installation, operation or maintenance.

Should further information be desired, or should particular problems arise which are not covered sufficiently for the purchaser's purposes, contact the nearest Radio Communication Equipment Sales Office of the General Electric Company.

MAINTENANCE MANUAL
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MOBILE RADIO DEPARTMENT
GENERAL ELECTRIC COMPANY • LYNCHBURG, VIRGINIA 24502



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